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NAVIGATION

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RAY'S MATHEMATICAL SERIES.

SURVEYING

AND

NAVIGATION,

WITH A PRELIMINARY TREATISE ON

TRIGONOMETRY AND MENSURATION,

BY

A. SCHUYLER, M. A.,

*Professor of Mathematics and Philosophy in Kansas Wesleyan University;
Author of Principles of Logic, Empirical and Rational Psychology
and of a Series of Mathematical Works.*

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PREFACE.

Nearly twenty years ago the Publishers made the following
announcement: "*Surveying and Navigation*; containing Survey-
ing and Leveling, Navigation, Barometric Heights, etc."

To redeem this promise, the present work now appears.

It is customary to preface works on Surveying by a meager
sketch of Plane Trigonometry, but it has been thought best
to include in this work a thorough treatment of Plane and
Spherical Trigonometry and Mensuration. These subjects have
been treated in view of the wants of our best High Schools
and Colleges.

Certain modern writers have defined the Trigonometric func-
tions as ratios; for example, in a right triangle, the sine of an
angle is the ratio of the opposite side to the hypotenuse, etc.

The historical method of considering the sine, co-sine, tan-
gent, etc., as linear functions of the arc, explains the origin of
these terms—avoids the ambiguity of the word *ratio*; explains
how the logarithm of the sine, for example, can reach the limit
10, which would be impossible if the limit of the sine itself is
1, and is much more readily apprehended by the student.

The advantages in analytic investigations resulting from
defining these functions as ratios have been secured in the
principles relating to the Right Triangle, Art. 64.

Each of the circular functions has, in the first place, been
considered by itself, and its value traced, for all arcs, from 0°
• to 360°.

Then follows the solution of triangles, right and oblique, the general relations of the circular functions, the functions of the sum or difference of two angles, and a variety of interesting practical applications.

It is hoped that Spherical Trigonometry has been made intelligible to the diligent student. More than ordinary care has been given to the development of Napier's principles, and to the discussion of the species of the parts of both right and oblique spherical triangles, Arts. 126, 129, 145, 148, 151.

Mensuration, a subject at once interesting and practically important, has been discussed at length, and formulas have been developed instead of rules for the solution of the problems.

In the Surveying, the instruments are first represented and described, and the methods of making the adjustments given in detail.

The Author takes this opportunity to express his obligations to Messrs. W. & L. E. Gurley, Manufacturers of Surveying and Engineering Instruments, Troy, N. Y., who have kindly granted him the use of their Manual for the delineation and description of the instruments. In consequence of this courtesy, much better drawings and descriptions have been made than would otherwise have been possible.

The instruments themselves should, however, be accessible to the student, who should study them in connection with the descriptions in the book, and learn to use them in practical work, guided by a competent instructor.

The Rectangular method of surveying the Public lands, now, brought to great perfection under the direction of the Government, has been minutely explained, and illustrated by field notes of actual surveys. In this portion of the work, the United States Manual of Surveying Instructions has been taken as authority, and thus the authorized methods, which must form the basis for subsequent surveys, have been made accessible to the student.

The methods of finding the true meridian and the variation of the needle have been given at length; also specific direc-

tions for finding corners, taking bearings, measuring lines, recording field notes, and plotting.

In addition to the ordinary method of finding the area, a new method, developed by E. M. Pogue, of Kentucky, is given in Art. 304. This method has the merit of giving always a uniform result from the same field notes, and thus avoids disputes about the different results of the ordinary method, unavoidably attending the various distribution of errors by different calculators.

The methods of supplying omissions are explained and illustrated by examples.

Laying out and dividing land, operations admitting of an unlimited variety of applications, have been treated in view of the wants of the practical surveyor. The subject is also full of interest to the student, who can not fail to receive from it new views of the resources of mathematical science.

Leveling, the construction of railroad curves, embankments and excavations, the method of making Topographical surveys, with the authorized conventional symbols, Barometric heights, etc., have been explained and illustrated by diagrams and examples.

It has been thought best to give a clear, elementary treatment of Navigation, not only on account of those who may desire to pursue the subject further, but for the sake of gratifying the wishes of intelligent persons who may desire to know something of Navigation. The limits of the work, however, forbid the discussion of Nautical Astronomy. The examples in Navigation have been selected from the English work of J. R. Young.

The tables of Logarithms, Natural and Logarithmic sines, etc., have been carried only to five decimal places, and for the purposes intended will be found practically better than tables to six or seven places.

The Traverse table has been thrown into a new form, at once condensed and convenient.

These tables have been compiled by Mr. Henry H. Vail, and

by him compared with Babbage's and Wittstein's tables, then by the Author with Vega's tables to seven decimal places. It is hoped that by this double comparison perfect accuracy has been attained.

The table of Meridional Parts, taken from "Projection Tables for the use of the United States Navy," prepared by the Bureau of Navigation, and issued from the Government Printing office, was calculated in the Hydrographic office for the terrestrial spheroid, compression $\frac{1}{297}$. This table, now for the first time published in a text-book, is believed to be more correct than those in general use.

The Author takes pleasure in acknowledging his obligations to Prof. E. H. Warner for critical suggestions and acceptable aid in reading proof and testing the accuracy of the answers.

With the hope that the book will be attractive and useful to the student, teacher, and practical surveyor, it is sent forth to accomplish its work.

A. SCHUYLER.

BALDWIN UNIVERSITY,
BEREA, O., JUNE 12, 1873. }

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INTRODUCTION.

LOGARITHMS.

1. Definition.

A logarithm of a number is the exponent denoting the power to which a fixed number, called the base, must be raised in order to produce the given number.

Thus, in the equation, $b^x = n$, b is the base of the system, n is the number whose logarithm is to be taken, and x is the logarithm of n to the base b , which may be written: $x = \log_b n$.

Any positive number, except 1, may be assumed as the base, but when assumed, it remains fixed for a system; hence, there may be an infinite number of systems, since there may be an infinite number of bases.

2. Common Logarithms.

Common logarithms are the logarithms of numbers in the system whose base is 10.

$$\begin{aligned}
 10^0 &= 1; & \therefore & \text{by def., } \log 1 = 0. \\
 10^1 &= 10; & \therefore & \text{by def., } \log 10 = 1. \\
 10^2 &= 100; & \therefore & \text{by def., } \log 100 = 2. \\
 10^3 &= 1000; & \therefore & \text{by def., } \log 1000 = 3.
 \end{aligned}$$

Hence, In the common system, the logarithm of an exact power of 10 is the whole number equal to the exponent of the power.

3. Consequences.

1. If the number is greater than 1 and less than 10, its logarithm is greater than 0 and less than 1, or is 0 + a decimal.

2. If the number is greater than 10 and less than 100, its logarithm is greater than 1 and less than 2, or is 1 + a decimal.

3. In general, if the number is not an exact power of 10, its logarithm, in the common system, will consist of two parts—an entire part and a decimal part.

The entire part is called the *characteristic* and the decimal part is called the *mantissa*.

4. Problem.

To find the laws for the characteristic.

Let (1) $10^x = n$; then, by def., $\log n = x$.

But (2) $10^1 = 10$.

(1) + (2) = (3) $10^{x-1} = \frac{n}{10}$; then, by def., $\log \frac{n}{10} = x - 1$.

$$\therefore \log \frac{n}{10} = \log n - 1.$$

Hence, *The logarithm of the quotient of any number by 10 is less by 1 than the logarithm of the number.*

Let us now take the number 8979 and its logarithm 3.95323, as given in a table of logarithms, and divide the number successively by 10, and for each division subtract 1 from the logarithm of the dividend, then we have,

$$\text{Log } 8979 = 3.95323.$$

$$\text{" } 897.9 = 2.95323.$$

$$\text{" } 89.79 = 1.95323.$$

$$\text{" } 8.979 = 0.95323.$$

$$\text{Log } .8979 = \overline{1}.95323.$$

$$\text{" } .08979 = \overline{2}.95323.$$

$$\text{" } .008979 = \overline{3}.95323.$$

$$\dots \dots \dots$$

The minus sign applies only to the characteristic over which it is placed.

The mantissa is always positive, and is the same for all positions of the decimal point.

An inspection of the above will reveal the following laws:

1. *If the number is integral or mixed, the characteristic is positive and is one less than the number of integral figures.*

2. *If the number is entirely decimal, the characteristic is negative and is one greater, numerically, than the number of 0's immediately following the decimal point.*

5. Exercises on the Characteristic.

1. What is the characteristic of the logarithm of 7?

2. What is the characteristic of the logarithm of 465?

3. What is the characteristic of the logarithm of 4678?

4. What is the characteristic of the logarithm of 34.75?

5. What is the characteristic of the logarithm of .65?

6. What is the characteristic of the logarithm of .0789?

7. What is the characteristic of the logarithm of .00084?

8. If the characteristic of the logarithm of a number is 2, how many integral places has that number?

9. If the characteristic of the logarithm of a number is 5, how many integral places has that number?

10. If the characteristic of the logarithm of a number is 1, how many integral places has that number?

11. If the characteristic of the logarithm of a number is 0, how many integral places has that number?

12. If the characteristic of the logarithm of a number is negative, is the number integral, decimal, or mixed?

13. If the characteristic of the logarithm of a number is $\overline{4}$, how many 0's immediately follow the decimal point?

14. If the characteristic of the logarithm of a number is $\overline{2}$, how many 0's immediately follow the decimal point?

15. If the characteristic of the logarithm of a number is $\overline{1}$, how many 0's immediately follow the decimal point?

TABLE OF LOGARITHMS.

6. Description of the Table.

The table of logarithms annexed gives the mantissa of the logarithm of every number from 1000 to 10900. The characteristic can be found by the preceding laws.

It follows, from Art. 4, that the mantissa of the logarithm of a number is the same as the mantissa of the logarithm of the product or quotient of that number by any power of 10. Thus:

$$\begin{aligned}\text{Log } 12 &= 1.07918. \\ \text{" } 120 &= 2.07918. \\ \text{" } .012 &= \overline{2}.07918.\end{aligned}$$

Hence, we can determine from the table the logarithm of any number less than 1000. Thus, the mantissa of the logarithm of 8 is the same as that of the logarithm of 8000.

In the table, the first three or four figures of each number are given in the left-hand column, marked *N*. The next figure is given at the head and foot of one of the columns of mantissas.

The mantissas, in the column under 0, are given to five decimal places. The first and second decimal figures of this column are understood to be repeated in the spaces below, and to be prefixed, across the page, to the three figures of the remaining columns.

When the third decimal digit changes from 9 to 0, the second is increased by the 1 carried; and the corresponding mantissa, and all to the right, commence with a smaller figure, to indicate that the first two decimal figures, to be prefixed, are to be taken from the line below.

The last column, marked *D*, contains the difference of two successive mantissas, called the *tabular difference*.

7. Problem.

To find the logarithm of a given number.

1. Find the logarithm of 3675.

The characteristic is 3. Opposite 367, in the column headed *N*, and under the column headed 5, we find 526, to which prefix the two figures, 56, in the column headed 0, and we have for the mantissa .56526.

$$\therefore \log 3675 = 3.56526.$$

2. Find the logarithm of 76.

The characteristic is 1, and the mantissa is the same as that of 7600, which is .88081.

$$\therefore \log 76 = 1.88081.$$

3. Find the logarithm of .004268.

The characteristic is $\overline{3}$, and the mantissa is the same as that of 4268. Looking opposite 426, and under 8, we find 022, of which the 0 is a small figure. Prefixing

63, from the line below, in the column headed 0, we have for the mantissa .63022

$$\therefore \log 109684 = 5.63022.$$

4. Find the logarithm of 109684.

$$\text{The characteristic} = 5.$$

$$\text{The mantissa of } \log 1096 = .03981$$

$$\text{Tab. diff. is 40; and } 40 \times .84 = 34$$

$$\log 109684 = 5.04015$$

The reason for multiplying the tabular difference by 84 will be apparent from the following:

$$\log 109600 = 5.03981.$$

$$\log 109700 = 5.04021.$$

The difference of the logarithms is 40 hundred-thousandths, and the difference of the numbers is 100 but the difference of 109600 and 109684 is 84, which is .84 of 100; hence, the difference of the logarithms of 109600 and 109684 is .84 of 40 hundred-thousandths, which is 40 hundred-thousandths $\times .84 = 34$ hundred-thousandths, nearly.

It is assumed that the difference of the logarithms of two numbers is proportional to the difference of the numbers, which is approximately true, especially if the numbers are large.

5. Find the logarithm of 123.613.

$$\text{The characteristic} = 2.$$

$$\text{The mantissa of } \log 1236 = .09202$$

$$\text{Tab. diff. is 35; and } 35 \times .13 = 5$$

$$\therefore \log 123.613 = 2.09207$$

The tabular difference is .00035, and $.00035 \times .13 = 0.0000455$. But since the logarithms in this table are taken only to five decimal places, the two last figures,

55, are rejected, and 1 is carried to .00004, making .00005 for the correction.

In general, when the left-hand figure of the part rejected exceeds 4, carry 1.

When the tabular difference is large, as in the first part of the table, there may be small errors. Accordingly, for numbers between 10000 and 100000, it will be better to use the last two pages instead of the first page.

8. Rule.

1. If the number, or the product of the number by any power of 10, is found in the table, take the corresponding mantissa from the table, and prefix the proper characteristic.

2. If the number, without reference to the decimal point or 0's on the right, is expressed by more than five figures, take from the table the mantissa corresponding to the first four or five figures on the left, multiply the corresponding tabular difference by the number expressed by the remaining figures, considered as a decimal, reject from the product as many figures on the right as are in the multiplier, correct to the nearest unit, and add the result as so many hundred-thousandths to the mantissa before found, and to the sum prefix the proper characteristic.

9. Examples.

$$1. \text{ What is the logarithm of } 234? \quad \text{Ans. } 3.37051.$$

$$2. \text{ What is the logarithm of } 108457? \quad \text{Ans. } 5.03526.$$

$$3. \text{ What is the logarithm of } 376542? \quad \text{Ans. } 5.57581.$$

$$4. \text{ What is the logarithm of } 229.7052? \quad \text{Ans. } 2.36117.$$

$$5. \text{ What is the logarithm of } 1128737? \quad \text{Ans. } 6.05260.$$

$$6. \text{ What is the logarithm of } .30365? \quad \text{Ans. } 1.48237.$$

$$7. \text{ What is the logarithm of } .0042683? \quad \text{Ans. } 3.63025.$$

$$8. \text{ What is the logarithm of } 1245400? \quad \text{Ans. } 6.09551.$$

10. Problem.

To find the number corresponding to a given logarithm.

1. What number corresponds to logarithm 2.03262?

The mantissa is found in the column headed 8, and opposite 107 in the column headed N. Hence, without reference to the decimal point, the number corresponding is 1078; but since the characteristic is 2, the number is entirely decimal, and one 0 immediately follows the decimal point. Hence, the number corresponding is .01078.

2. What number corresponds to logarithm 2.83037?

Since this logarithm can not be found in the table, take the next less, which is 2.83033, and the corresponding number, without reference to the decimal point, which is 6766.

The difference between the given logarithm and the next less is 4, and the tabular difference is 6, which is the difference of the logarithms of the two numbers, 6766 and 6767, whose difference is 1.

If the tabular difference of the logarithms, 6, corresponds to a difference in the numbers of 1, the difference of the logarithms, 4, will correspond to a difference of $\frac{2}{3}$ of 1; which, reduced to a decimal, and annexed to 6766, will give for the number, without reference to the decimal point, 676666. But since the characteristic is 2, there will be three integral places; hence, 676.666 is the number required.

3. What number corresponds to logarithm 2.76398?

The given log 2.76398 \therefore number 580737

Next less log 2.76395 \therefore number 5807

Tab. difference 3,200 difference

37 = correction.

It is necessary to write only that part of the next less logarithm which differs from the given logarithm. Conceive 0s annexed to the difference, and divide by the tabular difference, and annex the quotient to the number corresponding to the next less logarithm.

In practical work abbreviate thus. Let l denote the given logarithm; l' , the next less logarithm, n and n' , the corresponding numbers; t , the tabular difference; d , difference of logarithms; c , the correction.

4. What number corresponds to logarithm 1.73048?

$$l = 1.73048 \therefore n = .537625$$

$$l' = 1.73046 \therefore n' = .5376$$

$$t = 8 \quad 2 \quad d, \quad n' \text{ is found first, then } n \text{ by annexing } c.$$

$$25 = c.$$

11. Rule.

1. If the given mantissa can be found in the table, take the number corresponding, and place the decimal point according to the law for the characteristic.

2. If the given mantissa can not be found in the table, take the next less and the corresponding number. Subtract this mantissa from the given mantissa, annex 0s to the remainder, divide the result by the tabular difference, annex the quotient to the number corresponding to the logarithm next less than the given logarithm, and place the decimal point according to the law for the characteristic.

12. Examples.

1. What number corresponds to logarithm 4.55763?

Ans. 36000

2. What number corresponds to logarithm 3.95147?

Ans. 89128

3. What number corresponds to logarithm 2.11130?

Ans. 1025781

4. What number corresponds to logarithm 1.18237?
Ans. .30365.
5. What number corresponds to logarithm 3.65025?
Ans. .0042683.

MULTIPLICATION BY LOGARITHMS.

13. Proposition.

The logarithm of the product of two numbers is equal to the sum of their logarithms.

$$\text{Let } \begin{cases} (1) \ b^x = m; \text{ then, by def., } \log m = x, \\ (2) \ b^y = n; \text{ then, by def., } \log n = y. \end{cases}$$

$$(1) \times (2) = (3) \ b^{x+y} = mn; \text{ then, by def., } \log mn = x + y.$$

$$\therefore \log mn = \log m + \log n.$$

14. Rule.

1. Find the logarithms of the factors and take their sum, which will be the logarithm of the product.
2. Find the number corresponding which will be their product.

15. Examples.

1. Find the product of 57846 and .003927.
 $\log 57846 = 4.76228$
 $\log .003927 = 3.59406$
 $\log \text{product} = 2.35634, \therefore \text{product} = 227.16.$
2. Find the product of 37.58 and 75864.
Ans. 2851000.
3. Find the product of .3754 and .00756.
Ans. .002838.

4. Find the product of 999.75 and 75.85.
Ans. 75831.667.
5. Find the product of 85, .097, and .125. *Ans.* 1.03062.

DIVISION BY LOGARITHMS.

16. Proposition.

The logarithm of the quotient of two numbers is equal to the logarithm of the dividend minus the logarithm of the divisor.

$$\text{Let } \begin{cases} (1) \ b^x = m; \text{ then, by def., } \log m = x. \\ (2) \ b^y = n; \text{ then, by def., } \log n = y. \end{cases}$$

$$(1) \div (2) = (3) \ b^{x-y} = \frac{m}{n}; \text{ then, by def., } \log \frac{m}{n} = x - y.$$

$$\therefore \log \frac{m}{n} = \log m - \log n.$$

17. Rule.

1. Find the logarithms of the numbers, subtract the logarithm of the divisor from the logarithm of the dividend, and the remainder will be the logarithm of the quotient.
2. Find the number corresponding which will be the quotient.

18. Examples.

1. Divide 73125 by .125.
 $\log 73125 = 1.86407$
 $\log .125 = 1.09691$
 $\log \text{quotient} = 2.76716, \therefore \text{quotient} = 585.$
2. Divide 7.5 by .000025. *Ans.* 300000.
3. Divide 87.9 by .0345. *Ans.* 2547.824.
4. Divide .31852 by .00789. *Ans.* 40.371.
5. Divide 85734 by 12.7523. *Ans.* 6723.

ARITHMETICAL COMPLEMENT.

19. Definition.

The **arithmetical complement** of a logarithm is the result obtained by subtracting that logarithm from 10. Thus, denoting the logarithm by l , and its arithmetical complement by $a. c. l$, we shall have the formula,

$$a. c. l = 10 - l$$

The arithmetical complement of a logarithm is most readily found by commencing at the left of the logarithm, and subtracting each digit from 9 till we come to the last numeral digit, which must be subtracted from 10.

Thus, to find the $a. c.$ of 3.47540, we say: 3 from 9, 6; 4 from 9, 5; 7 from 9, 2; 5 from 9, 4; 4 from 10, 6; 0 from 0, 0.

$$\therefore a. c. \text{ of } 3.47540 = 6.52460.$$

20. Proposition.

The difference of two logarithms is equal to the *mantissa*, plus the arithmetical complement of the subtrahend, minus 10.

$$\text{For, } l - l' = l + (10 - l') - 10.$$

It is convenient to use the $a. c.$ in division when either the dividend or the divisor is the indicated product of two or more factors. Thus, let it be required to find x in the proportion:

$$37.5 : 678.5 :: 27.56 : x; \therefore x = \frac{678.5 \times 27.56}{37.5}$$

$$\therefore \log x = \log 678.5 + \log 27.56 + a. c. \log 37.5 - 10.$$

$$\log 678.5 = 2.83155$$

$$\log 27.56 = 1.44028$$

$$a. c. \log 37.5 = 8.42597$$

$$\log x = 2.69780 \quad \therefore x = 498.656.$$

21. Examples.

$$1. \text{ Given } 125.5 : .0756 :: x : .0034532, \text{ to find } x$$

$$\text{Ans. } 5.7325$$

$$2. \text{ Given } 813 : x :: 732.534 : .759, \text{ to find } x.$$

$$\text{Ans. } .87346$$

$$3. \text{ Given } x : .034 :: .784 : .00489, \text{ to find } x.$$

$$\text{Ans. } 5.451125.$$

$$4. \text{ Given } x = \frac{32.015 \times .874}{.000216 \times .90257}, \text{ to find } x. \quad \text{Ans. } 1.4353$$

$$5. \text{ Given } .753 \div 12.234 \div 87.5 \div 3.7547 \div .565 \div x, \text{ to find } x$$

$$\text{Ans. } 2614.96$$

INVOLUTION BY LOGARITHMS.

22. Proposition.

The logarithm of any power of a number is equal to the logarithm of the number multiplied by the exponent of the power.

$$\text{Let } (1) \quad b^r = n, \text{ then, by def., } \log n = r.$$

$$(1)^p = (2) \quad b^{pr} = n^p, \text{ then, by def., } \log n^p = pr.$$

$$\log n^p = p \log n$$

23. Rule.

1. Find the logarithm of the number and multiply it by the exponent of the power, and the product will be the logarithm of the power.

2. Find the number corresponding which will be the power.

24. Examples.

$$1. \text{ Find the cube of } .034$$

$$(1) \log .034 = 2.53148$$

$$(1) \times 3 = (2) \log .034^3 = 5.59444 \quad .034^3 = .00039304$$

$$2. \text{ Find the square of } 25.7.$$

$$\text{Ans. } 660.49$$

3. Find the fourth power of .75. *Ans.* .3164.
 4. Find the cube of .807. *Ans.* .52555.
 5. Find the fifth power of .9. *Ans.* .59049.

EVOLUTION BY LOGARITHMS.

25. Proposition.

The logarithm of any root of a number is equal to the logarithm of the number divided by the index of the root.

Let (1) $b^x = n$; then, by def., $\log n = x$.

(1) $b^x = n$; then, by def., $\log b^x = \log n = x$.

$$\therefore \log \sqrt[r]{n} = \frac{\log n}{r}.$$

26. Rule.

1. Find the logarithm of the number, divide it by the index of the root, and the quotient will be the logarithm of the root.
2. Find the number corresponding which will be the root.

27. Examples.

1. Extract the square root of .75.

$$(1) \log .75 = 1.87506$$

$$(1) \div 2 = (2) \log \sqrt{.75} = 1.93753 \therefore \sqrt{.75} = .86602.$$

$$\text{Subtract } 1.87506 \div 2 = (2 + 1.87506) \div 2 = 1.93753$$

$$2. \text{ Extract the cube root of } 91125. \quad \text{Ans. } 45.$$

$$3. \text{ Find the value of } \frac{2}{3} \div 5. \quad \text{Ans. } .80443.$$

$$4. \text{ Extract the fifth root of } .075. \quad \text{Ans. } .59569.$$

$$5. \text{ Find the value of } \sqrt[4]{\frac{37.5 \times (.78)^2}{12.5 \times 5.9}}. \quad \text{Ans. } .676317.$$

TRIGONOMETRY.

28. Definition and Classification.

Trigonometry is that branch of Mathematics which treats of the solution of triangles.

Trigonometry is divided into two branches — *Plane* and *Spherical*.

PLANE TRIGONOMETRY.

29. Definition.

Plane Trigonometry is that branch of Trigonometry which treats of the solution of plane triangles.

30. Parts of a Triangle.

Every triangle has six parts—three sides and three angles.

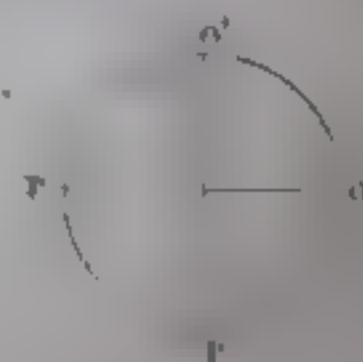
If three parts are given, one being a side, the remaining parts can be computed.

If the three angles only are given, the triangle is indeterminate, since an infinite number of similar triangles will satisfy the conditions.

31. Sexagesimal Division of Angles and Area.

The horizontal diameter, OP , called the *primary diameter*, and the vertical diameter, $O'P'$, called the *secondary diameter*, divide the circumference into four equal parts, called *quadrants*.

OO' is the *first quadrant*, $O'P'$ the *second*, $P'P$ the *third*, and PO the *fourth*.



A degree is one-ninetieth of a right angle, or of a quadrant.

A minute is one-sixtieth of a degree.

A second is one-sixtieth of a minute.

Thus, $25^{\circ} 34' 46''$ denote 25 degrees, 34 minutes, and 46 seconds.

An angle, whose vertex is at the center, has the same numerical measure, or contains the same number of degrees, minutes, and seconds, as the arc of the circumference intercepted by its sides.

32. Centesimal Division of Angles and Arcs.

A grade is one-hundredth of a right-angle, or of a quadrant.

A minute is one-hundredth of a grade.

A second is one-hundredth of a minute.

Thus, $7^{\circ} 24' 40''$ denotes 7 grades, 24 minutes, and 40 seconds.

$$\begin{aligned} 1^{\circ} &= \frac{10^{\circ}}{9}, \quad 1' = \frac{50'}{27}, \quad 1'' = \frac{250''}{81} \\ 1' &= \frac{9^{\circ}}{10}, \quad 1'' = \frac{27'}{50}, \quad 1''' = \frac{81''}{250} \end{aligned}$$

Let d, m, s , respectively, denote an angle expressed in degrees, sexagesimal minutes and seconds, and let g, μ, σ , respectively, denote the same angle expressed in grades, centesimal minutes and seconds, then expressing the ratio of the angle to a right angle in each kind of units, we shall have:

$$\begin{aligned} \frac{d}{90} &= \frac{g}{100}, \quad \frac{m}{5400} = \frac{\mu}{10000}, \quad \frac{s}{324000} = \frac{\sigma}{1000000} \\ \therefore d &= \frac{9}{10} g, \quad m = \frac{27}{50} \mu, \quad s = \frac{81}{250} \sigma \\ \therefore g &= \frac{10}{9} d, \quad \mu = \frac{50}{27} m, \quad \sigma = \frac{250}{81} s \end{aligned}$$

Let r denote the radius, and $\pi = 3.14159265358979 \dots$

πr = a semi-circumference = $180^{\circ} = 200^{\circ}$ = two right angles.

$\frac{\pi}{2} r$ = a quadrant = $90^{\circ} = 100^{\circ}$ = one right angle.

$2\pi r$ = a circumference = $360^{\circ} = 400^{\circ}$ = four right angles.

If $r = 1$, the above expressions become, respectively, $\pi, \frac{\pi}{2}, 2\pi$.

33. Unit of Circular Measure.

The unit of circular measure is that angle at the center whose intercepted arc is equal in length to the radius.

Let u denote the unit of circular measure, and r the radius.

Then, since πr = the semi-circumference, $\pi u = 180^{\circ} = 200^{\circ}$.

$$u = \frac{180^{\circ}}{\pi} = 57^{\circ}.29577951 \dots \quad \frac{200^{\circ}}{\pi} = 63^{\circ}.6619772 \dots$$

Let d, g, c , respectively, denote the number of degrees, grades, and units of circular measure in an angle, then,

$$d = \frac{180}{\pi} c, \quad g = \frac{200}{\pi} c, \quad c = \frac{\pi}{180} d, \quad c = \frac{\pi}{200} g.$$

34. Origin, Termini and Situation of Arcs.

The origin of an arc is the extremity at which it begins.

The primary origin of arcs is at the right extremity of the primary diameter.

The secondary origin of arcs is at the upper extremity of the vertical diameter.

The terminus of an arc is the extremity at which it ends.

An arc is said to be situated in that quadrant in which its terminus is situated, thus:

The arc OT is in the first quadrant.

The arc OOT' is in the second quadrant.

The arc OPT'' is in the third quadrant.

The arc OPT''' is in the fourth quadrant.

35. Positive and Negative Arcs.

Positive arcs are those which are estimated in the direction contrary to that of the motion of the hands of a watch.

Negative arcs are those which are estimated in the same direction as that of the motion of the hands of a watch.

Thus, OT , OT' , OT'' , OT''' , estimated to the left are positive, and OT''' , OT'' , OT' , OT , estimated to the right, are negative.

36. The Complement of an Arc.

The complement of an arc or angle is 90° minus that arc or angle.

If the arc or angle is less than 90° , its complement is *positive*.

If the arc or angle is greater than 90° , its complement is *negative*.

The complement of an arc, geometrically considered, is the arc estimated from the terminus of the given arc to the secondary origin. Therefore, by the preceding article, the complement of an arc will be positive

or negative, according as the arc is less or greater than 90° .

TO' is the complement of OT , and is positive.

$T'O'$ is the complement of OT' , and is negative.

$T''O'$ is the complement of OT'' , and is negative.

$T'''O'$ is the complement of OT''' , and is negative.

37. The Supplement of an Arc.

The supplement of an arc or angle is 180° minus that arc or angle.

If the arc or angle is less than 180° , its supplement is *positive*.

If the arc or angle is greater than 180° , its supplement is *negative*.

The supplement of an arc, geometrically considered, is the arc estimated from the terminus of the given arc to the left-hand extremity of the primary diameter. Therefore, by article 35, the supplement of an arc will be positive or negative, according as the arc is less or greater than 180° .

TP is the supplement of OT , and is positive.

$T'P$ is the supplement of OT' , and is positive.

$T''P$ is the supplement of OT'' , and is negative.

$T'''P$ is the supplement of OT''' , and is negative.

TRIGONOMETRICAL FUNCTIONS.

38. Preliminary Definitions and Remarks.

1. A function of a quantity is a quantity whose value depends on the given quantity.

2. The trigonometrical functions, called also *circular functions*, are auxiliary lines, which are functions of an arc or of the angle which has the same measure as that arc.

3. These functions are eight in number, and are called the *sin*, *cos*, *versine*, *cot-versed-sine*, *tangent*, *cot*, *secant* and *cosecant*, which are abbreviated thus, *sin*, *cos*, *vers*, *cotvers*, *tan*, *cot*, *sec*, *cosec*.

4. The solution of triangles is accomplished by the use of these functions, since they enable us to ascertain the relations which exist between the sides and angles of triangles.

5. The primary origin will be taken as the common origin of the arcs, unless the contrary is stated.

6. The origin of any arc, wherever situated, may be considered the primary origin of that arc; and its secondary origin is a quadrant's distance from the primary origin, in the direction of the positive or negative arc, according as the given arc is positive or negative.

7. An arc will be considered positive unless the contrary is stated.

8. The primary diameter passes through the primary origin; and the secondary diameter, through the secondary origin.

9. Lines estimated upward, toward the right, or from the center toward the terminus of the arc, are considered positive.

10. Lines estimated downward, toward the left, or from the center and the terminus of the arc, are considered negative.

11. The limiting values of the circular functions are their values for the arcs 0° , 90° , 180° , 270° , 360° .

12. The sign of a varying quantity, up to a limit is its sign at the limit.

13. Point out positive arcs in the following diagram, and the origin and terminus of each.

14. Point out negative arcs, the origin, terminus and primary diameter of each.

15. Point out the positive lines, also the negative.

39. The Sine of an Arc.

The **sine** of an arc is the perpendicular distance of its terminus from the primary diameter.

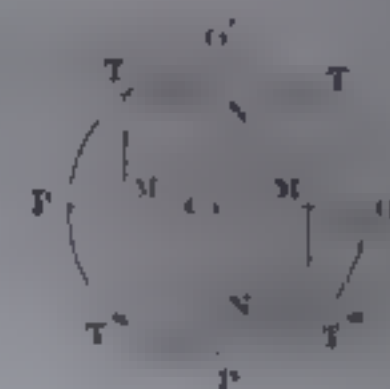
MT is the sine of the arc OT .

$M'T'$ is the sine of the arc OT' .

$M'T''$ is the sine of the arc OT'' .

MT''' is the sine of the arc OT''' .

By the arcs OT'' and OT''' , we are to understand the *positive* arcs, and not the negative arcs designated by the same letters.



The sine of an arc is the sine of the angle measured by that arc.

Thus, MT , the sine of the arc OT , is the sine of the angle OCT , which is measured by the arc OT ; and similarly for the other arcs and angles.

The arcs OT and OT' are in the first and second quadrants, respectively, and their sines MT and $M'T'$ are estimated upward, and are therefore *positive*; hence,

The sine of an arc in the first or second quadrant is positive.

The arcs OT'' and OT''' are in the third and fourth quadrants, respectively, and their sines, $M'T''$ and MT''' , are estimated downward, and are therefore *negative*; hence,

The sine of an arc in the third or fourth quadrant is negative.

Let the chord TT' be parallel to the primary diameter OP , then will $M'T'$ be equal to MT , and the arc OT will be equal to the arc $T'P$; but the arc $T'P$ is the supplement of the arc OT' ; therefore, the arc OT is the supplement of the arc OT' ; but $M'T'$,

the sine of the arc OT , is equal to MT , the sine of the arc OT , the supplement of OT' ; hence,

The sine of an arc is equal to the sine of its supplement.

The sine of 0° is 0. As the arc increases from 0° to 90° , the sine increases from 0 to $+1$. As the arc increases from 90° to 180° , the sine decreases from $+1$ to 0. As the arc increases from 180° to 270° , the sine passes through 0, changes its sign from $+$ to $-$, and increases numerically, but decreases algebraically from 0 to -1 . As the arc increases from 270° to 360° , the sine decreases numerically, but increases algebraically from -1 to -0 .

Hence, for the limiting values of the sine, we have

$$\begin{aligned} \sin 0^\circ &= 0, & \sin 90^\circ &= +1, & \sin 180^\circ &= +0, \\ \sin 270^\circ &= -1, & \sin 360^\circ &= -0. \end{aligned}$$

40. The Co-sine of an Arc.

The co-sine of an arc is the perpendicular distance of its terminus from the secondary diameter.

NT is the co-sine of the arc OT .
 NT' is the co-sine of the arc OT' .
 $N'T''$ is the co-sine of the arc OT'' .
 $N'T'''$ is the co-sine of the arc OT''' .
 The arcs OT and OT''' are in the first and fourth quadrants, respectively, and their co-sines NT and $N'T'''$ are estimated toward the right, and are therefore positive; hence,

The co-sine of an arc in the first or fourth quadrant is positive.

The arcs OT' and OT'' are in the second and third quadrants, respectively, and their co-sines, NT' and $N'T''$, are estimated toward the left, and are therefore negative; hence,

The co-sine of an arc in the second or third quadrant is negative.

The word *co-sine* is an abbreviation of *complementi sinus*, the sine of the complement. In fact, NT , the co-sine of OT , is the sine of OT' , the complement of OT ; hence,

The co-sine of an arc is the sine of its complement.

MT , the sine of OT , is the co-sine of OT' , the complement of OT ; hence,

The sine of an arc is the co-sine of its complement.

Since the radius CO is perpendicular to the chord TT' , NT and NT' are numerically equal; but since NT is estimated toward the right, and NT' toward the left, they have contrary signs; hence, $NT = -NT'$; but NT is the co-sine of OT , and NT' is the co-sine of OT' , the supplement of OT ; hence,

The co-sine of an arc is equal to minus the co-sine of its supplement.

It is evident that CN is equal to the sine of OT , or of OT' , and that CN' is equal to the sine of OT'' , or of OT''' ; hence,

The sine of an arc is equal to that part of the secondary diameter from the center to the foot of the co-sine.

It is evident that CM is equal to the co-sine of OT , or of OT''' , and that CM' is equal to the co-sine of OT' or of OT'' ; hence,

The co-sine of an arc is equal to that part of the primary diameter from the center to the foot of the sine.

The co-sine of 0° is $+1$. As the arc increases from 0° to 90° , the co-sine decreases from $+1$ to $+0$. As the arc increases from 90° to 180° , the co-sine passes through 0, changes its sign from $+$ to $-$, and increases numerically, but decreases algebraically from 0 to -1 .

As the arc increases from 180° to 270° , the co-sine decreases numerically, but increases algebraically

from -1 to $+1$. As θ increases from 270° to 360° , the cosine passes through 0, changes its sign from $-$ to $+$, and increases from -1 to $+1$.

Hence, for the limiting values of the co-sine, we have

$\cos 0^\circ = 1,$	$\cos 90^\circ = 0,$	$\cos 180^\circ = -1,$
$\cos 270^\circ = 0,$	$\cos 360^\circ = 1.$	

41. The Versed-Sine of an Arc.

The versed-sine of an arc is the perpendicular distance of the primary origin from the sine.

Mo is the versed-sine of the arc OT , and of the arc OT''' .

$W'D$ is the versed-sine of the arc OT' , and of the arc OT'' .

The versed-sine of an arc, in any quadrant, is estimated to the *right*, and is therefore positive; hence,

The resistance is always positive

The versed-sine of 0° is 0. As the arc increases from 0° to 90° , the versed-sine increases from 0 to +1. As the arc increases from 90° to 180° , the versed-sine increases from +1 to +2. As the arc increases from 180° to 270° , the versed-sine decreases from +2 to +1. As the arc increases from 270° to 360° , the versed-sine decreases from +1 to +0.

Hence, the limiting values of the versed-sine are
 $\text{vers } 0^\circ = 0,$ $\text{vers } 90^\circ = +1,$ $\text{vers } 180^\circ = +2,$
 $\text{vers } 270^\circ = +1,$ $\text{vers } 360^\circ = +0.$

What are the least and greatest values of the sine, and what are the corresponding arcs?

What are the least and greatest values of the cosine, and what are the corresponding arcs?

What are the least and greatest values of the versed-sine, and what are the corresponding arcs?



42. The Co-versed-sine of an Arc.

The co-versed-sine of an arc is the perpendicular distance of the secondary origin from the co-sine.

Thus, see diagram of the last article, NO is the co-versed-sine of the arc OT , and of the arc OT' ; $N'O$ is the co-versed-sine of the arc OT'' , and of the arc OT''' .

The co-versed-sine of an arc in any quadrant is estimated upwards, and is therefore *positive*; hence,

The co-versed-sine is always positive.

The word *co-versed-sine* is an abbreviation of *complementi versatus sinus*, the *versed* or *turned* sine of the complement. In fact, NO' , the co-versed-sine of OT , is the versed sine of OT' , the complement of OT ; hence,

The co-versed-sine of an arc is the versed-sine of its complement.

MO , the versed-sine of OT , is the co-versed-sine of OT , the complement of OT ; hence,

The versed-sine of an arc is the co-versed-sine of its complement.

The co-versed-sine of 0° is 1. As the arc increases from 0° to 90° , the co-versed-sine decreases from $+1$ to $+0$. As the arc increases from 90° to 180° , the co-versed-sine increases from $+0$ to $+1$. As the arc increases from 180° to 270° , the co-versed-sine increases from $+1$ to $+2$. As the arc increases from 270° to 360° , the co-versed-sine decreases from $+2$ to $+1$. Hence, the limiting values of the co-versed-sine are, covers $0^\circ = +1$, covers $90^\circ = +0$, covers $180^\circ = +1$, covers $270^\circ = +2$, covers $360^\circ = +1$.

What are the least and greatest values of the co-versed sine, and what are the corresponding arcs?

Trace the arcs from 0° to 360° , and the changing functions.

43. The Tangent of an Arc.

The tangent of an arc is the perpendicular to the primary diameter, produced from the primary origin, till it meets the prolongation of the diameter through the terminus of the arc.

OR is the tangent of the arcs OT and OT'' .

OR' is the tangent of the arcs OT' and OT''' .

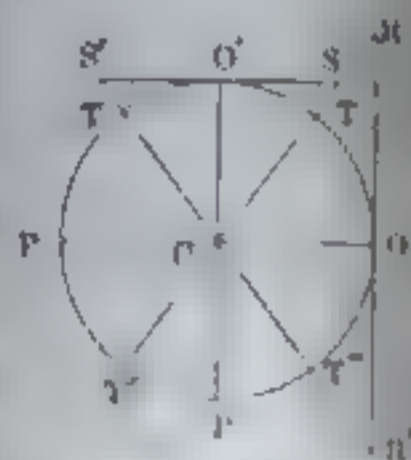
The arcs OT and OT'' are in the first and third quadrants, respectively, and their tangent, OR , is estimated upward, and is therefore positive; hence,

The tangent of an arc in the first or third quadrant is positive.

The arcs OT' and OT''' are in the second and fourth quadrants, respectively, and their tangent, OR' , is estimated downward, and is therefore negative; hence,

The tangent of an arc in the second or fourth quadrant is negative.

Let the arc OT be equal to the arc $T'P$. Then, since $T'P$ is the supplement of OT' , OT will be the supplement of OT' ; but the arc $T'''O$ is the supplement of OT' ; hence, $OT = T'''O$, and the angle OCR is equal to the angle OCR' . The angle OCR is equal to the angle OCR' , since each is a right angle. Hence, the two triangles OCR and OCR' have two angles, and the included side of the one equal to two angles and the included side of the other, each to each, and are therefore equal in all their parts. Hence, OR , opposite the angle OCR , is equal to OR' , opposite the equal angle OCR' . Since OR is estimated upward, and OR' downward, they have contrary signs; hence, $OR = -OR'$. But OR is the tangent



of the arc OT , and OR' is the tangent of the arc OT' , the supplement of OT ; hence,

The tangent of an arc is equal to minus the tangent of its supplement.

The tangent of 0° is 0. As the arc increases from 0° to 90° , the tangent increases from 0 to $+\infty$. As the arc increases from 90° to 180° , the tangent passes through ∞ , changes its sign from $+$ to $-$, and decreases numerically, but increases algebraically from $-\infty$ to -0 . As the arc increases from 180° to 270° , the tangent passes through 0, changes its sign from $-$ to $+$, and increases from -0 to $+\infty$. As the arc increases from 270° to 360° , the tangent passes through ∞ , changes its sign from $+$ to $-$, and decreases numerically, but increases algebraically from $-\infty$ to -0 . Hence, for the limiting values of the tangent we have

$$\begin{aligned} \tan 0^\circ &= 0, & \tan 90^\circ &= +\infty, & \tan 180^\circ &= -0, \\ \tan 270^\circ &= +\infty, & \tan 360^\circ &= -0. \end{aligned}$$

44. The Co-tangent of an Arc.

The co-tangent of an arc is the perpendicular to the secondary diameter, produced from the secondary origin, till it meets the prolongation of the diameter through the terminus of the arc.

OS is the co-tangent of OT and OT'' .

OS' is the co-tangent of OT' and OT''' .

The arcs OT and OT'' are in the first and third quadrants, respectively, and their co-tangent, OS , is estimated to the right, and is therefore positive; hence,

The co-tangent of an arc in the first or third quadrant is positive.

The arcs OT' and OT''' are in the second and fourth quadrants, respectively, and their co-tangent, OS' , is estimated to the left, and is therefore negative; hence,

The *co-tangent* of an arc in the second or fourth quadrant is *negative*.

The word *co-tangent* is an abbreviation of *complementi tangenti*, the tangent of the complement. In fact, OS , the co-tangent of OT , is the tangent of OT' , the complement of OT ; hence,

The co-tangent of an arc is the tangent of its complement.

OK , the tangent of OT , is the co-tangent of OT' , the complement of OT ; hence,

The tangent of an arc is the co-tangent of its complement.

Let the arcs OT and $T'P$ be equal. Then, since $T'P$ is the supplement of OT' , OT will be the supplement of OT' .

The arcs OT and OT' are equal, since they are complements of the equal arcs OT and $T'P$; hence, the angles OCT and OCT' , measured by these equal arcs, are equal. The angles $CO'S$ and $CO'S'$ are equal, since each is a right angle. Hence, the two triangles $CO'S$ and $CO'S'$ have the common side CO , and the two adjacent angles equal, and are therefore equal in all their parts; and OS , opposite the angle OCS , is equal to OS' , opposite the equal angle OCS' .

Since OS is estimated to the right, and OS' to the left, they have contrary signs; hence, $OS = -OS'$. But OS is the co-tangent of OT , and OS' is the co-tangent of OT' , the supplement of OT ; hence,

The co-tangent of an arc is equal to minus the co-tangent of its complement.

The co-tangent of 0° is $+\infty$. As the arc increases from 0° to 90° , the co-tangent decreases from $+\infty$ to $+0$. As the arc increases from 90° to 180° , the co-tangent passes through 0, changes its sign from $+$ to $-$, and increases numerically, but decreases algebraically from -0 to $-\infty$. As the arc increases from 180° to 270° , the co-tangent passes through ∞ , changes

its sign from $-$ to $+$, and decreases from $+\infty$ to $+0$. As the arc increases from 270° to 360° , the co-tangent passes through 0, changes its sign from $+$ to $-$, and increases numerically, but decreases algebraically from 0 to $-\infty$.

Hence, the limiting values of the co-tangent are
 $\cot 0^\circ = +\infty$, $\cot 90^\circ = +0$, $\cot 180^\circ = -\infty$,
 $\cot 270^\circ = +0$, $\cot 360^\circ = -\infty$.

45. The Secant of an Arc.

The *secant* of an arc is the line drawn from the center of the circle to the terminus of the tangent.

CR is the secant of OT and OT'' .

CR' is the secant of OT' and OT''' .

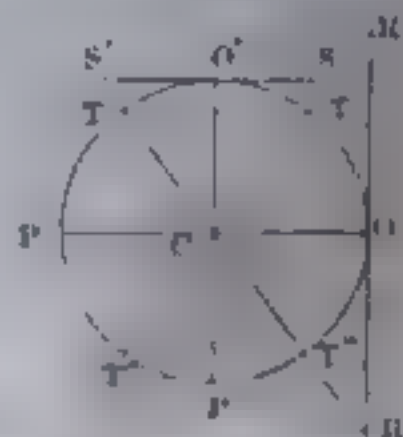
The arcs OT and OT''' are in the first and fourth quadrants, respectively, and their secants, CR and CR' are estimated from the center toward the termini of the arcs, and are therefore positive; hence,

The secant of an arc in the first or fourth quadrant is positive.

The arcs OT' and OT'' are in the second and third quadrants, respectively, and their secants, CR' and CR , are estimated from the center, from the termini of the arcs, and are therefore negative; hence,

The secant of an arc in the second or third quadrant is negative.

Let the arcs OT and $T'P$ be equal. Then, since $T'P$ is the supplement of OT' , OT is the supplement of OT' ; but $T''O$ is the supplement of OT' ; therefore, $T''O$ is equal to OT , and the angle $T''CO$, measured by $T''O$, is equal to the angle OCT , measured by the equal arc OT . The right angles COR and $CO'R'$ are



equal. Hence, in the triangles having the common side CO , and the two adjacent angles equal, CR is equal to CR' . But CR , the secant of OT , is positive; and CR' , the secant of OT' , the supplement of OT , is negative, hence, $CR = -CR'$; hence,

The secant of an arc is equal to minus the secant of its complement.

The secant of 0° is $+1$. As the arc increases from 0° to 90° , the secant increases from $+1$ to $+\infty$. As the arc increases from 90° to 180° , the secant passes through ∞ , changes its sign from $+$ to $-$, and decreases numerically, but increases algebraically from ∞ to -1 . As the arc increases from 180° to 270° , the secant increases numerically, but decreases algebraically from -1 to $-\infty$. As the arc increases from 270° to 360° , the secant passes through ∞ , changes its sign from $-$ to $+$, and decreases from $+\infty$ to $+1$. Hence, for the limiting values of the secant we have
 $\sec 0^\circ = +1$, $\sec 90^\circ = +\infty$, $\sec 180^\circ = -1$,
 $\sec 270^\circ = -\infty$, $\sec 360^\circ = +1$.

46. The Co-secant of an Arc.

The co-secant of an arc is the line drawn from the center of the circle to the terminus of the co-tangent.

CS is the co-secant of OT and OT'' .

CS' is the co-secant of OT' and OT''' .

The arcs OT and OT' are in the first and second quadrants, respectively, and their co-secants CS and CS' are estimated from the center toward the termini of the arcs, and are therefore positive; hence,

The co-secant of an arc in the first or second quadrant is positive.

The arcs OT'' and OT''' are in the third and fourth quadrants, respectively, and their co-secants, CS and CS' , are estimated from the center and the termini of the arcs, and are therefore negative; hence,

The co-secant of an arc in the third or fourth quadrant is negative.

The word co-secant is an abbreviation of *complementi secans*, the secant of the complement. In fact, CS , the co-secant of OT , is the secant of OT' , the complement of OT ; hence,

The co-secant of an arc is the secant of its complement.

CR , the secant of OT , is the co-secant of OT' , the complement of OT ; hence,

The secant of an arc is the co-secant of its complement.

Let the arcs OT and OT' be equal. Then, since OT' is the supplement of OT , OT will be the supplement of OT' , $OT = OT'$, since they are complements of equal arcs. Hence, the angle COO' , measured by the arc OT , is equal to the angle COO' , measured by the equal arc OT' . The right angles, COO and COO' , are equal.

Hence, in the triangles having the common side CO , and the two adjacent angles equal, CS is equal to CS' , but CS is the co-secant of OT , and positive, and CS' is the co-secant of OT' , and positive, hence,

The co-secant of an arc is equal to the co-secant of its complement.

The co-secant of 0° is $+\infty$. As the arc increases from 0° to 90° , the co-secant decreases from $+\infty$ to $+1$. As the arc increases from 90° to 180° , the co-secant increases from $+1$ to $+\infty$. As the arc increases from 180° to 270° , the co-secant passes through ∞ , changes its sign from $+$ to $-$, and decreases numerically, but increases algebraically from $-\infty$ to -1 . As the arc increases from 270° to 360° , the co-secant increases

numerically, but decreases algebraically from -1 to $-\infty$. Hence, the limiting values of the cosecant are $\text{cosec } 0^\circ = +\infty$, $\text{cosec } 90^\circ = 1$, $\text{cosec } 180^\circ = +\infty$, $\text{cosec } 270^\circ = -1$, $\text{cosec } 360^\circ = -\infty$.

To aid the memory, and for convenience of reference, we give the following tabular summaries:

47. Signs of the Circular Functions.

Functions.	1 st q.	2 ^d q.	3 ^d q.	4 th q.
sine	+	+	—	—
co-sine	+	—	—	+
versed sine.	+	+	+	+
co-versed sine.	+	+	+	+
tangent.	+	—	+	—
co-tangent.	+	—	+	—
secant.	+	—	—	+
cosecant.	+	+	—	—

48. Limiting Values of the Circular Functions.

0°	90°	180°	270°	360°
$\sin = +0$	$\sin = +1$	$\sin = +0$	$\sin = -1$	$\sin = -0$
$\cos = +1$	$\cos = +0$	$\cos = -1$	$\cos = -0$	$\cos = +1$
$\text{vsin} = +0$	$\text{vsin} = +1$	$\text{vsin} = +2$	$\text{vsin} = +1$	$\text{vsin} = 0$
$\text{cvs} = +1$	$\text{cvs} = +0$	$\text{cvs} = +1$	$\text{cvs} = +2$	$\text{cvs} = +1$
$\tan = +0$	$\tan = +\infty$	$\tan = -0$	$\tan = +\infty$	$\tan = -0$
$\cot = +\infty$	$\cot = +0$	$\cot = -\infty$	$\cot = +0$	$\cot = -\infty$
$\sec = +1$	$\sec = +\infty$	$\sec = -1$	$\sec = -\infty$	$\sec = +1$
$\text{cosec} = +\infty$	$\text{cosec} = +1$	$\text{cosec} = +\infty$	$\text{cosec} = -1$	$\text{cosec} = -\infty$

49. Problem.

To find any function of an angle to the radius R , in terms of the corresponding function of the same angle to the radius 1, and the reverse.

Let $\sin C_1$ denote $\sin C$ to the radius $CT=1$, and $\sin C_2$ denote $\sin C$ to the radius $CT'=R$.

From similar triangles,

$$CT : CT' :: MT : M'T',$$

$$\text{or } 1 : R :: \sin C_1 : \sin C_2.$$



$$\therefore (1) \sin C_2 = \sin C_1 \times R. \quad \therefore (2) \sin C_1 = \frac{\sin C_2}{R}.$$

Let formulas for other functions be deduced; hence,

1. Any function of an angle to the radius R is equal to the corresponding function of the same angle to the radius 1, multiplied by R .

2. Any function of an angle to the radius 1 is equal to the corresponding function of the same angle to the radius R , divided by R .

TABLE OF NATURAL FUNCTIONS.

50. Description of the Table.

This table gives, to the radius 1, the values of the sine, co-sine, tangent, and co-tangent, to five decimal places, for every $10'$ from 0° to 90° .

For sines and tangents, the degrees are given in the left column, and the minutes at the top.

For co-sines and co-tangents, the degrees are given in the right-hand column, and the minutes at the bottom.

51. Problem.

To find the natural sine, cosine, tangent, or co-tangent of a given arc or angle.

Let us find the natural sine of $35^{\circ} 42' 24''$.

The difference between the natural sines of $35^{\circ} 40'$ and $35^{\circ} 50'$, as given in the table, is .00236. Now $2' 24'' = 24$ of $10'$, which is found thus:

$$\begin{array}{r} 10 \quad 24 \\ | \quad .24 \end{array}$$

Then take Nat sin $35^{\circ} 40' = .58307$

Correction for $2' 24'' = .00236 \times .24 = .00057$

\therefore Nat sin $35^{\circ} 42' 24'' = .58364$

In case of co-sine or co-tangent, the correction must be subtracted, since, between 0° and 90° , the greater the angle, the less the co-sine and co-tangent.

52. Examples.

- 1 Find the natural sine of $75^{\circ} 45' 30''$.

Ans. .96927.

- 2 Find the natural co-sine of $15^{\circ} 36' 12''$.

Ans. .96315

- 3 Find the natural tangent of $43^{\circ} 33' 18''$.

Ans. .95079.

- 4 Find the natural co-tangent of $84^{\circ} 28' 30''$.

Ans. .09673.

53. Problem.

To find the angle corresponding to a given natural sine, cosine, tangent, or co-tangent.

- 1 Find the angle corresponding to the natural sine .50754

Looking in the table we find the angle $30^{\circ} 30'$.

2. Find the angle whose natural sine = .82468.

The next less sine, sin $55^{\circ} 30' = .82413$.

Difference 55

Difference corresponding to $10' = 164$

\therefore Correction $10' \times \frac{55}{164} = 3' 21''$.

\therefore Angle $55^{\circ} 30' + 3' 21'' = 55^{\circ} 33' 21''$.

In case of co-sine and co-tangent, the angular difference must be subtracted, since the greater the co-sine or co-tangent, the less the angle, for values between 0° and 90° .

54. Examples.

1. Find the angle whose sine is .75684.

Ans. $49^{\circ} 11' 13''$.

- 2 Find the angle whose co-sine is .67898.

Ans. $47^{\circ} 14' 10''$.

3. Find the angle whose tangent is 1.34567.

Ans. $53^{\circ} 22' 59''$.

4. Find the angle whose co-tangent is .98765.

Ans. $45^{\circ} 21' 22''$.

TABLE OF LOGARITHMIC FUNCTIONS.

55. Description of the Table.

The table of logarithmic functions gives to the radius 10,000,000,000 the logarithm of the sine, co-sine, tangent, and co-tangent, for every minute, from 0° to 90° .

The expression, *logarithmic sine, tangent, etc.*, is equivalent to the *logarithm of the sine, of the tangent, etc.*

For sines and tangents, the degrees are given at the top of the page, and the minutes in the left-hand column.

For co-sines and co-tangents, the degrees are given at the bottom of the page, and the minutes in the right-hand column.

The columns marked D 1" contain the difference for 1".

56. Problem.

Find the logarithmic sine of $48^\circ 25' 30''$.

$$\begin{array}{r} \log \sin 48^\circ 25' \quad 9.87390 \\ D \ 1'' \quad .19. \quad \therefore \text{Correc. for } 30'' \quad .19 \times 30 \quad 6 \\ \therefore \log \sin 48^\circ 25' 30'' \quad 9.87396 \end{array}$$

In case of co-sine or co-tangent, the correction must be subtracted, since between 0° and 90° , the greater the angle, the less the co-sine and co-tangent.

57. Examples.

1. Find the logarithmic sine of $75^\circ 35'$.
Ans. 9.98610.
2. Find the logarithmic sine of $25^\circ 40' 21''$.
Ans. 9.63673.
3. Find the logarithmic co-sine of $29^\circ 55' 55''$.
Ans. 9.93782.
4. Find the logarithmic tangent of $50^\circ 50' 50''$.
Ans. 10.08927.
5. Find the logarithmic co-tangent of $65^\circ 45' 30''$.
Ans. 9.65349.

58. Problem.

To find the angle corresponding to a given logarithmic sine, co-sine, tangent, or co-tangent.

Find the angle whose logarithmic sine 9.84567
For next less we have $\sin 44^\circ 30' \quad 9.84566$

$$\begin{array}{l} D \ 1'' = .21 \quad \therefore \text{Correc.} = 1'' \times \frac{1}{.21} = 5'', \quad .21)1.00(5. \\ \therefore \text{Angle} \quad 44^\circ 30' 05''. \end{array}$$

In case of co-sine and co-tangent, the correction for seconds must be subtracted, since the greater the co-sine or co-tangent, and consequently the greater the logarithm, the less the angle for values between 0° and 90° .

59. Examples.

1. Find the angle whose logarithmic sine is 9.98437.
Ans. $71^\circ 43' 17''$.
2. Find the angle whose logarithmic co-sine is 9.78456.
Ans. $52^\circ 29' 19''$.
3. Find the angle whose logarithmic tangent is 10.12346.
Ans. $53^\circ 02' 11''$.
4. Find the angle whose logarithmic co-tangent is 9.99999.
Ans. $45^\circ 00' 03''$.

60. Problem.

Given any natural function, to find the corresponding logarithmic function.

1st SOLUTION.

Find from the natural function the corresponding angle, then, from the angle, the corresponding logarithmic function.

2d SOLUTION.

Let α denote any arc or angle, $f(\alpha)$, any function of α to the radius 1, and $f(\alpha)_L$ the corresponding

fraction of a to the radius R . Then, by article 49 we have,

$$f(a)_R = f(a)_1 \times R.$$

Substituting the value of R in the second member,

$$f(a)_R = f(a)_1 \cdot 10,000,000,000.$$

$$\therefore \log f(a)_R = \log f(a)_1 + 10.$$

Hence, Add 10 to the logarithm of the natural function.

61. Examples.

1. Given nat. sin $a = .98457$, required a and log sin a .
Ans. $a = 79^\circ 55' 25''$, log sin $a = 9.99325$.

2. Given nat. cos $a = .63878$, required a and log cos a .
Ans. $a = 50^\circ 17' 52''$, log cos $a = 9.80536$.

3. Given nat. tan $a = 1.68685$, required a and log tan a .
Ans. $a = 59^\circ 20' 23''$, log tan $a = 10.22708$.

4. Given nat. cot $a = 1.41987$, required a and log cot a .
Ans. $a = 35^\circ 09' 24''$, log cot $a = 10.15225$.

62. Problem.

Given any logarithmic function, to find the corresponding natural function.

1st SOLUTION.

Find from the logarithmic function the corresponding angle: then, from the angle, the corresponding natural function.

2d SOLUTION.

From article 49 we have,

$$f(a)_1 = \frac{f(a)_R}{R}.$$

$$\therefore \log f(a)_1 = \log f(a)_R - 10.$$

Hence, Subtract 10 from the logarithmic function, and find the number corresponding to the resulting logarithm.

63. Examples.

1. Given log sin $a = 9.87654$, required a and nat. sin a .
Ans. $a = 48^\circ 48' 41''$, nat. sin $a = .75255$.

2. Given log cos $a = 9.84877$, required a and nat. cos a .
Ans. $a = 45^\circ 05' 41''$, nat. cos $a = .70595$.

3. Given log tan $a = 10.22708$, required a and nat. tan a .
Ans. $a = 59^\circ 20' 23''$, nat. tan $a = 1.68685$.

4. Given log cot $a = 10.15225$, required a and nat. cot a .
Ans. $a = 35^\circ 09' 24''$, nat. cot $a = 1.41987$.

RIGHT TRIANGLES.

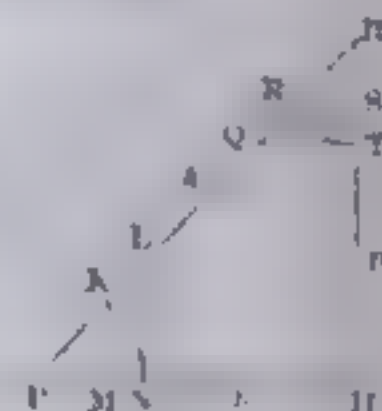
64. Principles.

$$PB : PK :: HB : MK,$$

$$\text{or } h : 1 :: p : \sin P.$$

$$BP : BR :: HP : SR,$$

$$\text{or } h : 1 :: b : \sin B.$$



$$\therefore (1) \left\{ \begin{array}{l} p = h \sin P, \\ b = h \sin B. \end{array} \right\} \therefore (2) \left\{ \begin{array}{l} \sin P = \frac{p}{h}, \\ \sin B = \frac{b}{h}. \end{array} \right\}$$

1. Either side adjacent to the right angle is equal to the sine of the opposite angle multiplied by the hypotenuse.

2. The sine of either acute angle is equal to the opposite side divided by the hypotenuse.

Since the angles P and B are complements of each other, $\sin P = \cos B$ and $\sin B = \cos P$; \therefore (1) and (2) become,

$$(3) \begin{cases} p = h \cos B, \\ b = h \cos P. \end{cases} \text{ and (4) } \begin{cases} \cos B = \frac{p}{h}, \\ \cos P = \frac{b}{h}. \end{cases}$$

3. *Either side adjacent to the right angle is equal to the cosine of the adjacent acute angle multiplied by the hypotenuse.*

4. *The cosine of either acute angle is equal to the adjacent side divided by the hypotenuse.*

$$PH : PN :: HB : NL, \text{ or } b : 1 :: p : \tan P.$$

$$BH : BT :: HP : TQ, \text{ or } p : 1 :: b : \tan B.$$

$$\therefore (5) \begin{cases} p = b \tan P, \\ b = p \tan B. \end{cases} \therefore (6) \begin{cases} \tan P = \frac{p}{b}, \\ \tan B = \frac{b}{p}. \end{cases}$$

5. *Either side adjacent to the right angle is equal to the tangent of the opposite angle multiplied by the other side.*

6. *The tangent of either acute angle is equal to the opposite side divided by the adjacent side.*

Since the angles P and B are complements of each other, $\tan P = \cot B$, and $\tan B = \cot P$; \therefore (5) and (6) become,

$$(7) \begin{cases} p = b \cot B, \\ b = p \cot P. \end{cases} \text{ and (8) } \begin{cases} \cot B = \frac{p}{b}, \\ \cot P = \frac{b}{p}. \end{cases}$$

7. *Either side adjacent to the right angle is equal to the co-tangent of the adjacent acute angle multiplied by the other side.*

8. *The co-tangent of either acute angle is equal to the adjacent side divided by the opposite side.*

$$BH : BT :: BP : BQ, \text{ or } p : 1 :: h : \sec B.$$

$$PH : PN :: PB : PL, \text{ or } b : 1 :: h : \sec P.$$

$$(9) \begin{cases} p = \frac{h}{\sec B}, \\ b = \frac{h}{\sec P}. \end{cases} \therefore (10) \begin{cases} \sec B = \frac{h}{p}, \\ \sec P = \frac{h}{b}. \end{cases}$$

9. *Either side adjacent to the right angle is equal to the hypotenuse divided by the secant of the adjacent acute angle.*

10. *The secant of either acute angle is equal to the hypotenuse divided by the adjacent side.*

Since the angles B and P are complements of each other, $\sec B = \operatorname{cosec} P$, $\sec P = \operatorname{cosec} B$; \therefore (9) and (10) become,

$$(11) \begin{cases} p = \frac{h}{\operatorname{cosec} P}, \\ b = \frac{h}{\operatorname{cosec} B}. \end{cases} \text{ and (12) } \begin{cases} \operatorname{cosec} P = \frac{h}{p}, \\ \operatorname{cosec} B = \frac{h}{b}. \end{cases}$$

11. *Either side adjacent to the right angle is equal to the hypotenuse divided by the cosecant of the angle opposite that side.*

12. *The cosecant of either acute angle is equal to the hypotenuse divided by the side opposite that angle.*

Scholium. By some authors, principles 2, 4, 6, 8, 10, and 12, have been given in the form of definitions.

Introducing radius into these formulas, by substituting for any function to the radius 1, the corresponding function to the radius R divided by R , and reducing, we have:

$$S : N ::$$

$$(1) \begin{cases} p = \frac{h \sin P}{R} \\ b = \frac{h \sin B}{R} \end{cases} \quad (2) \begin{cases} \sin P = \frac{Rp}{h} \\ \sin B = \frac{Rb}{h} \end{cases}$$

$$(3) \begin{cases} p = \frac{h \cos B}{R} \\ b = \frac{h \cos P}{R} \end{cases} \quad (4) \begin{cases} \cos B = \frac{Rp}{h} \\ \cos P = \frac{Rb}{h} \end{cases}$$

$$(5) \begin{cases} p = \frac{h \tan P}{R} \\ b = \frac{p \tan B}{R} \end{cases} \quad (6) \begin{cases} \tan P = \frac{Rp}{b} \\ \tan B = \frac{Rb}{p} \end{cases}$$

$$(7) \begin{cases} p = \frac{h \cot B}{R} \\ b = \frac{p \cot P}{R} \end{cases} \quad (8) \begin{cases} \cot B = \frac{Rp}{b} \\ \cot P = \frac{Rb}{p} \end{cases}$$

$$(9) \begin{cases} p = \frac{Rh}{\sec B} \\ b = \frac{Rh}{\sec P} \end{cases} \quad (10) \begin{cases} \sec B = \frac{Rp}{h} \\ \sec P = \frac{Rb}{h} \end{cases}$$

$$(11) \begin{cases} p = \frac{Rh}{\operatorname{cosec} P} \\ b = \frac{Rh}{\operatorname{cosec} B} \end{cases} \quad (12) \begin{cases} \operatorname{cosec} P = \frac{Rh}{p} \\ \operatorname{cosec} B = \frac{Rh}{b} \end{cases}$$

Applying logarithms to these formulas, we have.

$$(1) \begin{cases} \log p = \log h + \log \sin P - 10 \\ \log b = \log h + \log \sin B - 10. \end{cases}$$

$$(2) \begin{cases} \log \sin P = 10 + \log p - \log h \\ \log \sin B = 10 + \log b - \log h. \end{cases}$$

$$(3) \begin{cases} \log p = \log h + \log \cos B - 10 \\ \log b = \log h + \log \cos P - 10. \end{cases}$$

$$(4) \begin{cases} \log \cos B = 10 + \log p - \log h \\ \log \cos P = 10 + \log b - \log h. \end{cases}$$

$$(5) \begin{cases} \log p = \log b + \log \tan P - 10 \\ \log b = \log p + \log \tan B - 10. \end{cases}$$

$$(6) \begin{cases} \log \tan P = 10 + \log p - \log b \\ \log \tan B = 10 + \log b - \log p. \end{cases}$$

$$(7) \begin{cases} \log p = \log b + \log \cot B - 10 \\ \log b = \log p + \log \cot P - 10. \end{cases}$$

$$(8) \begin{cases} \log \cot B = 10 + \log p - \log b \\ \log \cot P = 10 + \log b - \log p. \end{cases}$$

$$(9) \begin{cases} \log p = 10 + \log h - \log \sec B \\ \log b = 10 + \log h - \log \sec P. \end{cases}$$

$$(10) \begin{cases} \log \sec B = 10 + \log h - \log p \\ \log \sec P = 10 + \log h - \log b. \end{cases}$$

$$(11) \begin{cases} \log p = 10 + \log h - \log \operatorname{cosec} P \\ \log b = 10 + \log h - \log \operatorname{cosec} B. \end{cases}$$

$$(12) \begin{cases} \log \operatorname{cosec} P = 10 + \log h - \log p \\ \log \operatorname{cosec} B = 10 + \log h - \log b. \end{cases}$$

65. Case I.

Given the hypotenuse and one acute angle, required the remaining parts.

$$1. \text{ Given } \begin{cases} h = 365, \\ P = 33^\circ 12'. \end{cases} \text{ Requir. } \begin{cases} B. \\ p. \\ b. \end{cases}$$

$$B = 56^\circ \quad P = 33^\circ 12' \quad 90^\circ - 33^\circ 12' = 56^\circ 48'$$

Either side adjacent to the right angle is equal to the sine of the opposite angle, multiplied by the hypotenuse

$$\therefore p = h \sin P.$$

Introducing radius, we have, $p = \frac{h \sin P}{R}$.

Applying logarithms, we have,

$$\begin{aligned} \log p &= \log h + \log \sin P - 10. \\ \log h (365) & 2.56229 \\ \log \sin P (33^\circ 12') & 9.73843 \\ \log p & = 2.30072 \therefore p = 199.85. \end{aligned}$$

In like manner, from either formula, $b = h \sin B$ or $b = h \cos P$, we find $b = 305.41$.

$$2. \text{ Given } \begin{cases} h = 73.26. \\ B = 49^\circ 12' 20''. \end{cases} \text{ Requir. } \begin{cases} P = 40^\circ 47' 10'' \\ b = 55.4625. \\ p = 47.8644. \end{cases}$$

$$3. \text{ Given } \begin{cases} h = 2195. \\ P = 27^\circ 38' 50''. \end{cases} \text{ Requir. } \begin{cases} B = 62^\circ 21' 10'' \\ p = 1018.512 \\ b = 1944.364. \end{cases}$$

66. Case II.

Given the hypotenuse and one side adjacent to the right angle, required the remaining parts.

$$1. \text{ Given } \begin{cases} h = 112 \\ p = 97. \end{cases} \text{ Required } \begin{cases} P. \\ B. \\ b. \end{cases}$$



The sine of either acute angle is equal to the opposite side divided by the hypotenuse.

$$\therefore \sin P = \frac{p}{h}.$$

Introducing radius, and multiplying by R , we have,

$$\sin P = \frac{Rp}{h}$$

Applying logarithms, we have,

$$\log \sin P = 10 + \log p - \log h.$$

$$\begin{aligned} \log p (97) & 1.98677 \\ \log h (112) & 2.04922 \\ \log \sin P & 9.93755 \therefore P = 60^\circ (or) 17''. \end{aligned}$$

$$B = 90^\circ - P = 90^\circ - 60^\circ (or) 17'' = 29^\circ 59' 43''.$$

$$b = h \sin B, \text{ or } b = h \cos P, \therefore b = 55.991.$$

We can also find b as follows:

$$b = \sqrt{h^2 - p^2} = \sqrt{(h+p)(h-p)}.$$

$$\log b = \frac{1}{2} [\log (h+p) + \log (h-p)].$$

$$2. \text{ Given } \begin{cases} h = 7269 \\ b = 3162 \end{cases} \text{ Required } \begin{cases} B = 25^\circ 47' 07''. \\ P = 64^\circ 12' 53''. \\ p = 6545. \end{cases}$$

$$3. \text{ Given } \begin{cases} h = 4114 \\ p = 159. \end{cases} \text{ Required } \begin{cases} P = 19^\circ 43' 36''. \\ B = 70^\circ 16' 24''. \\ b = 418.33. \end{cases}$$

67. Case III.

Given the side adjacent to the right angle and one acute angle, required the remaining parts.

$$1. \text{ Given } \begin{cases} h = 152.67 \\ P = 50^\circ 18' 32''. \end{cases} \text{ Requir. } \begin{cases} B. \\ p. \\ b. \end{cases}$$



$$B = 90^\circ - P = 90^\circ - 50^\circ 18' 32'' = 39^\circ 41' 28''.$$

Either side adjacent to the right angle is equal to the tangent of the opposite angle multiplied by the other side.

$$\therefore p = b \tan P.$$

Introducing radius and applying logarithms, as in the preceding cases, we find $p = 183.95$.

Either side adjacent to the right angle is equal to the cosine of the adjacent acute angle multiplied by the hypotenuse.

$$\therefore b = h \cos P; \therefore h = \frac{b}{\cos P}.$$

Introducing radius and applying logarithms, as above, we shall find $h = 239.05$.

2. Given $\begin{cases} p = 3963.35 \text{ miles} = \text{the earth's radius,} \\ P = 57' 2.3'' = \text{the moon's horizontal parallax} \end{cases}$

Required h , the distance of the moon from the earth.

$$\text{Ans. } h = 238889 \text{ miles.}$$

3. Given $\begin{cases} p = 3963.35 \text{ miles} = \text{the earth's radius,} \\ P = 8.9'' = \text{the sun's horizontal parallax.} \end{cases}$

Required h , the distance of the sun from the earth.

$$\text{Ans. } h = 91852000 \text{ miles.}$$

$$\text{Scholium. } \sin 8.9'' = \sin 1' \times \frac{8.9}{60}.$$

$$\therefore \log \sin 8.9'' = \log \sin 1' + \log 8.9 + \text{a.c. log } 60 = 10.$$

68. Case IV.

Given the two sides adjacent to the right angle, required the remaining parts.

1. Given $\begin{cases} p = 29.37. \\ b = 37.29. \end{cases}$ Requir. $\begin{cases} P. \\ B. \\ h. \end{cases}$



The tangent of either acute angle is equal to the opposite side divided by the adjacent side.

$$\therefore \tan P = \frac{p}{b}.$$

Introducing radius and applying logarithms, we shall find that $P = 38^\circ 13' 28''$.

$$B = 90^\circ - P = 90^\circ - 38^\circ 13' 28'' = 51^\circ 46' 32''.$$

Either side adjacent to the right angle is equal to the sine of the opposite angle multiplied by the hypotenuse.

$$\therefore p = h \sin P. \therefore h = \frac{p}{\sin P}.$$

Introducing radius and applying logarithms, we find $h = 47.468$.

2. Given $\begin{cases} p = 694.73. \\ b = 8372.1. \end{cases}$ Required $\begin{cases} P = 4^\circ 41' 37''. \\ B = 85^\circ 15' 23''. \\ h = 8401. \end{cases}$

3. Given $\begin{cases} p = 101. \\ b = 101. \end{cases}$ Required $\begin{cases} P = 44^\circ 26' 17''. \\ B = 45^\circ 33' 43''. \\ h = 144.253. \end{cases}$

4. Given $\begin{cases} p = 1728. \\ b = 1575. \end{cases}$ Required $\begin{cases} P = 47^\circ 39' 07''. \\ B = 42^\circ 20' 53''. \\ h = 2338.1. \end{cases}$

OBLIQUE TRIANGLES.

69. Case I.

Given one side and two angles, required the remaining parts.

Let ABC be an oblique triangle, and let the sides opposite the angles A , B , and C be denoted respectively by a , b and c .



Let the angles A and B and the side a be given, and the angle C and the sides b and c be required.

We find C from the formula,

$$C = 180^\circ - (A + B).$$

Draw the perpendicular p from the vertex C to the side c , thus forming two right triangles. There are two cases:

1st. When the perpendicular falls on the side c .

From the principles of the right triangle we have,

$$p = b \sin A \text{ and } p = a \sin B.$$

$$\therefore b \sin A = a \sin B.$$

$$\therefore (1) \sin A : \sin B :: a : b.$$

2d. When the perpendicular falls on c produced.

$$p = b \sin A \text{ and } p = a \sin CBD.$$

But CBD is the supplement of CBA , or B of the triangle. Since the sine of an angle is equal to the sine of its supplement,

$$\sin CBD = \sin B; \therefore p = a \sin B.$$

$$\therefore b \sin A = a \sin B.$$

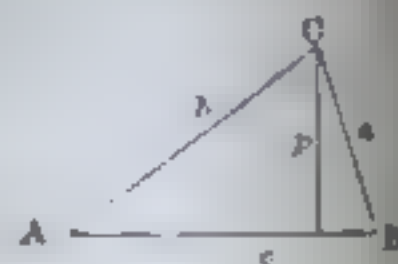
$$\therefore (1) \sin A : \sin B :: a : b.$$

In like manner we may find,

$$(2) \sin A : \sin C :: a : c.$$

Hence, *The sine of the angle opposite the given side is to the sine of the angle opposite the required side as the given side is to the required side.*

Introducing radius by substituting for the function to the radius 1, the corresponding function to the



radius R divided by R , and reducing, the proportions (1) and (2) will be of the same form as before substitution, and hence are true for any radius.

From proportions (1) and (2), we find,

$$(3) \quad b = \frac{a \sin B}{\sin A}, \quad (4) \quad c = \frac{a \sin C}{\sin A}.$$

Applying logarithms to (3) and (4), we have,

$$(5) \quad \log b = \log a + \log \sin B + a. c. \log \sin A - 10.$$

$$(6) \quad \log c = \log a + \log \sin C + a. c. \log \sin A - 10.$$

70. Examples.

$$1. \text{ Given } \begin{cases} A = 35^\circ 45', \\ B = 15^\circ 28', \\ a = 7985. \end{cases} \quad \text{Req. } \begin{cases} C, \\ b, \\ c. \end{cases}$$



$$C = 180^\circ - (A + B) = 180^\circ - 81^\circ 13' = 98^\circ 47'.$$

Since the sine of the angle opposite the given side is to the sine of the angle opposite the required side as the given side is to the required side, we have the proportion,

$$\sin A : \sin B :: a : b, \therefore b = \frac{a \sin B}{\sin A}.$$

$$\therefore \log b = \log a + \log \sin B + a. c. \log \sin A - 10.$$

$$\log a (7985) = 3.90227$$

$$\log \sin B (45^\circ 28') = 9.85299$$

$$a. c. \log \sin A (35^\circ 45') = 0.23340$$

$$\log b = 3.98866 \therefore b = 9742.25.$$

In like manner we have the proportion,

$$\sin A : \sin C :: a : c, \therefore c = \frac{a \sin C}{\sin A}.$$

$$\therefore \log c = \log a + \log \sin C + a. c. \log \sin A = 10$$

$$\log a (7985) \quad 3.90227$$

$$\log \sin C (98^\circ 47') \quad 9.99488$$

$$a. c. \log \sin A (35^\circ 45') = 0.23340$$

$$\log c \quad 4.13055 \quad \therefore c = 13506.88.$$

In finding $\log \sin 98^\circ 47'$, take the supplement of $98^\circ 47'$, which is $81^\circ 13'$, and find $\log \sin 81^\circ 13'$.

$$2. \text{ Given } \begin{cases} A = 50^\circ 30' 40'' \\ B = 70^\circ 45' 30'' \\ a = 478.35 \text{ yd.} \end{cases} \text{ Req. } \begin{cases} C = 58^\circ 43' 50'' \\ b = 585.2 \text{ yd.} \\ c = 529.8 \text{ yd.} \end{cases}$$

$$3. \text{ Given } \begin{cases} B = 65^\circ 25' 35'' \\ C = 60^\circ 28' 34'' \\ b = 12.25 \text{ miles.} \end{cases} \text{ Req. } \begin{cases} A = 54^\circ 05' 51'' \\ c = 11.72 \text{ miles} \\ a = 10.91 \text{ miles} \end{cases}$$

71. Case II.

Given two sides and an angle opposite one of them, required the remaining parts.

1. WHEN THE GIVEN ANGLE IS ACUTE.

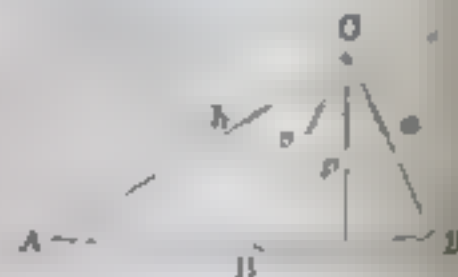
Let the sides a and b and the angle A be given, and the remaining parts be required.

Let the perpendicular p be drawn from C to the opposite side. Then we shall have,

$$p = b \sin A.$$

1st. If $a > p$ and $a < b$, there will be two solutions.

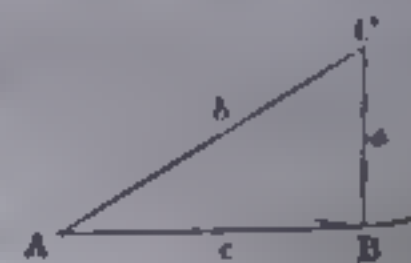
For, if with C as a center and a as radius a circumference be described, it will intersect the side opposite C in two points, B and B' , and either triangle, ABC or $AB'C$ will fulfill the conditions of the problem, since



it will have two sides and an angle opposite one of them the same as those given. Hence, there will be two solutions if a has any value between the limits p and b .

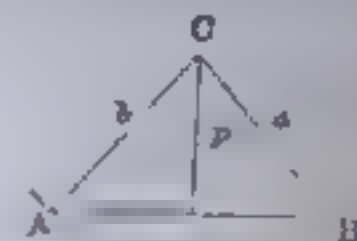
2d. If $a = p$, there will be but one solution.

For, as a diminishes and approaches p , the two points B and B' approach; and if $a = p$, B and B' will unite, the arc will be tangent to c , and the two triangles will become one, and there will be one solution.



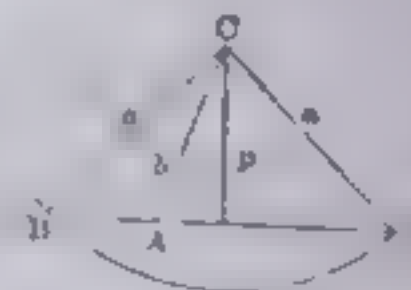
3d. If $a = b$, there will be but one solution.

For, as a increases and approaches b , the points B and B' separate, the triangle ABC increases, and the triangle $AB'C$ decreases; and when a becomes equal to b , the triangle $AB'C$ vanishes, and there remains but one triangle, or there is but one solution.



4th. If $a > b$, there will be but one solution.

For, although there are two triangles ABC and $AB'C$, the latter is excluded by the condition that the given angle A is acute, since CAB' is obtuse, and there remains but one triangle ABC which satisfies the conditions, or there is but one solution.



5th. If $a < p$, there will be no solution.

For the arc described with C as center and a as radius will neither intersect the opposite side nor be tangent to it. The triangle can not be constructed, or there will be no solution.



2. WHEN THE GIVEN ANGLE IS OBTUSE.

1st. If $a > b$ there will be but one solution.

For, although there are two triangles ABC and $AB'C$, the latter is excluded by the conditions of the problem, since the angle CAB' is acute while the given angle is obtuse. There remains but one triangle, ABC , which satisfies all the conditions of the problem, or there is but one possible solution.



2d. If $a = b$ there will be no solution.

For as a diminishes and approaches b , B will approach A ; and when a becomes equal to b , B will unite with A , and the triangle ABC will vanish. The triangle $AB'C$ will remain, but will be excluded by the conditions of the problem, since the angle CAB' is acute while the given angle is obtuse.

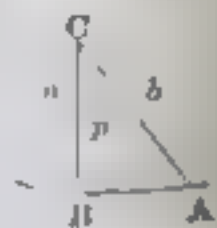


3d. If $a < b$ there will be no solution. For then,

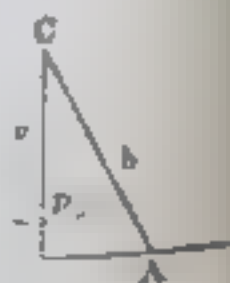
If $a > p$ there will be two triangles, ABC and $AB'C$, but both are excluded by the condition that the given angle is obtuse.



If $a = p$ the two triangles reduce to one, right-angled at B , which is excluded by the condition that the given angle is obtuse.



If $a < p$ no triangle can be constructed with the given parts, and there will be no solution.



72. Summary of Results.

1. When $A < 90^\circ$.

Two Solutions, If $a > p$ and $a < b$.

One Solution, $\begin{cases} 1st. \text{ If } a = p. \\ 2d. \text{ If } a = b. \\ 3d. \text{ If } a > b. \end{cases}$

No Solution, If $a < p$

2. When $A > 90^\circ$.

One Solution, If $a > b$.

No Solution, $\begin{cases} 1st. \text{ If } a = b. \\ 2d. \text{ If } a < b. \end{cases}$

73. Method of Computation.

Reversing the order of the couplets of the proportion in Case I, we have

$$1) \quad a : b :: \sin A : \sin B$$

Hence, *The side opposite the given angle is to the side opposite the compared angle, as the sine of the given angle is to the sine of the required angle.*

$$(1) \text{ gives } \sin B = \frac{b \sin A}{a}$$

$$\therefore (3) \quad \log \sin B = \log b + \log \sin A + a. c. \log a - 10.$$

If there is but one solution, take from the table the angle B corresponding to $\log \sin B$. if there are two solutions, take B and its supplement B' , for both correspond to $\log \sin B$.

We find C from the formula,

$$C = 180^\circ - (A + B) \text{ or } C = 180^\circ - (A + B').$$

We find c from the proportion,

$$\sin A : \sin C :: a : c, \therefore c = \frac{a \sin C}{\sin A}.$$

$$\therefore \log c = \log a + \log \sin C + a. c. \log \sin A - 10$$

74. Examples.

1. Given $\left\{ \begin{array}{l} a = 9.25. \\ b = 12.56. \\ A = 30^\circ 25'. \end{array} \right\}$ Req. $\left\{ \begin{array}{l} B. \\ C. \\ c. \end{array} \right.$



$$p = b \sin A.$$

Introducing R and applying logarithms, we have

$$\log p = \log b + \log \sin A - 10.$$

$$\begin{array}{rcl} \log b (12.56) & = & 1.09899 \\ \log \sin A (30^\circ 25') & = & 9.70439 \\ \log p & = & 0.80338 \therefore p = 6.3589. \end{array}$$

Since $a > p$ and $a < b$, there are two solutions.

Since the side opposite the given angle is to the side opposite the required angle as the sine of the given angle is to the sine of the required angle, we have the proportion,

$$a : b :: \sin A : \sin B, \therefore \sin B = \frac{b \sin A}{a}.$$

$$\log \sin B = \log b + \log \sin A + a. c. \log a - 10.$$

$$\begin{array}{rcl} \log b (12.56) & = & 1.09899 \\ \log \sin A (30^\circ 25') & = & 9.70439 \\ a. c. \log a (9.25) & = & 9.03386 \\ \log \sin B & = & 9.83724 \therefore \left\{ \begin{array}{l} B = 43^\circ 25' 41''. \\ B = 136^\circ 34' 19''. \end{array} \right. \end{array}$$

$$C = 180^\circ - (A + B) = 106^\circ 9' 19'',$$

$$C' = 180^\circ - (A + B') = 13^\circ 0' 41''.$$

$$\sin A : \sin C :: a : c, \therefore c = \frac{a \sin C}{\sin A}.$$

$$\log c = \log a + \log \sin C + a. c. \log \sin A - 10.$$

Taking the value of C , we have,

$$\begin{array}{rcl} \log a (9.25) & = & 0.96614 \\ \log \sin C (106^\circ 9' 19'') & = & 9.98250 \\ a. c. \log \sin A (30^\circ 25') & = & 0.29561 \\ \log c & = & 1.24425 \therefore c = 17.549. \end{array}$$

Taking the value of C' , we have,

$$\begin{array}{rcl} \log a (9.25) & = & 0.96614 \\ \log \sin C' (13^\circ 0' 41'') & = & 9.5246 \\ a. c. \log \sin A (30^\circ 25') & = & 0.29561 \\ \log c & = & 0.61121 \therefore c = 4.1135. \end{array}$$

2. Given $\left\{ \begin{array}{l} a = 20.25. \\ b = 20.25. \\ A = 72^\circ 35' 27''. \end{array} \right\}$ Req. $\left\{ \begin{array}{l} B = 72^\circ 35' 27''. \\ C = 74^\circ 49' 06''. \\ c = 24.725. \end{array} \right.$

3. Given $\left\{ \begin{array}{l} a = 645.8. \\ b = 234.5. \\ A = 48^\circ 35'. \end{array} \right\}$ Req. $\left\{ \begin{array}{l} B = 15^\circ 48' 04''. \\ C = 115^\circ 36' 56''. \\ c = 776.33. \end{array} \right.$

4. Given $\left\{ \begin{array}{l} a = 17. \\ b = 10.25. \\ A = 27^\circ 43' 15''. \end{array} \right\}$ Req. $\left\{ \begin{array}{l} B \\ C \\ c \end{array} \right\}$ No Solution.

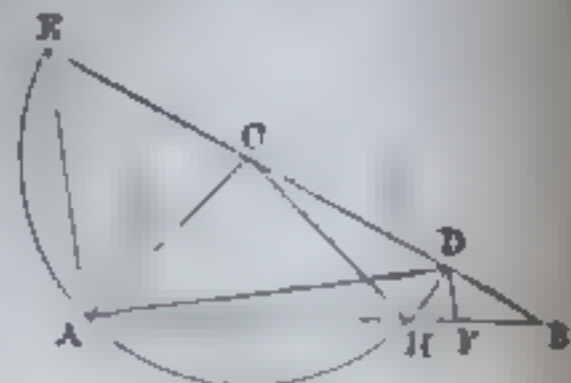
5. Given $\left\{ \begin{array}{l} a = 94.26. \\ b = 126.72. \\ A = 27^\circ 50'. \end{array} \right\}$ Req. $\left\{ \begin{array}{l} B = \left\{ \begin{array}{l} 38^\circ 52' 46''. \\ 141^\circ 7' 14''. \end{array} \right. \\ C = \left\{ \begin{array}{l} 113^\circ 17' 14''. \\ 11^\circ 2' 46''. \end{array} \right. \\ c = \left\{ \begin{array}{l} 185.130 \\ 38.682. \end{array} \right. \end{array} \right.$

$$\text{6. Given } \begin{cases} a = 1800. \\ b = 2000. \\ B = 111^\circ 15'. \end{cases} \quad \text{Req. } \begin{cases} A = 57^\circ 0' 50''. \\ C = 11^\circ 44' 10''. \\ c = 436.49. \end{cases}$$

75. Case III.

Given two sides and their included angle, required the remaining parts.

Let ABC be a triangle, and let the sides opposite the angles A, B, C , be denoted, respectively, by a, b, c . Let a and b , and their included angle C , be given, and the remaining parts, A, B , and c , required.



The sum of the angles A and B is found from the formula,

$$A + B = 180^\circ - C.$$

With C as a center, and b , the shorter of the two given sides, as a radius, describe a circumference cutting a in D , a produced in E , and c in H . Draw AE , AD , CH , and DF parallel to AE . The angle DAE is a right angle, since it is inscribed in a semi-circle; hence, its alternate angle, ADF , is also a right angle.

The angle ACE being exterior to the triangle ABC , is equal to $A + B$. But ACE having its vertex at the center, is measured by the intercepted arc AE . The inscribed angle ADE is measured by one-half the arc AE ; hence, $ADE = \frac{1}{2} ACE = \frac{1}{2}(A + B)$.

$CH = CA$, since they are radii of the same circle; hence, the angle $CHA = A$. The angle CHA being exterior to the triangle CHB is equal to $HCB + B$; hence,

$$HCB + B = A. \quad \therefore HCB = A - B.$$

But HCB , having its vertex at the center, is measured by the intercepted arc DH ; and DAF , being an inscribed angle, is measured by one-half the arc DH ; hence, $DAF = \frac{1}{2} HCB = \frac{1}{2}(A - B)$.

In the right triangles ADE and ADF we have

$$AE = AD \tan ADE = AD \tan \frac{1}{2}(A + B).$$

$$DF = AD \tan DAF = AD \tan \frac{1}{2}(A - B).$$

From the similar triangles, ABE and FBD , we have

$$BE : BD :: AE : DF.$$

$$\text{Since } CE = CA, BE = BC + CA = a + b.$$

$$\text{Since } CD = CA, BD = BC - CA = a - b.$$

Substituting the values of BE, BD, AE , and DF in the above proportion, and omitting the common factor AD in the second couplet, we have

$$a + b : a - b :: \tan \frac{1}{2}(A + B) : \tan \frac{1}{2}(A - B).$$

Hence, In any plane triangle, the sum of the sides including an angle is to their difference as the tangent of half the sum of the other two angles is to the tangent of half their difference.

We find from the proportion, the equation

$$\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}.$$

$$\therefore \log \tan \frac{1}{2}(A - B) = \log(a - b) + \log \tan \frac{1}{2}(A + B) + a. c. \log(a + b) - 10.$$

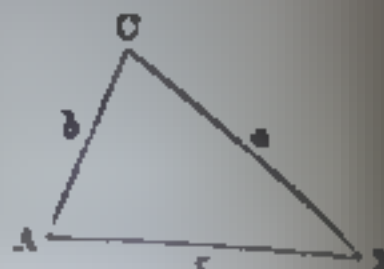
We have now found $\frac{1}{2}(A + B)$ and $\frac{1}{2}(A - B)$.

$$A = \frac{1}{2}(A + B) + \frac{1}{2}(A - B), \quad B = \frac{1}{2}(A + B) - \frac{1}{2}(A - B).$$

$$\sin A : \sin C :: a : c, \quad \therefore c = \frac{a \sin C}{\sin A}.$$

$$\therefore \log c = \log a + \log \sin C + a. c. \log \sin A - 10.$$

76. Examples.

$$1. \text{ Given } \begin{cases} a = 37.56. \\ b = 23.75. \\ C = 68^\circ 25'. \end{cases} \text{ Req. } \begin{cases} A. \\ B. \\ c. \end{cases}$$


$$A + B = 180^\circ - C = 111^\circ 35'.$$

$$a + b : a - b :: \tan \frac{1}{2}(A + B) : \tan \frac{1}{2}(A - B).$$

$$\therefore \tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}.$$

$$\therefore \log \tan \frac{1}{2}(A - B) = \log (a - b) + \log \tan \frac{1}{2}(A + B) + a. c. \log (a + b) - 10$$

$$\log (a - b) (13.81) = 1.14019$$

$$\log \tan \frac{1}{2}(A + B) (55^\circ 47' 30'') = 10.16761$$

$$a. c. \log (a + b) (61.31) = 8.21247$$

$$\log \tan \frac{1}{2}(A - B) = 9.52027$$

$$\therefore \frac{1}{2}(A - B) = 18^\circ 19' 55''$$

$$A = \frac{1}{2}(A + B) + \frac{1}{2}(A - B) = 74^\circ 7' 25''.$$

$$B = \frac{1}{2}(A + B) - \frac{1}{2}(A - B) = 37^\circ 27' 35''.$$

$$\sin A : \sin C :: a : c, \therefore c = \frac{a \sin C}{\sin A}$$

$$\log c = \log a + \log \sin C + a. c. \log \sin A - 10.$$

$$\log a (37.56) = 1.57473$$

$$\log \sin C (68^\circ 25') = 9.96843$$

$$a. c. \log \sin A (74^\circ 7' 25'') = 0.01689$$

$$\log c = 1.56005, \therefore c = 36.312$$

$$2. \text{ Given } \begin{cases} a = 996.63. \\ b = 712.83. \\ C = 72^\circ 29' 48''. \end{cases} \text{ Req. } \begin{cases} A = 66^\circ 30' 37''. \\ B = 40^\circ 59' 35''. \\ c = 1036.35. \end{cases}$$

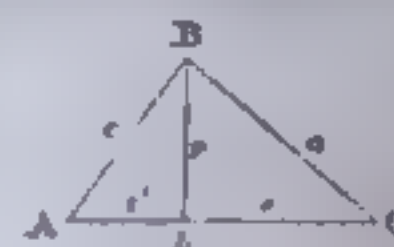
$$3. \text{ Given } \begin{cases} b = 776.525. \\ c = 231.5. \\ A = 48^\circ 35'. \end{cases} \text{ Req. } \begin{cases} B = 115^\circ 36' 56''. \\ C = 15^\circ 48' 04''. \\ a = 645.8. \end{cases}$$

$$4. \text{ Given } \begin{cases} a = 11.7209. \\ c = 10.9232. \\ B = 65^\circ 25' 35''. \end{cases} \text{ Req. } \begin{cases} A = 60^\circ 25' 34''. \\ C = 54^\circ 08' 51''. \\ b = 12.256. \end{cases}$$

77. Case IV.

Given the three sides of a triangle, required the angles.

Let ABC be a triangle, take the longest side for the base, and draw the perpendicular p from the vertex B to the base.



Denote the segments of the base by s and s' respectively.

$$\text{Then, (1) } c^2 - s'^2 = p^2, \text{ and (2) } a^2 - s^2 = p^2.$$

$$\therefore (3) c^2 - s'^2 = a^2 - s^2, \therefore (4) s^2 - s'^2 = a^2 - c^2.$$

$$\therefore (5) (s + s')(s - s') = (a + c)(a - c).$$

$$\therefore (6) s + s' : a + c :: a - c : s - s'.$$

Hence, The sum of the segments of the base is to the sum of the other sides as the difference of those sides is to the difference of the segments.

$$(6) \text{ gives } (7) s - s' = \frac{(a + c)(a - c)}{s + s'}.$$

$$\therefore (8) \log (s - s') = \log (a + c) + \log (a - c) + a. c. \log (s + s') - 10.$$

In case the sides of the triangle are small, find $s - s'$ from (7); otherwise, it will be more convenient to employ (8).

Having $s = s'$ and $s = s'$, we find s and s' thus,

$$(9) \quad s = \frac{1}{2}(s + s') + \frac{1}{2}(s - s'), \quad (10) \quad s' = \frac{1}{2}(s + s') - \frac{1}{2}(s - s')$$

$$(11) \quad \cos A = \frac{s'}{c}, \quad (12) \quad \cos C = \frac{s}{a}.$$

Introducing R , reducing, and applying logarithms,

$$(13) \quad \log \cos A = 10 + \log s' - \log c.$$

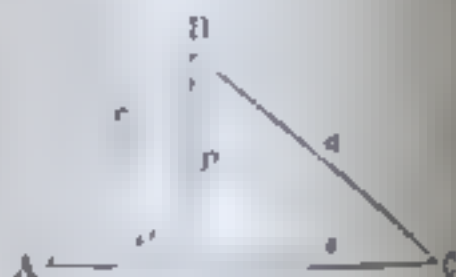
$$(14) \quad \log \cos C = 10 + \log s - \log a.$$

From which we find A and C .

$$\text{Then, } (15) \quad B = 180^\circ - (A + C).$$

78. Examples.

$$1. \text{ Given } \begin{cases} a = 125. \\ b = 150. \\ c = 100. \end{cases} \quad \text{Req. } \begin{cases} A. \\ B. \\ C. \end{cases}$$



$$s + s' : a + c :: a - c : s - s'.$$

$$\therefore s - s' = \frac{(a + c)(a - c)}{s + s'} = \frac{225 \times 25}{150} = 37.5.$$

$$s = \frac{1}{2}(s + s') + \frac{1}{2}(s - s') = 75 + 18.75 = 93.75.$$

$$s' = \frac{1}{2}(s + s') - \frac{1}{2}(s - s') = 75 - 18.75 = 56.25.$$

$$\cos A = \frac{s'}{c}, \text{ or introducing } R, \cos A = \frac{Rs'}{c}.$$

$$\therefore \log \cos A = 10 + \log s' - \log c.$$

$$\log s' (56.25) = 1.75012$$

$$\log c (100) = 2.00000$$

$$\log \cos A = 9.75012 \quad \therefore A = 55^\circ 46' 18''.$$

$$\cos C = \frac{s}{a}, \text{ or introducing } R, \cos C = \frac{Rs}{a}.$$

$$\therefore \log \cos C = 10 + \log s - \log a.$$

$$\log s (93.75) = 1.97197$$

$$\log a (125) = 2.09691$$

$$\log \cos C = 9.87506 \quad \therefore C = 41^\circ 21' 34''.$$

$$B = 180 - (A + C) = 82^\circ 49' 08''.$$

$$2. \text{ Given } \begin{cases} a = 832.21. \\ b = 345.46. \\ c = 237.61. \end{cases} \quad \text{Required } \begin{cases} A = 66^\circ 30' 35''. \\ B = 72^\circ 29' 53''. \\ C = 40^\circ 59' 32''. \end{cases}$$

$$3. \text{ Given } \begin{cases} a = 864. \\ b = 1308. \\ c = 1086. \end{cases} \quad \text{Required } \begin{cases} A = 41^\circ 00' 38''. \\ B = 83^\circ 25' 14''. \\ C = 55^\circ 34' 08''. \end{cases}$$

$$4. \text{ Given } \begin{cases} a = 251.25. \\ b = 302.5. \\ c = 342. \end{cases} \quad \text{Required } \begin{cases} A = 15^\circ 22' 41''. \\ B = 58^\circ 58' 20''. \\ C = 75^\circ 38' 59''. \end{cases}$$

APPLICATION TO HEIGHTS AND DISTANCES

79. Definitions.

1. A horizontal plane is a plane parallel to the horizon.

2. A vertical plane is a plane perpendicular to a horizontal plane.

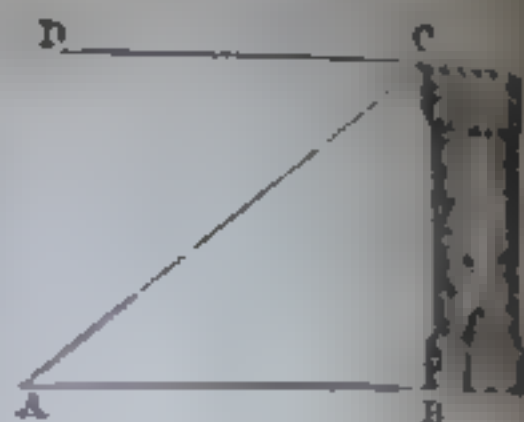
3. A horizontal line is a line parallel to a horizontal plane.

4. A vertical line is a line perpendicular to a horizontal plane.

5. A horizontal angle is an angle whose plane is horizontal.

6. A vertical angle is an angle whose plane is vertical.

7. An angle of elevation is a vertical angle, one of whose sides is horizontal, and the inclined side above the horizontal side. Thus, BAC .



8. An angle of depression is a vertical angle, one of whose sides is horizontal, and the inclined side below the horizontal side. Thus, DCA .

80. Problems.

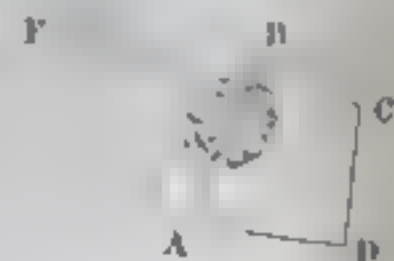
1. Wishing to know the height of a tree standing on a horizontal plane, I measured from the tree the horizontal line BA , 150 ft., and found the angle of elevation, BAC , to the top of the tree to be $35^\circ 20'$. Required the height of the tree.

Ans. 106.335 ft.



2. In surveying a tract of land, I found it impracticable to measure the side AB on account of thick brushwood lying between A and B . I therefore measured AE , 7.50 ch., and EB , 8.70 ch., and found the angle $AEB = 38^\circ 46'$. Required AB .

Ans. 5.494 ch.



3. One side of a triangular field is double another, their included angle is 60° , and the third side is 1 ch. Required the longest side.

Ans. 17.32 ch.

4. Wishing to know the width of a river, from the point A on one bank to the point C on the other bank, I measure the distance AB , 75 yd., and find the angle $BAC = 87^\circ 28' 30''$, and the angle $ABC = 47^\circ 38' 25''$. Required AC , the width of the river. *Ans.* 78.53 yd.



5. I find the angle of elevation, BAC , from the foot of a hill to the top to be $46^\circ 25' 30''$. Measuring back from the hill, $AD = 500$ ft., I find the angle of elevation $ADC = 25^\circ 38' 40''$. Required BC , the vertical height of the hill. *Ans.* 441.87 ft.



6. From the foot of a tower standing at the top of a declivity, I measured $AB = 45$ ft., and the angle $ABD = 50^\circ 15'$. I also measured, in a straight line with AB , $BC = 68$ ft., and the angle $BCD = 30^\circ 45'$. Required AD , the height of the tower. *Ans.* 82.94 ft.



7. Wishing to know the height of a tower standing on a hill, I find the angle of elevation, BAC , to the top of the hill to be $44^\circ 35'$, and the angle of elevation to the top of the tower to be $59^\circ 48'$. Measuring the horizontal line AE , 275 ft., I find the angle of eleva-



tion to the top of the tower to be $46^\circ 25'$. Required the height of the tower. *Ans.* 317.143 ft.

S. Given $\left\{ \begin{array}{l} DC = 24 \text{ ch.} \\ CDB = 45^\circ. \\ BDA = 50^\circ. \\ DCA = 48^\circ. \\ ACB = 60^\circ. \end{array} \right.$



Required $AB = 38.61 \text{ ch.}$

9. Given $AB = 800 \text{ yd.}$, $AC = 600 \text{ yd.}$, $BC = 400 \text{ yd.}$, $ADC = 33^\circ 45'$, $BDC = 22^\circ 30'$. Required DA , DC , DB .

Ans. $DA = 710.15 \text{ yd.}$, $DC = 1042.5 \text{ yd.}$, $DB = 934.28 \text{ yd.}$

Remark.—Describing the circumference through A , B , D , and drawing AE and BE , $EAB = BDC$, $EBA = ADC$.



RELATIONS OF CIRCULAR FUNCTIONS.

1. Fundamental Formulas.

Let a be the angle OCT the arc OT , and $CO = CT = 1$. Then, we have $MT = CN = \sin a$, $NT = CM = \cos a$, $MO = \text{vers } a$, $NO = \text{covers } a$, $OR = \tan a$, $OS = \cot a$, $CR = \sec a$, $CS = \text{cosec } a$.

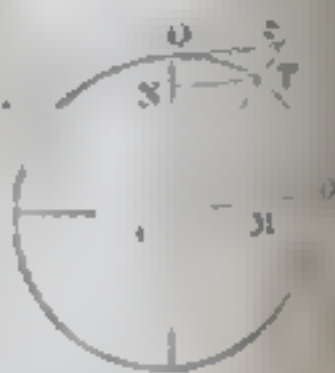
By articles 39–46, $\sin(90^\circ - a) = \cos a$, $\cos(90^\circ - a) = \sin a$, etc.

From the diagram we have

$$MT^2 + CM^2 = CT^2.$$

Substituting the values of MT , CM , and CT , we have

$$(1) \sin^2 a + \cos^2 a = 1.$$



Hence, *The square of the sine of any arc plus the square of its co-sine is equal to 1.*

From (1) we have, by transposition,

$$(2) \sin^2 a = 1 - \cos^2 a,$$

$$(3) \cos^2 a = 1 - \sin^2 a. \text{ Hence,}$$

1. *The square of the sine of any arc is equal to 1 minus the square of its co-sine.*

2. *The square of the co-sine of any arc is equal to 1 minus the square of its sine.*

From the diagram we have

$$MO = CO - CM.$$

Substituting the values of MO , CO , and CM , we have

$$(4) \text{vers } a = 1 - \cos a.$$

Hence, *The versed-sine of any arc is equal to 1 minus its co-sine.*

$$\therefore \text{vers}(90^\circ - a) = 1 - \cos(90^\circ - a)$$

$$\therefore \text{covers } a = 1 - \sin a.$$

Hence, *The coversed-sine of any arc is equal to 1 minus its sine.*

From the diagram we have

$$CM : CO :: MT : OR,$$

$$\text{or } \cos a : 1 :: \sin a : \tan a.$$

$$\therefore (6) \tan a = \frac{\sin a}{\cos a}.$$

Hence, *The tangent of any arc is equal to its sine divided by its co-sine.*

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$$\therefore \tan (90^\circ - a) = \frac{\sin (90^\circ - a)}{\cos (90^\circ - a)}.$$

$$\therefore (7) \cot a = \frac{\cos a}{\sin a}.$$

Hence, *The co-tangent of any arc is equal to its cosine divided by its sine.*

$$(6) \times (7) = (8) \tan a \cot a = 1.$$

Hence, *The tangent of any arc into its co-tangent is equal to 1.*

$$(8) \div \cot a = (9) \tan a = \frac{1}{\cot a}.$$

Hence, *The tangent of any arc is equal to the reciprocal of its co-tangent.*

$$(8) \div \tan a = (10) \cot a = \frac{1}{\tan a}.$$

Hence, *The co-tangent of any arc is equal to the reciprocal of its tangent.*

$$CM : CO :: CT : CR, \text{ or } \cos a : 1 :: 1 : \sec a.$$

$$\therefore (11) \sec a = \frac{1}{\cos a}.$$

Hence, *The secant of any arc is equal to the reciprocal of its cosine.*

$$\therefore \sec (90^\circ - a) = \frac{1}{\cos (90^\circ - a)}.$$

$$\therefore (12) \operatorname{cosec} a = \frac{1}{\sin a}.$$

Hence, *The co-secant of any arc is equal to the reciprocal of its sine.*

$$\overline{CR}^2 = \overline{CO}^2 + \overline{OR}^2,$$

$$\therefore (13) \sec^2 a = 1 + \tan^2 a.$$

Hence, *The square of the secant of any arc is equal to 1, plus the square of its tangent.*

$$\therefore \sec^2 (90^\circ - a) = 1 + \tan^2 (90^\circ - a).$$

$$\therefore (14) \operatorname{cosec}^2 a = 1 + \cot^2 a.$$

Hence, *The square of the co-secant is equal to 1, plus the square of the co-tangent.*

82. Summary of Fundamental Formulas.

$$1. \sin^2 a + \cos^2 a = 1.$$

$$2. \sin^2 a = 1 - \cos^2 a.$$

$$3. \cos^2 a = 1 - \sin^2 a.$$

$$4. \operatorname{vers} a = 1 - \cos a.$$

$$5. \operatorname{covers} a = 1 - \sin a.$$

$$6. \tan a = \frac{\sin a}{\cos a}.$$

$$7. \cot a = \frac{\cos a}{\sin a}.$$

$$8. \tan a \cot a = 1.$$

$$9. \tan a = \frac{1}{\cot a}.$$

$$10. \cot a = \frac{1}{\tan a}.$$

$$11. \sec a = \frac{1}{\cos a}.$$

$$12. \operatorname{cosec} a = \frac{1}{\sin a}.$$

$$13. \sec^2 a = 1 + \tan^2 a.$$

$$14. \operatorname{cosec}^2 a = 1 + \cot^2 a.$$

83. Problems.

1. Prove that the above formulas become homogeneous by the introduction of R .

2. Deduce formulas (5), (7), (12) and (14) from the diagram.

3. Prove that the above formulas are true if a is in the second, third, or fourth quadrant.

84. Each Function in Terms of the Others.

$$\sin a = \sqrt{1 - \cos^2 a}.$$

$$\sin a = 1 - 2 \text{vers } a = \sqrt{1 - \cos^2 a}.$$

$$\sin a = 1 - \text{covers } a.$$

$$\sin a = \frac{\tan a}{\sqrt{1 + \tan^2 a}}.$$

$$\sin a = \frac{1}{\sqrt{1 + \cot^2 a}}.$$

$$\sin a = \frac{1 - \sec^2 a}{\sec a}.$$

$$\sin a = \frac{1}{\text{cosec } a}.$$

$$\cos a = \sqrt{1 - \sin^2 a}.$$

$$\cos a = 1 - \text{vers } a.$$

$$\cos a = 1 - \sqrt{2 \text{cvs } a - \text{cvs}^2 a}.$$

$$\cos a = \frac{1}{\sqrt{1 + \tan^2 a}}.$$

$$\cos a = \frac{\cot a}{\sqrt{1 + \cot^2 a}}.$$

$$\cos a = \frac{1}{\sec a}.$$

$$\cos a = \frac{1 - \text{cosec}^2 a}{\text{cosec } a}.$$

$$\text{vers } a = 1 - \sqrt{1 - \sin^2 a}.$$

$$\text{vers } a = 1 - \cos a.$$

$$\text{vers } a = 1 - \sqrt{2 \text{cvs } a - \text{cvs}^2 a}.$$

$$\text{vers } a = 1 - \frac{1}{\sqrt{1 + \tan^2 a}}.$$

$$\text{vers } a = 1 - \frac{\cot a}{\sqrt{1 + \cot^2 a}}.$$

$$\text{vers } a = \frac{\sec a - 1}{\sec a}.$$

$$\text{vers } a = 1 - \frac{1 - \text{cosec}^2 a}{\text{cosec } a}.$$

$$\text{covers } a = 1 - \sin a.$$

$$\text{covers } a = 1 - \sqrt{1 - \cos^2 a}.$$

$$\text{cvs } a = 1 - \sqrt{2 \text{vs } a - \text{vs}^2 a}.$$

$$\text{covers } a = 1 - \frac{\tan a}{\sqrt{1 + \tan^2 a}}.$$

$$\text{covers } a = 1 - \frac{1}{\sqrt{1 + \cot^2 a}}.$$

$$\text{covers } a = 1 - \frac{1 - \sec^2 a}{\sec a}.$$

$$\text{covers } a = \frac{\text{cosec } a - 1}{\text{cosec } a}.$$

84. Each Function in Terms of the Others.

$$\tan a = \frac{\sin a}{\sqrt{1 - \sin^2 a}}.$$

$$\tan a = \frac{1 - \cos^2 a}{\cos a}.$$

$$\tan a = \frac{\sqrt{2 \text{vs } a - \text{vs}^2 a}}{1 - \text{vs } a}.$$

$$\tan a = \frac{1 - \text{cvs } a}{\sqrt{2 \text{cvs } a - \text{cvs}^2 a}}.$$

$$\tan a = \frac{1}{\cot a}.$$

$$\tan a = \sqrt{\sec^2 a - 1}.$$

$$\tan a = \frac{1}{1 - \text{cosec}^2 a}.$$

$$\cot a = \frac{1 - \sin^2 a}{\sin a}.$$

$$\cot a = \frac{\cos a}{1 - \cos^2 a}.$$

$$\cot a = \frac{1 - \text{vs } a}{\sqrt{2 \text{vs } a - \text{vs}^2 a}}.$$

$$\cot a = \frac{1 - \text{cvs } a}{\sqrt{2 \text{cvs } a - \text{cvs}^2 a}}.$$

$$\cot a = \frac{1}{\tan a}.$$

$$\cot a = \frac{1}{1 - \sec^2 a}.$$

$$\cot a = 1 - \text{cosec}^2 a.$$

$$\sec a = \frac{1}{\sqrt{1 - \sin^2 a}}.$$

$$\sec a = \frac{1}{\cos a}.$$

$$\sec a = \frac{1}{1 - \text{vers } a}.$$

$$\sec a = \frac{1}{\sqrt{2 \text{cvs } a - \text{cvs}^2 a}}.$$

$$\sec a = \sqrt{1 + \tan^2 a}.$$

$$\sec a = \frac{1 + \cot^2 a}{\cot a}.$$

$$\sec a = \frac{\text{cosec } a}{1 - \text{cosec}^2 a}.$$

$$\text{cosec } a = \frac{1}{\sin a}.$$

$$\text{cosec } a = \frac{1}{1 - \cos^2 a}.$$

$$\text{cosec } a = \frac{1}{1 - 2 \text{vs } a + \text{vs}^2 a}.$$

$$\text{cosec } a = \frac{1}{1 - \text{covers } a}.$$

$$\text{cosec } a = \frac{\sqrt{1 + \tan^2 a}}{\tan a}.$$

$$\text{cosec } a = \sqrt{1 + \cot^2 a}.$$

$$\text{cosec } a = \frac{\sec a}{1 - \sec^2 a}.$$

85. Functions of Negative Arcs.

We first find the sine and co-sine of $-a$, in terms of the functions of a from the diagram. Then, dividing the sine by the co-sine, the cosine by the sine, taking the reciprocal of the co-sine and the reciprocal of the sine, we have



$$\begin{aligned}\sin(-a) &= -\sin a, & \cos(-a) &= \cos a, \\ \tan(-a) &= -\tan a, & \cot(-a) &= -\cot a, \\ \sec(-a) &= \sec a, & \operatorname{cosec}(-a) &= -\operatorname{cosec} a.\end{aligned}$$

86. Functions of $(n 90^\circ \mp a)$.

1. Let n be 1 and a be negative.

From the figure of the last article, and by similar processes,

$$\begin{aligned}\sin(90^\circ - a) &= \cos a, & \cos(90^\circ - a) &= \sin a, \\ \tan(90^\circ - a) &= \cot a, & \cot(90^\circ - a) &= \tan a, \\ \sec(90^\circ - a) &= \operatorname{cosec} a, & \operatorname{cosec}(90^\circ - a) &= \sec a.\end{aligned}$$

These relations have already been found, articles 39—46.

2. Let n be 1 and a be positive.

$$\begin{aligned}\sin(90^\circ + a) &= \cos a, & \cos(90^\circ + a) &= -\sin a, \\ \tan(90^\circ + a) &= -\cot a, & \cot(90^\circ + a) &= -\tan a, \\ \sec(90^\circ + a) &= -\operatorname{cosec} a, & \operatorname{cosec}(90^\circ + a) &= \sec a.\end{aligned}$$

3. Let n be 2, and a be negative.

$$\begin{aligned}\sin(180^\circ - a) &= \sin a, & \cos(180^\circ - a) &= -\cos a, \\ \tan(180^\circ - a) &= -\tan a, & \cot(180^\circ - a) &= -\cot a, \\ \sec(180^\circ - a) &= -\sec a, & \operatorname{cosec}(180^\circ - a) &= \operatorname{cosec} a.\end{aligned}$$

4. Let n be 2, and a be positive.

$$\begin{aligned}\sin(180^\circ + a) &= -\sin a, & \cos(180^\circ + a) &= -\cos a, \\ \tan(180^\circ + a) &= \tan a, & \cot(180^\circ + a) &= \cot a, \\ \sec(180^\circ + a) &= \sec a, & \operatorname{cosec}(180^\circ + a) &= -\operatorname{cosec} a.\end{aligned}$$

5. Let n be 3, and a be negative.

$$\begin{aligned}\sin(270^\circ - a) &= \cos a, & \cos(270^\circ - a) &= -\sin a, \\ \tan(270^\circ - a) &= \cot a, & \cot(270^\circ - a) &= \tan a, \\ \sec(270^\circ - a) &= -\operatorname{cosec} a, & \operatorname{cosec}(270^\circ - a) &= -\sec a.\end{aligned}$$

6. Let n be 3, and a be positive.

$$\begin{aligned}\sin(270^\circ + a) &= -\cos a, & \cos(270^\circ + a) &= \sin a, \\ \tan(270^\circ + a) &= \cot a, & \cot(270^\circ + a) &= \tan a, \\ \sec(270^\circ + a) &= \operatorname{cosec} a, & \operatorname{cosec}(270^\circ + a) &= -\sec a.\end{aligned}$$

7. Let n be 4, and a be negative.

$$\begin{aligned}\sin(360^\circ - a) &= -\sin a, & \cos(360^\circ - a) &= \cos a, \\ \tan(360^\circ - a) &= -\tan a, & \cot(360^\circ - a) &= -\cot a, \\ \sec(360^\circ - a) &= \sec a, & \operatorname{cosec}(360^\circ - a) &= -\operatorname{cosec} a.\end{aligned}$$

8. Let n be 4, and a be positive.

$$\begin{aligned}\sin(360^\circ + a) &= \sin a, & \cos(360^\circ + a) &= \cos a, \\ \tan(360^\circ + a) &= \tan a, & \cot(360^\circ + a) &= \cot a, \\ \sec(360^\circ + a) &= \sec a, & \operatorname{cosec}(360^\circ + a) &= \operatorname{cosec} a.\end{aligned}$$

It will be observed that when n is even, the functions in the two members of the equations have the same name; and that when n is odd, they have contrary names. The algebraic sign attributed to the second member is determined by the quadrant in which the arc is situated.

Let this article be reviewed, and these principles applied in determining the names and algebraic signs of the second members.

Hence, functions of arcs greater than 90° can be found in terms of functions of arcs less than 90° . Thus,

$$\begin{aligned} 1. \quad \sin 120^\circ &= \sin (90^\circ + 30^\circ) = \cos 30^\circ. \\ 2. \quad \cos 270^\circ &= \cos (270^\circ + 20^\circ) = -\sin 20^\circ. \\ 3. \quad \tan 165^\circ &= \tan (180^\circ - 15^\circ) = -\tan 15^\circ. \end{aligned}$$

If n is integral and positive, prove the following:

$$\begin{aligned} 4. \quad \sin [n 180^\circ + (-1)^n a] &= \sin a. \\ 5. \quad \cos (n 360^\circ \pm a) &= \cos a. \\ 6. \quad \tan (n 180^\circ + a) &= \tan a. \\ 7. \quad \text{Any function of } (n 360^\circ + a) &= \text{the same function of } a, \text{ whatever be the value of } a. \end{aligned}$$

87. Values of Functions of Particular Arcs.

1. To find the functions of 30° .

Since 60° is one-sixth of the circumference, the chord of 60° is equal to one side of a regular inscribed hexagon, which is equal to the radius or 1. But the sine of 30° is equal to one-half the chord of 60° .

$$\therefore (1) \sin 30^\circ = \frac{1}{2}, \quad \therefore (2) \cos 30^\circ = \sqrt{1 - \frac{1}{4}} = \frac{1}{2} \sqrt{3}.$$

Dividing (1) by (2), then (2) by (1), taking the reciprocals of (2) and (1), we have

$$(3) \tan 30^\circ = \frac{1}{\sqrt{3}}, \quad (4) \cot 30^\circ = \sqrt{3}.$$

$$(5) \sec 30^\circ = \frac{2}{\sqrt{3}}, \quad (6) \operatorname{cosec} 30^\circ = 2.$$

2. To find the functions of 60° .

From article 40, $\sin 60^\circ = \sin (90^\circ - 30^\circ) = \cos 30^\circ$,
 $\cos 60^\circ = \cos (90^\circ - 30^\circ) = \sin 30^\circ$. Hence,

$$\begin{aligned} (1) \sin 60^\circ &= \frac{1}{2} \sqrt{3}, & (2) \cos 60^\circ &= \frac{1}{2}, \\ (3) \tan 60^\circ &= \sqrt{3}, & (4) \cot 60^\circ &= \frac{1}{\sqrt{3}}, \\ (5) \sec 60^\circ &= 2, & (6) \operatorname{cosec} 60^\circ &= \frac{2}{\sqrt{3}}. \end{aligned}$$

3. To find the functions of 45° .

From Art. 40, $\sin 45^\circ = \sin (90^\circ - 45^\circ) = \cos 45^\circ$;
 but $\sin^2 45^\circ + \cos^2 45^\circ = 1$,

$$\therefore 2 \sin^2 45^\circ = 1, \quad \therefore \sin^2 45^\circ = \frac{1}{2}. \text{ Hence,}$$

$$\begin{aligned} (1) \sin 45^\circ &= \frac{1}{2} \sqrt{2}, & (2) \cos 45^\circ &= \frac{1}{2} \sqrt{2}, \\ (3) \tan 45^\circ &= 1, & (4) \cot 45^\circ &= 1, \\ (5) \sec 45^\circ &= \sqrt{2}, & (6) \operatorname{cosec} 45^\circ &= \sqrt{2}. \end{aligned}$$

Prove the following:

$$\begin{array}{ll} 1. \sec 120^\circ = -2. & 5. \operatorname{cosec} 210^\circ = -2. \\ 2. \cos 135^\circ = -\frac{1}{2} \sqrt{2}. & 6. \cot 240^\circ = \frac{1}{\sqrt{3}}. \\ 3. \sin 300^\circ = -\frac{1}{2} \sqrt{3}. & 7. \sin 330^\circ = \frac{1}{2}. \\ 4. \tan 225^\circ = -1. & 8. \cos (-120^\circ) = -\frac{1}{2}. \end{array}$$

9. Construct an angle whose tangent is -1 .
 10. Construct an angle whose sine is $-\frac{1}{2}$.
 11. Find all the functions of 150° .

88. Inverse Trigonometric Functions.

If $x = \sin a$, then a is the angle or arc whose sine is x , which is written $a = \sin^{-1} x$, and read a equals the arc whose sine is x .

It must not be supposed that $^{-1}$ is an exponent, and that $\sin^{-1} x = \frac{1}{\sin x}$; this would be a grievous error.

Let the following be read:

$$\cos^{-1} x, \tan^{-1} x, \sec^{-1} x, \csc^{-1} x, \sin^{-1}(\cos x), \sin(\sin^{-1} x), \\ \sin^{-1} x = \csc^{-1} \frac{1}{x}, \cos^{-1} x = \sec^{-1} \frac{1}{x}, \tan^{-1} x = \cot^{-1} \frac{1}{x}.$$

The above notation is not altogether arbitrary; for let $f(x)$ be any function of x , and let $f[f(x)]$, or, more briefly, let $f^2(x)$ be the same function of $f(x)$, which notation denotes, not the square of $f(x)$, that is, not $[f(x)]^2$, but that the same function is taken of $f(x)$ as of x . Thus, if $f(x) = \sin x$, $f[f(x)] = \sin(\sin x)$, then, in general,

$$(1) \quad f^n f^m(x) = f^{n+m}(x).$$

If $n = 0$, (1) becomes,

$$(2) \quad f^n f^0(x) = f^n(x).$$

$$\therefore (3) \quad f^0(x) = x.$$

If $m = 1$, and $n = -1$, (1) becomes,

$$(4) \quad f f^{-1}(x) = f^0(x) = x.$$

Hence, $f^{-1}(x)$ denotes a quantity whose like function is x .

Hence, if $y = \sin^{-1} x$, $\sin y = \sin(\sin^{-1} x) = x$; that is, y or $\sin^{-1} x$ is an arc whose sine is x .

It would follow from the above that $\sin^2 a$ ought to signify $\sin(\sin a)$, and not $(\sin a)^2$; but since we rarely have $\sin(\sin a)$, it is customary to write $\sin^2 a$ for $\sin a^2$, as we are thus saved the trouble of writing the parenthesis.

It would not, of course, do to write $\sin a^2$ for $(\sin a)^2$, for then we should have the sine of the square of an arc for the square of the sine of an arc.

Let the following equations be proved:

$$\begin{array}{ll} 1. \quad \sin^{-1} \frac{1}{2} = \cos^{-1} \frac{1}{2}. & 4. \quad \cos^{-1} \frac{1}{2} = 2 \cot^{-1} \sqrt{3}. \\ 2. \quad \sin^{-1} \frac{1}{2} = \frac{1}{2} \tan^{-1} \sqrt{3}. & 5. \quad \sin^{-1} 1 = 2 \tan^{-1} 1. \\ 3. \quad \tan^{-1} \sqrt{3} = \sec^{-1} 2. & 6. \quad \sec^{-1} 2 = \frac{1}{2} \sec^{-1}(-2). \end{array}$$

89. Problem.

To find the sine and co-sine of the sum of two angles.

Let $a =$ the angle OCA , and $b =$ the angle ACB . Draw BL perpendicular to CA , BP and LM perpendicular to CO , and LN parallel to CO .

The triangles NBL and MCL are similar, since their sides are respectively perpendicular; hence, the angle NBL opposite the side NL equals the angle MCL opposite the homologous side ML . But $MCL = a$; hence $NBL = a$.



From the diagram we find the following relations:

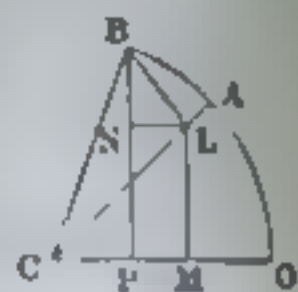
- (1) $LB = \sin b$.
- (2) $CL = \cos b$.
- (3) $PB = ML + NB$.
- (4) $PB = \sin OCB = \sin(a + b)$.
- (5) $ML = \sin MCL \times CL = \sin a \cos b$.
- (6) $NB = \cos NBL \times LB = \cos a \sin b$.

Substituting the values of PB , ML , and NB , found in (4), (5), and (6), in (3), and denoting the formula by (a), we have

$$(a) \quad \sin(a + b) = \sin a \cos b + \cos a \sin b.$$

Hence, *The sine of the sum of two angles is equal to the sine of the first plus the cosine of the second, plus the cosine of the first into the sine of the second.*

From the diagram we find the following relations:



- (1) $CP = CM - NL$
- (2) $CP = \cos OCB = \cos (a + b)$.
- (3) $CM = \cos MCL \times CL = \cos a \cos b$.
- (4) $NL = \sin NBL \times LB = \sin a \sin b$.

Substituting the values of CP , CM , and NL , found in (2), (3), and (4), in (1), we have

$$(b) \cos (a + b) = \cos a \cos b - \sin a \sin b.$$

Hence, *The cosine of the sum of two angles is equal to the product of their co-sines minus the product of their sines.*

90. Problems.

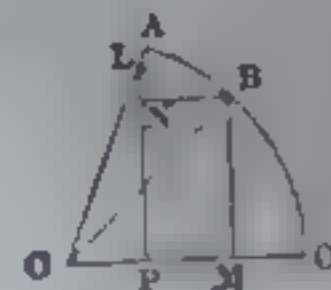
1. Prove that formulas (a) and (b) become homogeneous by introducing R .
2. Prove that formulas (a) and (b) are true when $(a + b)$ is in the second quadrant.
3. Prove that formulas (a) and (b) are true when $(a + b)$ is in the third quadrant.
4. Prove that formulas (a) and (b) are true when $a - b$ is in the fourth quadrant.
5. Deduce formula (b) from formula (a) by substituting $90^\circ - a$ for a , and $-b$ for b , and reducing by articles 85-86.
6. Develop $\sin (45^\circ + 30^\circ)$ by formula (a).
7. Develop $\cos 105^\circ$ by formula (b).

91. Problem.

To find the sine and co-sine of the difference of two angles.

Let $a =$ the angle OCA , and $b =$ the angle BCA .

Draw BL perpendicular to CA , LP and BM perpendicular to CO , and BN parallel to CO .



The triangles NLB and PCL are similar, since their sides are respectively perpendicular; hence, the angle NLB , opposite the side NB , equals the angle PCL opposite the homologous side PL . But the angle $PCL = a$, hence, the angle $NLB = a$. Then we shall have

- (1) $LB = \sin b$.
- (2) $CL = \cos b$.
- (3) $MB = PL - NL$.
- (4) $MB = \sin OCB = \sin (a - b)$.
- (5) $PL = \sin PCL \times CL = \sin a \cos b$.
- (6) $NL = \cos NLB \times LB = \cos a \sin b$.

Substituting the values of MB , PL , and NL , found in (4), (5), and (6), in (3), we have

$$(c) \sin (a - b) = \sin a \cos b - \cos a \sin b.$$

Hence, *The sine of the difference of two angles is equal to the sine of the first into the co-sine of the second, minus the co-sine of the first into the sine of the second.*

From the diagram we find the following relations:

- (1) $CM = CP + NB$.
- (2) $CM = \cos OCB = \cos (a - b)$.
- (3) $CP = \cos PCL \times CL = \cos a \cos b$.
- (4) $NB = \sin NLB \times LB = \sin a \sin b$.

Substituting in (1) the values of CM , CP , and NB in (1), (2), (3), and (4), we have

$$(1) \cos(a-b) = \cos a \cos b + \sin a \sin b.$$

Hence, *The cosine of the difference of two angles is equal to the product of their cosines, plus the product of their sines.*

92. Problems.

1. Prove that formulas (c) and (d) become homogeneous by introducing R .
2. Deduce formulas (c) and (d) from (a) and (b), respectively, by substituting $-b$ for b , and reducing by article 85.
3. Prove that formulas (c) and (d) are true when $a-b$ is in the second quadrant.
4. Prove that formulas (c) and (d) are true when $a-b$ is in the third quadrant.
5. Prove that formulas (c) and (d) are true when $a-b$ is in the fourth quadrant.

93. Problem.

To find the tangent and co-tangent of the sum or difference of two angles.

Dividing (a) by (b), we have

$$\frac{\sin(a+b)}{\cos(a+b)} = \frac{\sin a \cos b + \cos a \sin b}{\cos a \cos b - \sin a \sin b}.$$

Dividing both terms of the fraction in the second member by $\cos a \cos b$, reducing, and recollecting that

the sine of an arc divided by its co-sine is equal to its tangent, we have

$$(c) \tan(a+b) = \frac{\tan a + \tan b}{1 - \tan a \tan b}.$$

Hence, *The tangent of the sum of two angles is equal to the sum of their tangents, divided by 1 minus the product of their tangents.*

Dividing (b) by (a), and reducing, we have

$$(f) \cot(a+b) = \frac{\cot a \cot b - 1}{\cot a + \cot b}.$$

Hence, *The co-tangent of the sum of two angles is equal to the product of their co-tangents, minus 1, divided by the sum of their co-tangents.*

Dividing (c) by (d), and reducing, we have

$$(g) \tan(a-b) = \frac{\tan a - \tan b}{1 + \tan a \tan b}.$$

Hence, *The tangent of the difference of two angles is equal to the tangent of the first minus the tangent of the second, divided by 1 plus the product of their tangents.*

Dividing (d) by (c), and reducing, we have

$$(h) \cot(a-b) = \frac{\cot a \cot b + 1}{\cot b - \cot a}.$$

Hence, *The co-tangent of the difference of two angles is equal to the product of their co-tangents, plus 1, divided by the co-tangent of the second, minus the co-tangent of the first.*

94. Problems.

1. Prove that (c), (f), (g), (h) become homogeneous by introducing R .

2. Deduce (g) from (c) by substituting $-b$ for b .
3. Deduce (h) from (f) by substituting $-b$ for b .
4. Deduce (f) from (c) by taking the reciprocal of each member, substituting $\frac{1}{\cot a}$ for $\tan a$, $\frac{1}{\cot b}$ for $\tan b$, and reducing.
5. Deduce, in like manner, (h) from (g).
6. Find the value of $\sin(a+b+c)$ by substituting $b+c$ for b in (a).
7. Find the value of $\cos(a+b+c)$ by substituting $b+c$ for b in (b).
8. Find the value of $\tan(a+b+c)$ by substituting $b+c$ for b in (e).
9. Find the value of $\cot(a+b+c)$ by substituting $b+c$ for b in (f).

95. Functions of Double and Half Angles.

Making $b = a$ in (a), (b), (c), and (f), we have

$$(1) \sin 2a = 2 \sin a \cos a.$$

$$(2) \cos 2a = \cos^2 a - \sin^2 a.$$

$$(3) \tan 2a = \frac{2 \tan a}{1 - \tan^2 a}.$$

$$(4) \cot 2a = \frac{\cot^2 a - 1}{2 \cot a}.$$

Substituting $\frac{1}{2}a$ for a in (1), (2), (3), (4), we have

$$(5) \sin a = 2 \sin \frac{1}{2}a \cos \frac{1}{2}a.$$

$$(6) \cos a = \cos^2 \frac{1}{2}a - \sin^2 \frac{1}{2}a.$$

$$(7) \tan a = \frac{2 \tan \frac{1}{2}a}{1 - \tan^2 \frac{1}{2}a}.$$

$$(8) \cot a = \frac{\cot^2 \frac{1}{2}a - 1}{2 \cot \frac{1}{2}a}.$$

Substituting $1 - \sin^2 \frac{1}{2}a$ for $\cos^2 \frac{1}{2}a$, then $1 - \cos^2 \frac{1}{2}a$ for $\sin^2 \frac{1}{2}a$, in (6), and reducing, we have

$$(9) 1 - \cos a = 2 \sin^2 \frac{1}{2}a.$$

$$(10) 1 + \cos a = 2 \cos^2 \frac{1}{2}a.$$

$$\therefore (11) \sin \frac{1}{2}a = \sqrt{\frac{1 - \cos a}{2}}.$$

$$\therefore (12) \cos \frac{1}{2}a = \sqrt{\frac{1 + \cos a}{2}}.$$

Dividing (11) by (12), then (12) by (11), we have

$$(13) \tan \frac{1}{2}a = \sqrt{\frac{1 - \cos a}{1 + \cos a}}.$$

$$(14) \cot \frac{1}{2}a = \sqrt{\frac{1 + \cos a}{1 - \cos a}}.$$

Dividing (5) first by (10), then by (9), and transposing, we have

$$(15) \tan \frac{1}{2}a = \frac{\sin a}{1 + \cos a}.$$

$$(16) \cot \frac{1}{2}a = \frac{\sin a}{1 - \cos a}.$$

Taking the reciprocal of (16), then of (15), we have

$$(17) \tan \frac{1}{2}a = \frac{1 - \cos a}{\sin a}.$$

$$(18) \cot \frac{1}{2}a = \frac{1 + \cos a}{\sin a}.$$

Let the formulas of this article be expressed in words.

96. Consequences of (a), (b), (c), (d).

Taking the sum and difference of (a) and (c), (d) and (b), we have

$$(1) \sin(a+b) + \sin(a-b) = 2 \sin a \cos b.$$

$$(2) \sin(a+b) - \sin(a-b) = 2 \cos a \sin b.$$

$$(3) \cos(a+b) + \cos(a-b) = 2 \cos a \cos b.$$

$$(4) \cos(a+b) - \cos(a-b) = 2 \sin a \sin b.$$

$$\text{Let } \begin{cases} a+b=s, \\ a-b=d, \end{cases} \text{ then } \begin{cases} a=\frac{1}{2}(s+d), \\ b=\frac{1}{2}(s-d). \end{cases}$$

Substituting the values of $a+b$, $a-b$, a , and b , in (1), (2), (3), and (4), we have

$$(5) \sin s + \sin d = 2 \sin \frac{1}{2}(s+d) \cos \frac{1}{2}(s-d).$$

$$(6) \sin s - \sin d = 2 \cos \frac{1}{2}(s+d) \sin \frac{1}{2}(s-d).$$

$$(7) \cos s + \cos d = 2 \cos \frac{1}{2}(s+d) \cos \frac{1}{2}(s-d).$$

$$(8) \cos d - \cos s = 2 \sin \frac{1}{2}(s+d) \sin \frac{1}{2}(s-d).$$

By formula (5) of the preceding article we have

$$(9) \sin(s+d) = 2 \sin \frac{1}{2}(s+d) \cos \frac{1}{2}(s-d).$$

$$(10) \sin(s-d) = 2 \sin \frac{1}{2}(s-d) \cos \frac{1}{2}(s+d).$$

Dividing each of these formulas by each of the following, we have

$$(11) \frac{\sin s + \sin d}{\sin s - \sin d} = \frac{\sin \frac{1}{2}(s+d) \cos \frac{1}{2}(s-d)}{\cos \frac{1}{2}(s+d) \sin \frac{1}{2}(s-d)} = \tan \frac{1}{2}(s+d).$$

$$(12) \frac{\sin s + \sin d}{\cos s + \cos d} = \frac{\sin \frac{1}{2}(s+d)}{\cos \frac{1}{2}(s+d)} = \tan \frac{1}{2}(s+d).$$

$$(13) \frac{\sin s + \sin d}{\cos d - \cos s} = \frac{\cos \frac{1}{2}(s-d)}{\sin \frac{1}{2}(s-d)} = \cot \frac{1}{2}(s-d).$$

$$(14) \frac{\sin s - \sin d}{\sin(s+d)} = \frac{\cos \frac{1}{2}(s-d)}{\cos \frac{1}{2}(s+d)}.$$

$$(15) \frac{\sin s + \sin d}{\sin(s-d)} = \frac{\sin \frac{1}{2}(s+d)}{\sin \frac{1}{2}(s-d)}.$$

$$(16) \frac{\sin s - \sin d}{\cos s + \cos d} = \frac{\sin \frac{1}{2}(s-d)}{\cos \frac{1}{2}(s-d)} = \tan \frac{1}{2}(s-d).$$

$$(17) \frac{\sin s - \sin d}{\cos d - \cos s} = \frac{\cos \frac{1}{2}(s+d)}{\sin \frac{1}{2}(s+d)} = \cot \frac{1}{2}(s+d).$$

$$(18) \frac{\sin s - \sin d}{\sin(s+d)} = \frac{\sin \frac{1}{2}(s-d)}{\sin \frac{1}{2}(s+d)}.$$

$$(19) \frac{\sin s - \sin d}{\sin(s-d)} = \frac{\cos \frac{1}{2}(s+d)}{\cos \frac{1}{2}(s-d)}.$$

$$(20) \frac{\cos s + \cos d}{\cos d - \cos s} = \frac{\cot \frac{1}{2}(s+d)}{\tan \frac{1}{2}(s-d)}.$$

$$(21) \frac{\cos s + \cos d}{\sin(s+d)} = \frac{\cos \frac{1}{2}(s-d)}{\sin \frac{1}{2}(s+d)}.$$

$$(22) \frac{\cos s - \cos d}{\sin(s-d)} = \frac{\cos \frac{1}{2}(s+d)}{\sin \frac{1}{2}(s-d)}.$$

$$(23) \frac{\cos d - \cos s}{\sin(s+d)} = \frac{\sin \frac{1}{2}(s-d)}{\cos \frac{1}{2}(s+d)}.$$

$$(24) \frac{\cos d - \cos s}{\sin(s-d)} = \frac{\sin \frac{1}{2}(s+d)}{\cos \frac{1}{2}(s-d)}.$$

$$(25) \frac{\sin(s+d)}{\sin(s-d)} = \frac{\sin \frac{1}{2}(s+d) \cos \frac{1}{2}(s+d)}{\sin \frac{1}{2}(s-d) \cos \frac{1}{2}(s-d)}.$$

Formula (11) gives the proportion,

$$\sin s + \sin d : \sin s - \sin d :: \tan \frac{1}{2}(s+d) : \tan \frac{1}{2}(s-d).$$

Hence, *The sum of the sines of two angles is to their difference as the tangent of one-half the sum of the angles is to the tangent of one-half their difference.*

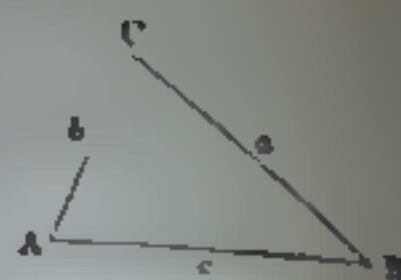
Let us apply this principle in solving triangles when two sides and their included angle are given Article 75.

$$a : b :: \sin A : \sin B.$$

$$\therefore a + b : a - b :: \sin A + \sin B : \sin A - \sin B.$$

$$\sin A + \sin B : \sin A - \sin B :: \tan \frac{1}{2}(A+B) : \tan \frac{1}{2}(A-B).$$

$$\therefore a + b : a - b :: \tan \frac{1}{2}(A+B) : \tan \frac{1}{2}(A-B).$$



97. Theorem.

The square of any side of a triangle is equal to the sum of the squares of the other sides, minus twice their product into the cosine of their included angle.

1st. When the angle is acute.

$$(1) \quad m = b - n.$$

$$(2) \quad m^2 = b^2 + n^2 - 2bn.$$

$$(3) \quad p^2 = p^2.$$

$$(2) + (3) \quad (4) \quad m^2 + p^2 = b^2 + n^2 + p^2 - 2bn.$$

But $m^2 + p^2 = a^2$ and $n^2 + p^2 = c^2$, \therefore (4) becomes

$$(5) \quad a^2 = b^2 + c^2 - 2bn.$$

But $n = c \cos A$, which substituted in (5) gives

$$(6) \quad a^2 = b^2 + c^2 - 2bc \cos A.$$



2d. When the angle is obtuse.

$$(1) \quad m = b + n.$$

$$(2) \quad m^2 = b^2 + n^2 + 2bn.$$

$$(3) \quad p^2 = p^2.$$

$$(2) + (3) \quad (4) \quad m^2 + p^2 = b^2 + n^2 + p^2 + 2bn.$$



But $m^2 + p^2 = a^2$ and $n^2 + p^2 = c^2$, \therefore (4) becomes

$$(5) \quad a^2 = b^2 + c^2 + 2bn.$$

But $n = c \cos BAD = -c \cos BAC = -c \cos A$.

$$\therefore (6) \quad a^2 = b^2 + c^2 - 2bc \cos A.$$

98. Problem.

To find the angles of a triangle when the sides are given.

From either formula (6) of the last article we have

$$(1) \quad \cos A = \frac{b^2 + c^2 - a^2}{2bc}.$$

Hence, The co-sine of any angle of a triangle is equal to the sum of the squares of the adjacent sides, minus the square of the opposite side, divided by twice the rectangle of the adjacent sides.

Formula (1) gives the natural co-sine of A ; hence, A can be found. But it is best to place the formula under such a form as to adapt it to logarithmic computation.

Adding 1 to both members of (1) we have

$$(2) \quad 1 + \cos A = \frac{(b + c)^2 - a^2}{2bc} = \frac{(a + b + c)(b + c - a)}{2bc}.$$

But $1 + \cos A = 2 \cos^2 \frac{1}{2}A$. Article 95, (10).

$$\text{Let } a + b + c = p, \text{ then } \frac{(a + b + c)(b + c - a)}{2bc} = \frac{p(p - 2a)}{2bc}.$$

Substituting these values in (2), and dividing by 2, we have

$$(3) \quad \cos^2 \frac{1}{2}A = \frac{\frac{1}{2}p(\frac{1}{2}p - a)}{bc}.$$

$$\sqrt{(3)} = (4) \quad \cos \frac{1}{2}A = \sqrt{\frac{\frac{1}{2}p(\frac{1}{2}p - a)}{bc}}$$

In like manner, (5) $\cos \frac{1}{2} B = \sqrt{\frac{\frac{1}{2} p - \frac{1}{2} p - b}{ac}}$.

Also, (6) $\cos \frac{1}{2} C = \sqrt{\frac{\frac{1}{2} p - \frac{1}{2} p - c}{ab}}$.

Introducing R , applying logarithms, and reducing, 4 becomes

$$\log \cos \frac{1}{2} A = \frac{1}{2} [\log \frac{1}{2} p + \log (\frac{1}{2} p - a) + a.c. \log b + a.c. \log c]$$

In like manner introduce R and apply logarithms to 5 and 6.

By subtracting both members of (1) from 1 and reducing we find

$$(7) \sin \frac{1}{2} A = \sqrt{\frac{(\frac{1}{2} p - b)(\frac{1}{2} p - c)}{\frac{1}{2} p(\frac{1}{2} p - a)}}$$

$$(8) \sin \frac{1}{2} B = \sqrt{\frac{(\frac{1}{2} p - a)(\frac{1}{2} p - c)}{\frac{1}{2} p(\frac{1}{2} p - b)}}$$

$$(9) \sin \frac{1}{2} C = \sqrt{\frac{(\frac{1}{2} p - a)(\frac{1}{2} p - b)}{\frac{1}{2} p(\frac{1}{2} p - c)}}$$

$$(7) \div (4) = (10) \tan \frac{1}{2} A = \sqrt{\frac{(\frac{1}{2} p - b)(\frac{1}{2} p - c)}{\frac{1}{2} p(\frac{1}{2} p - a)}}$$

$$(8) \div (5) = (11) \tan \frac{1}{2} B = \sqrt{\frac{(\frac{1}{2} p - a)(\frac{1}{2} p - c)}{\frac{1}{2} p(\frac{1}{2} p - b)}}$$

$$(9) \div (6) = (12) \tan \frac{1}{2} C = \sqrt{\frac{(\frac{1}{2} p - a)(\frac{1}{2} p - b)}{\frac{1}{2} p(\frac{1}{2} p - c)}}$$

99. Examples.

$$1. \text{ Given } \begin{cases} a = 125 \\ b = 150 \\ c = 100 \end{cases} \quad \text{Required } \begin{cases} A = 55^\circ 46' 18'' \\ B = 82^\circ 49' 08'' \\ C = 41^\circ 24' 34'' \end{cases}$$

$$2. \text{ Given } \begin{cases} a = 864 \\ b = 1308 \\ c = 1086 \end{cases} \quad \text{Required } \begin{cases} A = 41^\circ 00' 38'' \\ B = 83^\circ 25' 14'' \\ C = 55^\circ 34' 08'' \end{cases}$$

100. Problem.

To find the area of a triangle when two sides and their included angle are given.

Let k denote the area of the triangle ABC , of which the two sides b and c and their included angle A are given.



$$(1) 2k = bp.$$

$$(2) p = c \sin A.$$

$$\therefore (3) 2k = bc \sin A.$$

Introducing R , and applying logarithms, we have

$$\log (2k) = \log b + \log c + \log \sin A - 10.$$

101. Examples.

1. Two sides of a triangle are 345.6 and 485, respectively, and their included angle is $38^\circ 45' 40''$; what is the area?
Ans. 52468.

2. Two sides of a triangle are 784.25 and 1095.8, respectively, and their included angle is $85^\circ 40' 20''$; what is the area.
Ans. 428470.

102. Problem.

To find the area of a triangle when the three sides are given.

By the last problem we find

$$(1) k = \frac{1}{2} bc \sin A,$$

$$(2) \sin A = 2 \sin \frac{1}{2} A \cos \frac{1}{2} A \quad \text{Article 95, (5),}$$

$$(3) \sin \frac{1}{2} A = \sqrt{\frac{(\frac{1}{2} p - b)(\frac{1}{2} p - c)}{bc}} \quad \text{Article 98, (7),}$$

$$\begin{aligned}
 (4) \quad \cos \frac{1}{2} A &= \sqrt{\frac{\frac{1}{2} p (\frac{1}{2} p - a)}{bc}}, \text{ Article 98, (4).} \\
 (5) \quad \sin A &= \frac{2 \sqrt{\frac{1}{2} p (\frac{1}{2} p - a) (\frac{1}{2} p - b) (\frac{1}{2} p - c)}}{bc} \\
 (6) \quad k &= \sqrt{\frac{1}{2} p (\frac{1}{2} p - a) (\frac{1}{2} p - b) (\frac{1}{2} p - c)}.
 \end{aligned}$$

103. Examples.

1. The sides of a triangle are 40, 45, 55, required the area.
Ans. 887.412.

2. The sides of a triangle are 467, 845, 756, required the area.
Ans. 175508.

104. Problem.

Given the perimeter and angles of a triangle, required the sides.

$$(1) \quad \frac{b}{a} = \frac{\sin B}{\sin A}, \quad (2) \quad \frac{c}{a} = \frac{\sin C}{\sin A}.$$

Adding and reducing by Articles 96, (5) and 95, (5), we have

$$(3) \quad \frac{b+c}{a} = \frac{\sin \frac{1}{2}(B+C) \cos \frac{1}{2}(B-C)}{\sin \frac{1}{2} A \cos \frac{1}{2} A}.$$

$\sin \frac{1}{2}(B+C) = \cos \frac{1}{2} A$, and $\sin \frac{1}{2} A = \cos \frac{1}{2}(B+C)$.

$$\therefore (3) \quad \frac{b+c}{a} = \frac{\cos \frac{1}{2}(B-C)}{\cos \frac{1}{2}(B+C)}.$$

Adding 1 to both members, we have

$$(4) \quad \frac{a+b+c}{a} = \frac{\cos \frac{1}{2}(B+C) + \cos \frac{1}{2}(B-C)}{\cos \frac{1}{2}(B+C)}.$$

Let $p = \frac{1}{2}(a+b+c)$, and reduce by 96, (7), we have

$$(5) \quad \frac{p}{a} = \frac{2 \cos \frac{1}{2} B \cos \frac{1}{2} C}{\sin \frac{1}{2} A}.$$

$$\therefore (6) \quad a = \frac{\frac{1}{2} p \sin \frac{1}{2} A}{\cos \frac{1}{2} B \cos \frac{1}{2} C}.$$

Introducing R and applying logarithms, we have

$$\begin{aligned}
 \log a &= \log \frac{1}{2} p + \log \sin \frac{1}{2} A + \\
 &\quad a. c. \log \cos \frac{1}{2} B + a. c. \log \cos \frac{1}{2} C - 10.
 \end{aligned}$$

Similar formulas can be found for b and c . But, after a is found, b and c can be more readily found by article 69.

105. Examples.

1. Given $p = 150$, $A = 70^\circ$, $B = 60^\circ$, $C = 50^\circ$, required a , b , c .

$$\text{Ans. } a = 54.81, b = 50.51, c = 44.68.$$

2. Given $p = 31234.36$, $A = 35^\circ 45'$, $B = 45^\circ 28'$, $C = 98^\circ 47'$, required a , b , c .

$$\text{Ans. } a = 7985, b = 9742.5, c = 13506.86.$$

3. Given $p = 375$, $A = 55^\circ 46' 18''$, $B = 82^\circ 49' 08''$, $C = 41^\circ 21' 34''$, required a , b , c .

$$\text{Ans. } a = 125, b = 150, c = 100.$$

106. Problem.

Given the three sides of a triangle, to find the radius of the inscribed circle.

$$(1) \quad BOC + AOC + AOB = ABC.$$

$$(2) \quad BOC = \frac{1}{2} ar.$$

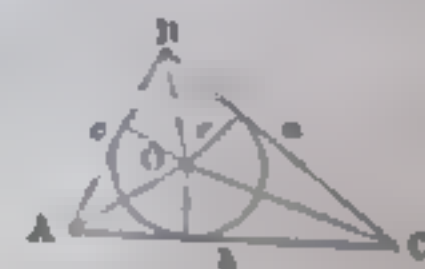
$$(3) \quad AOC = \frac{1}{2} br.$$

$$(4) \quad AOB = \frac{1}{2} cr.$$

$$\therefore (5) \quad BOC + AOC + AOB = \frac{1}{2} (a+b+c) r = \frac{1}{2} pr.$$

$$\text{But (6) } ABC = \sqrt{\frac{1}{2} p (\frac{1}{2} p - a) (\frac{1}{2} p - b) (\frac{1}{2} p - c)}.$$

S. N. P.



$$\therefore (7) \quad \frac{1}{2}pr = \frac{1}{2}p(\frac{1}{2}p-a)(\frac{1}{2}p-b)(\frac{1}{2}p-c).$$

$$\therefore (8) \quad r = \sqrt{\frac{\frac{1}{2}p-a}{\frac{1}{2}p} \cdot \frac{\frac{1}{2}p-b}{\frac{1}{2}p} \cdot \frac{\frac{1}{2}p-c}{\frac{1}{2}p}} = \frac{k}{\frac{1}{2}p}.$$

107. Examples.

1. The three sides of a triangle are 20, 30, 40, respectively, required the radius of the inscribed circle.

Ans. 6.455.

2. The three sides of a triangle are 100, 150, 200, respectively, required the radius of the inscribed circle.

Ans. 32.275.

108. Problem.

Given the three sides of a triangle to find the radius of the circumscribed circle.

Let O be the center of the circle, and R the radius.

Let OD be perpendicular to b , then
 $AD = \frac{b}{2}$.

The angle $O =$ the angle B , since each is measured by one-half the arc AC .

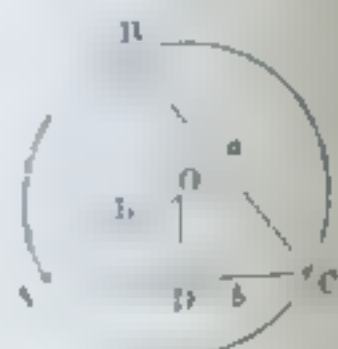
$$(1) \quad AD = \frac{b}{2} = AO \sin O = R \sin B.$$

$$\therefore (2) \quad R = \frac{b}{2 \sin B}.$$

$$\sin B = 2 \sin \frac{1}{2}B \cos \frac{1}{2}B = \frac{2}{a} \frac{\frac{1}{2}p(\frac{1}{2}p-a)}{\frac{1}{2}p(\frac{1}{2}p-b)(\frac{1}{2}p-c)}.$$

$$\therefore (3) \quad R = \frac{abc}{4 \sqrt{\frac{1}{2}p(\frac{1}{2}p-a)(\frac{1}{2}p-b)(\frac{1}{2}p-c)}} = \frac{abc}{4k}.$$

Prove that the formula will be the same if the center is without the triangle.



109. Examples.

1. The sides of a triangle are 7, 9, 10, respectively, required the radius of the circumscribed circle.

Ans. 5.118.

2. The sides of a triangle are 50, 60, 70, respectively, required the radius of the circumscribed circle.

Ans. 35.72.

110. Theorem.

The perpendicular let fall on either side of a triangle from the vertex of the opposite angle is equal to that side into the product of the sines of the adjacent angles divided by the sine of the sum of those angles.

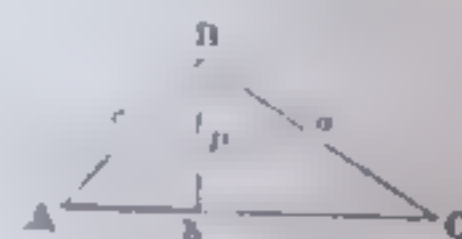
$$(1) \quad p = c \sin A.$$

$$(2) \quad \sin B : \sin C :: b : c, \therefore c = \frac{b \sin C}{\sin B}.$$

$$\therefore (3) \quad p = \frac{b \sin A \sin C}{\sin B}.$$

$$(4) \quad \sin B = \sin [180^\circ - (A + C)] = \sin (A + C).$$

$$\therefore (5) \quad p = \frac{b \sin A \sin C}{\sin (A + C)}.$$



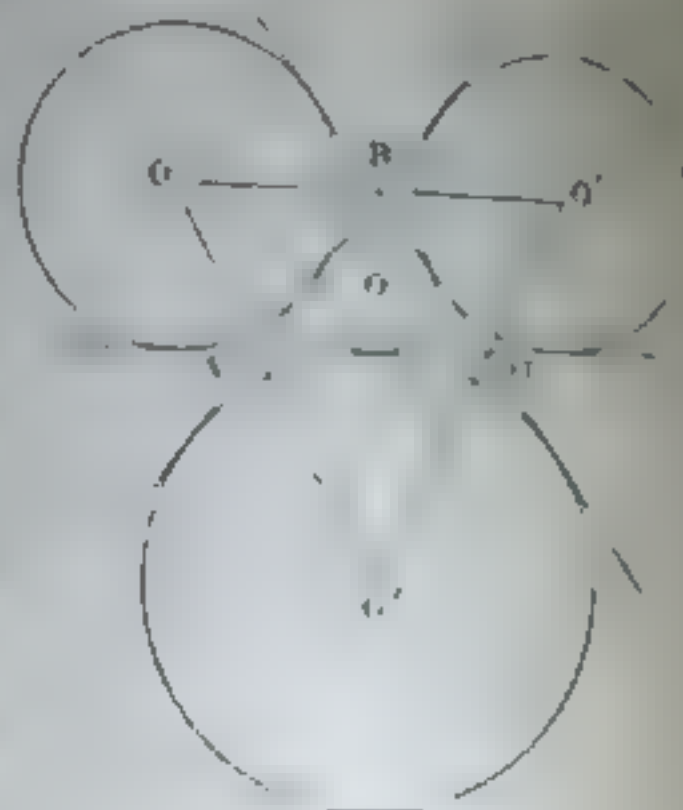
111. Problem.

Given the three sides of a triangle to find the radii of the escribed circles.

The escribed circles are the three circles external to the triangle, each tangent to one side and to the prolongation of the other sides.

The centers of the escribed circles are the points of intersection of the lines bisecting the external angles.

The radii r' , r'' , r''' , of the escribed circles, will be the perpendiculars let fall from their centers O' , O'' , O''' , respectively, on the three sides a , b , c .



Hence, by the last article,

$$(1) \quad r' = \frac{a \sin (90^\circ - \frac{1}{2}B) \sin (90^\circ - \frac{1}{2}C)}{\sin [180^\circ - \frac{1}{2}(B + C)]}$$

$$\therefore (2) \quad r' = \frac{a \cos \frac{1}{2}B \cos \frac{1}{2}C}{\cos \frac{1}{2}A} = \frac{1}{2}p \tan \frac{1}{2}A. \quad \text{Art. 104.}$$

Substituting the value of $\tan \frac{1}{2}A$, article 98, we have

$$(3) \quad r' = \sqrt{\frac{\frac{1}{2}p(\frac{1}{2}p-b)(\frac{1}{2}p-c)}{\frac{1}{2}p-a}} = \frac{k}{\frac{1}{2}p-a}.$$

$$\therefore (4) \quad r'' = \sqrt{\frac{\frac{1}{2}p(\frac{1}{2}p-a)(\frac{1}{2}p-c)}{\frac{1}{2}p-b}} = \frac{k}{\frac{1}{2}p-b}.$$

$$\therefore (5) \quad r''' = \sqrt{\frac{\frac{1}{2}p(\frac{1}{2}p-a)(\frac{1}{2}p-b)}{\frac{1}{2}p-c}} = \frac{k}{\frac{1}{2}p-c}.$$

112. Examples.

* 1. Given the sides of a triangle, 6, 9, 11, required the radii of the three escribed circles.

Ans. 3.854, 6.745, 13.49.

2. Given $p = 100$, $A = 55^\circ$, $B = 60^\circ$, $C = 65^\circ$, required the radii of the three escribed circles.

[See (2), Art. 111.] *Ans.* 26.028, 28.867, 31.854.

113. Theorem.

The product of the radius of the inscribed circle and the radii of the three escribed circles is equal to the square of the area of the triangle.

The product of (8), article 106, and (3), (4), (5), article 111, gives

$$rr'r'r'' = \frac{k^4}{\frac{1}{2}p(\frac{1}{2}p-a)(\frac{1}{2}p-b)(\frac{1}{2}p-c)} = \frac{k^4}{k^2} = k^2.$$

114. Theorem.

The reciprocal of the radius of the inscribed circle, the sum of the reciprocals of the radii of the escribed circles, and the sum of the reciprocals of the perpendiculars let fall from the vertices of the three angles on the opposite sides of a triangle are equal to each other.

Taking the reciprocal of (8), article 106, we have

$$(1) \quad \frac{1}{r} = \frac{p}{2k}.$$

Taking the sum of the reciprocals of (3), (4), (5), article 111,

$$(2) \quad \frac{1}{r'} + \frac{1}{r''} + \frac{1}{r'''} = \frac{p-2a}{2k} + \frac{p-2b}{2k} + \frac{p-2c}{2k} = \frac{p}{2k}.$$

Let p' , p'' , p''' , respectively, be the perpendiculars let fall from the vertices of the three angles on the sides a , b , and c . Then we have

$$ap' = 2k. \quad \therefore \quad \frac{1}{p'} = \frac{a}{2k}.$$

In like manner, $\frac{1}{p''} = \frac{b}{2k}$. Also, $\frac{1}{p'''} = \frac{c}{2k}$.

$$(3) \quad \frac{1}{p} = \frac{1}{p'} + \frac{1}{p''} = \frac{a+b+c}{2k} = \frac{p}{2k}.$$

$$\therefore (4) \quad \frac{1}{r} = \frac{1}{r'} + \frac{1}{r''} + \frac{1}{r'''} = \frac{1}{p'} + \frac{1}{p''} + \frac{1}{p'''}.$$

115. Problem.

To find the distance between the centers of the circumscribed and inscribed circles of a triangle.

Let R and r be the radii, and P and O the centers of the circles, and let $D = OP$.

Draw PE perpendicular to AC . The angle $APE = B$, since each is measured by one-half the arc AC ; but $PAE = 90^\circ - APE$, $\therefore PAE = 90^\circ - B$. $OAC = \frac{1}{2}A$. $PAO = PAE - OAC$.

$$\therefore PAO = 90^\circ - B - \frac{1}{2}A = \frac{1}{2}(C - B). \quad AO = \frac{r}{\sin \frac{1}{2}A}.$$

$$(1) \quad OP^2 = AP^2 + AO^2 - 2 AP \times AO \cos PAO. \quad \text{Art. 97.}$$

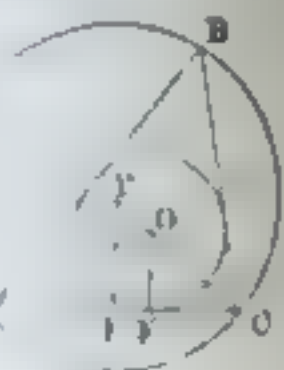
Substituting the values of OP , AP , AO , and PAO , we have

$$(2) \quad D^2 = R^2 + \frac{r^2}{\sin^2 \frac{1}{2}A} - \frac{2 Rr \cos \frac{1}{2}(C - B)}{\sin \frac{1}{2}A}.$$

$$(3) \quad R = \frac{b}{2 \sin B} = \frac{b}{4 \sin \frac{1}{2}B \cos \frac{1}{2}B}. \quad \text{Arts. } \begin{cases} 108, (2). \\ 95, (5). \end{cases}$$

$$(4) \quad r = \frac{b \sin \frac{1}{2}A \sin \frac{1}{2}C}{\sin \frac{1}{2}(A + C)} = \frac{b \sin \frac{1}{2}A \sin \frac{1}{2}C}{\cos \frac{1}{2}B}. \quad \text{Art. 110.}$$

$$\therefore (5) \quad \frac{r^2}{\sin^2 \frac{1}{2}A} = \frac{4 Rr \sin \frac{1}{2}B \sin \frac{1}{2}C}{\sin \frac{1}{2}A}.$$



Substituting in (2), and reducing by article 91, (d), and 89, (b), we have

$$(6) \quad D^2 = R^2 - \frac{2 Rr \cos \frac{1}{2}(B + C)}{\sin \frac{1}{2}A} = R^2 - 2 Rr.$$

$$\therefore (7) \quad D = \sqrt{R^2 - 2 Rr}.$$

116. Examples.

1. The sides of a triangle are 12, 13, 15; required the distance between the centers of the circumscribed and inscribed circles. *Ans.* 1.616.

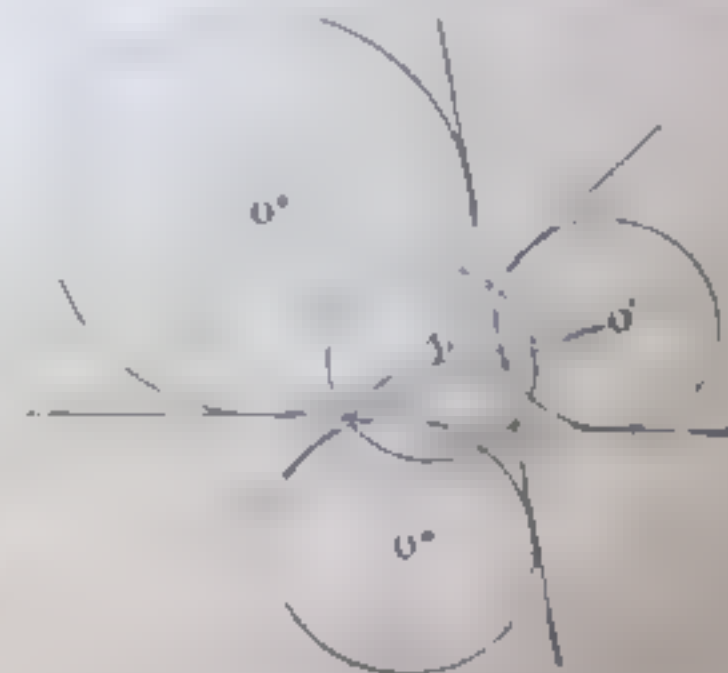
2. Two sides of a triangle are 35 and 37, and their included angle is 50° ; required the distance between the centers of the circumscribed and inscribed circles. *Ans.* 3.266.

3. The perimeter of a triangle is 120, the angles are 40° , 60° , and 80° , respectively; required the distance between the centers of the circumscribed and inscribed circles. *Ans.* 8.353.

117. Problem.

To find the distance between the centers of the circumscribed and escribed circles.

Let r' , r'' , r''' be the radii of the escribed circles, and D , D' , D'' , be the distances of their centers, O' , O'' , O''' , respectively, from P , the center of the circumscribed circle, whose radius is R .



As in the last Problem, we find

$$(1) \quad D^2 = R^2 + \frac{r'^2}{\sin^2 \frac{1}{2}A} - \frac{2 R r' \cos \frac{1}{2}(C-B)}{\sin \frac{1}{2}A}.$$

$$(2) \quad R = \frac{a}{2 \sin \frac{1}{2}A} = \frac{a}{4 \sin \frac{1}{2}A \cos \frac{1}{2}A} \quad \text{Arts. } \begin{cases} 108, (2) \\ 95, (5) \end{cases}$$

$$(3) \quad r' = \frac{a \cos \frac{1}{2}B \cos \frac{1}{2}C}{\cos \frac{1}{2}A} \quad \text{Art. 111, (2).}$$

$$\therefore (4) \quad \frac{r'^2}{\sin^2 \frac{1}{2}A} = \frac{4 R r' \cos \frac{1}{2}B \cos \frac{1}{2}C}{\sin \frac{1}{2}A}, \text{ by (2) and (3).}$$

Substituting (4) in (1), and reducing by (d) and (b), we have

$$(5) \quad D^2 = R^2 + \frac{2 R r' \cos \frac{1}{2}(B+C)}{\sin \frac{1}{2}A} = R^2 + 2 R r'.$$

$$\therefore (6) \quad D = \sqrt{R^2 + 2 R r'}.$$

$$\therefore (7) \quad D' = \sqrt{R^2 + 2 R r''}.$$

$$\therefore (8) \quad D'' = \sqrt{R^2 + 2 R r'''}$$

118. Examples.

1. The three sides of a triangle are 21, 23, 26; required the distances from the center of the circumscribed circle to the centers of the three escribed circles. *Ans.* 25.19, 26.64, 29.73.

2. The angles of a triangle are 56° , 60° , 64° , the greatest side is 25; required the distances from the center of the circumscribed circle to the centers of the three escribed circles. *Ans.* 26.96, 27.80, 28.65.

3. Given $p = 100$, $A = 55^\circ$, $B = 60^\circ$, $C = 65^\circ$, required D , D' , D'' . *Ans.* 37.10, 38.55, 40.01.

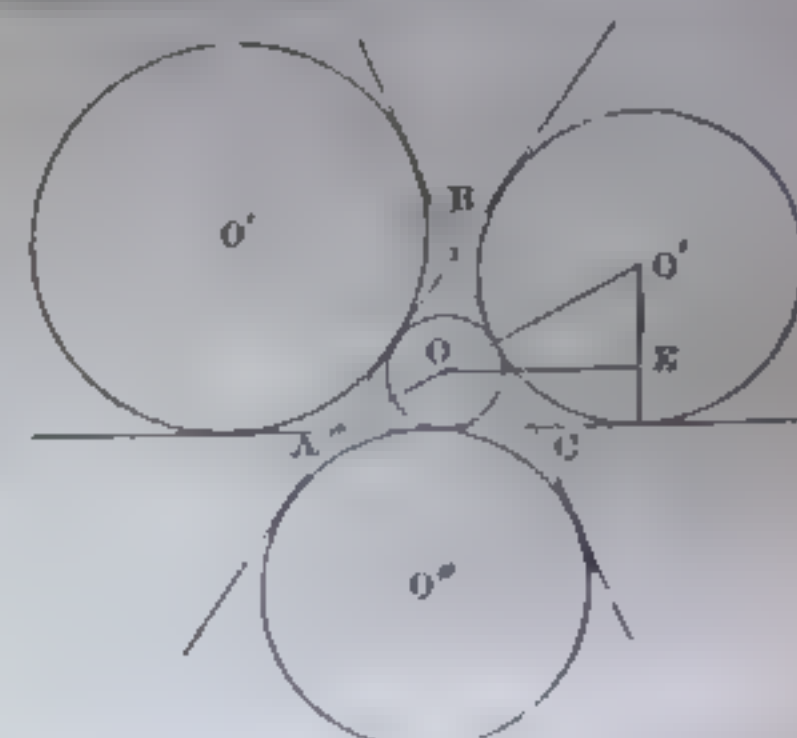
119. Problem.

To find the distance between the centers of the inscribed and escribed circles.

Let D_1 , D_2 , D_3 , be the distances.

In the triangle $OO'E$, we have

$$(1) \quad D_1 = \frac{r' - r}{\sin \frac{1}{2}A}.$$



Substituting the values of r' , r , and $\sin \frac{1}{2}A$, we have

$$(2) \quad D_1 = \frac{a}{\sqrt{\frac{1}{2}p(\frac{1}{2}p - a)}}.$$

$$(3) \quad D_2 = \frac{b}{\sqrt{\frac{1}{2}p(\frac{1}{2}p - b)}}.$$

$$(4) \quad D_3 = \frac{c}{\sqrt{\frac{1}{2}p(\frac{1}{2}p - c)}}.$$

120. Examples.

1. The three sides of a triangle are 30, 50, 60; required the distances between the centers of the inscribed and escribed circles. *Ans.* 31.05, 56.69, 87.83.

2. The sides of a triangle are 500, 600, 700; required the sides of the triangle formed by joining the centers of the inscribed and circumscribed circles and the center of the escribed circle, tangent to the sides 600 and 700 produced. *Ans.* 540.06, 104.58, 624.58.

121. Miscellaneous Exercises.

1. Prove that $\sin 15^\circ = \frac{1}{2} \frac{3 - 1}{2}$, $\cos 15^\circ = \frac{1}{2} \frac{3 + 1}{2}$,

$\tan 15^\circ = \frac{2 - 1}{2 + 1}$, $\cot 15^\circ = \frac{2 + 1}{2 - 1}$, $\sec 15^\circ = \frac{2 + 1}{2 - 1}$, $\csc 15^\circ = \frac{2 + 1}{2 - 1}$.

2. Find the sine and co-sine of 75° .

Ans. $\sin 75^\circ = \frac{1}{2} \frac{3 + 1}{2}$, $\cos 75^\circ = \frac{1}{2} \frac{3 - 1}{2}$.

3. Why is $\sin 75^\circ = \cos 15^\circ$, and $\cos 75^\circ = \sin 15^\circ$?

4. How may the values of tangent, co-tangent, secant, and co-secant of 75° be found from the values of the sine and co-sine?

5. Find the functions of 150° .

Ans. $\sin 150^\circ = \frac{1}{2}$, $\cos 150^\circ = -\frac{1}{2}$, ...

6. Given $\sin a + \cos a = \sqrt{2}$, to find a .

Ans. 45° , or $45^\circ + 360^\circ$; or, in general, $\frac{\pi}{4} + 2\pi n$.

7. Given $\sin 2a = \cos a$, to find a .

Ans. $\frac{\pi}{6} + 2\pi n$, or $\frac{1}{3}\pi + 2\pi n$.

8. Prove that the sum of the tangents of the three angles of a plane triangle is equal to their product.

9. Prove that the sum of the co-tangents of one-half the angles of a plane triangle is equal to their product.

10. Prove that ABC is isosceles if $\cos A = \frac{\sin B}{2 \sin C}$.

11. Prove that the sum of the diameters of the inscribed and circumscribed circles of any plane triangle ABC is

$$a \cot A + b \cot B + c \cot C.$$

12. If b is the base of the triangle ABC , p , the perpendicular to the base from the vertex of the opposite angle, and s , the sum of the sides a and c , prove that

$$\tan \frac{1}{2}B = \frac{2bp}{(s+b)(s-b)}.$$

13. If b is the base of the triangle ABC , p , the perpendicular to the base from the vertex of the opposite angle, and d , the difference of the sides a and c , prove that

$$\tan \frac{1}{2}B = \frac{(b+d)(b-d)}{2bp}.$$

14. If a , b , and c be the sides of the triangle ABC , s , the sum of the sides a and c , and r , the radius of the inscribed circle, prove that

$$\tan \frac{1}{2}B = \frac{2r}{s-b}.$$

122. Computation of Natural Functions.

Dividing the length of the semi-circumference to the radius 1, which is $\pi = 3.141592653589793...$ by 1080, the number of minutes in 180° , the quotient, which is .0002908882..., will be the length of the arc $1'$, and will differ insensibly from its sine.

$$\therefore (1) \sin 1' = .0002908882.$$

$$\therefore (2) \cos 1' = \sqrt{1 - \sin^2 1'} = .9999999577.$$

Adding (a) and (c), then (b) and (d), articles 89, 91, and transposing,

$$(3) \sin(a+b) = 2 \sin a \cos b - \sin(a-b).$$

$$(4) \cos(a+b) = 2 \cos a \cos b - \cos(a-b).$$

If in (3) and (4) $b = 1$, $a = 1, 2, 3, \dots$, in succession, we have

$$\sin 2' = 2 \cos 1' \sin 1' - \sin 0' = .0005817764.$$

$$\sin 3' = 2 \cos 1' \sin 2' - \sin 1' = .0008726646.$$

$$\sin 4' = 2 \cos 1' \sin 3' - \sin 2' = .0011635526.$$

$$\dots \dots \dots$$

$$\cos 2' = 2 \cos 1' \cos 1' - \cos 0' = .999998308.$$

$$\cos 3' = 2 \cos 1' \cos 2' - \cos 1' = .999996193.$$

$$\dots \dots \dots$$

To facilitate computation, for $2 \cos 1' = 1.999999154$, use its equal, $2 - .000000846$. Then we have

$$\sin 2' = 2 \sin 1' - .000000846 \sin 1' - \sin 0'.$$

$$\sin 3' = 2 \sin 2' - .000000846 \sin 2' - \sin 1'.$$

$$\dots \dots \dots$$

After finding the sines and cosines, the tangents and co-tangents can be calculated from the formulas:

$$(5) \tan a = \frac{\sin a}{\cos a}, \quad (6) \cot a = \frac{\cos a}{\sin a}.$$

It is not necessary to carry the computation beyond 45° , since $\sin a = \cos (90^\circ - a)$, etc.

The logarithmic functions can be found from the corresponding natural functions by the method of article 60.

SPHERICAL TRIGONOMETRY.

123. Definition and Remarks.

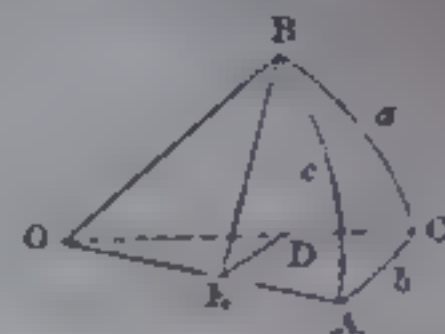
Spherical Trigonometry is that branch of Trigonometry which treats of the solution of spherical triangles.

If any three of the six parts of a spherical triangle are given, the remaining parts can be computed.

The radius of the sphere is taken equal to 1, and

each side has the same numerical measure as the subtended angle whose vertex is at the center of the sphere. Thus,

$$a = BOC, b = AOC, c = AOB.$$



An angle of a spherical triangle is the angle included by the planes of its sides which is measured by the angle included by two lines, one line in one plane, the other in the other, both perpendicular to the common intersection of the planes at the same point.

Thus, if BE , in the plane AOB , is perpendicular to OA , and if ED , in the plane AOC , is perpendicular to OA , then the angle BED will measure the inclination of the planes AOB and AOC , and will be equal to the angle A of the spherical triangle.

RIGHT TRIANGLES.

124. Napier's Circular Parts.

Napier's circular parts are the two sides adjacent to the right angle, the complements of their opposite angles, and the complement of the hypotenuse.

Thus, if HBP is a spherical triangle, right-angled at H , the circular parts are b , p , $90^\circ - B$, $90^\circ - P$, and $90^\circ - h$.



Adjacent parts are those which are not separated by an intervening circular part.

Thus, b and $90^\circ - P$, $90^\circ - P$ and $90^\circ - h$, $90^\circ - h$ and $90^\circ - B$, $90^\circ - B$ and p , p and b are adjacent parts.

The right angle H is not regarded as a circular part, nor as separating the parts b and p .

Opposite parts are those which are separated by an intervening circular part.

Thus, b and $90^\circ - h$, $90^\circ - P$ and $90^\circ - B$, $90^\circ - h$ and p , $90^\circ - B$ and b , p and $90^\circ - P$ are opposite parts.

Any one of these five circular parts is adjacent to two of the remaining parts, and opposite the other two parts.

Of any three circular parts, one part is either adjacent to both the others or opposite both.

A **middle part** is that which is adjacent to two other parts, or opposite two other parts.

125. Exercises.

Tell which is the middle part, and whether the other parts are adjacent to, or opposite, the middle in the following:

- | | |
|---|---|
| 1. $90^\circ - B$, $90^\circ - P$, $90^\circ - h$. | 6. $90^\circ - P$, $90^\circ - h$, p . |
| 2. b , $90^\circ - h$, p . | 7. b , $90^\circ - P$, p . |
| 3. $90^\circ - h$, $90^\circ - B$, p . | 8. $90^\circ - B$, $90^\circ - h$, b . |
| 4. $90^\circ - P$, $90^\circ - B$, b . | 9. $90^\circ - h$, $90^\circ - P$, b . |
| 5. b , $90^\circ - B$, p . | 10. $90^\circ - P$, $90^\circ - B$, p . |

126. Napier's Principles.

1. *The sine of the middle part is equal to the product of the tangents of the adjacent parts.*

Draw BD and DE , respectively perpendicular to OH and OP , and draw BE . BDE is a right angle, since the plane BOH is perpendicular to the plane POH , and BD is perpendicular to OH . The angle BED is equal to P .



$EB = \sin h$, $OE = \cos h$, $DB = \sin p$, and $OD = \cos p$.

$$\frac{ED}{EB} = \frac{OE}{EB} \times \frac{ED}{OE}, \text{ or } \cos P = \cot h \tan b.$$

$$\therefore (1) \sin (90^\circ - P) = \tan (90^\circ - h) \tan b.$$

$$\frac{ED}{OD} = \frac{DB}{OD} \times \frac{ED}{DB}, \text{ or } \sin b = \tan p \cot P.$$

$$\therefore (2) \sin b = \tan p \tan (90^\circ - P).$$

By changing P, b, p into B, p, h , (1) and (2) become

$$(3) \sin (90^\circ - B) = \tan (90^\circ - h) \tan p.$$

$$(4) \sin p = \tan b \tan (90^\circ - B).$$

Multiplying (2) by (4), member by member, we have

$$\sin b \sin p = \tan b \tan p \tan (90^\circ - B) \tan (90^\circ - P).$$

Dividing by $\tan b \tan p$, and reducing, we have

$$\cos b \cos p = \tan (90^\circ - B) \tan (90^\circ - P).$$

$$\cos b \cos p = \cos EOD \times OD = OE = \cos h = \sin (90^\circ - h).$$

$$\therefore (5) \sin (90^\circ - h) = \tan (90^\circ - B) \tan (90^\circ - P).$$

2. *The sine of the middle part is equal to the product of the co-sines of the opposite parts.*

$$OE = \cos EOD \times OD, \text{ or } \cos h = \cos b \cos p.$$

$$\therefore (6) \sin (90^\circ - h) = \cos b \cos p.$$

$$DB = EB \sin DEB, \text{ or } \sin p = \sin h \sin P.$$

$$\therefore (7) \sin p = \cos (90^\circ - h) \cos (90^\circ - P).$$

$$(3) \text{ gives } \sin (90^\circ - B) = \frac{\sin (90^\circ - h) \sin p}{\cos (90^\circ - h) \cos p}.$$

This, by substituting $\cos b \cos p$ for $\sin (90^\circ - h)$, $\cos (90^\circ - h) \cos (90^\circ - P)$ for $\sin p$, and reducing, gives

$$(8) \quad \sin (90^\circ - B) = \cos b \cos (90^\circ - P).$$

By changing p, P, B, b into b, B, P, p , (7) and (8) become

$$(9) \quad \sin b = \cos (90^\circ - h) \cos (90^\circ - B).$$

$$(10) \quad \sin (90^\circ - P) = \cos p \cos (90^\circ - B).$$

These ten formulas are thus reduced to two principles, from which the formulas can be written.

The memory will be further aided by observing the common vowel *a* in the first syllables of the words *tangent* and *adjacent* of the first principle, and the common vowel *o* in the first syllables of the words *co-sine* and *opposite* of the second principle; that is, we take the product of the *tangents* of the parts adjacent to the middle, and the product of the *co-sines* of the parts opposite the middle.

127. Mauduit's Principles.

If we take, as circular parts, the complements of the two sides adjacent to the right angle, their opposite angles, and the hypotenuse, we can readily deduce from the diagram, or from Napier's principles, the following principles:

1. The cosine of the middle part is equal to the product of the co-tangents of the adjacent parts.

2. The cosine of the middle part is equal to the product of the sines of the opposite parts.

Let the ten formulas be written and compared with those of the last article.

128. Analogies of Plane and Spherical Triangles.

The formulas which demonstrate Napier's principles may be placed under forms which will exhibit the analogies existing between Plane and Spherical Triangles, as in the subjoined table.

Plane Right Triangles		Spherical Right Triangles	
1. $\sin P = \frac{p}{h}$		1. $\sin P = \frac{\sin p}{\sin h}$	
2. $\sin B = \frac{b}{h}$		2. $\sin B = \frac{\sin b}{\sin h}$	
3. $\cos P = \frac{a}{b}$		3. $\cos P = \frac{\tan a}{\tan b}$	
4. $\cos B = \frac{a}{h}$		4. $\cos B = \frac{\tan a}{\tan h}$	
5. $\tan P = \frac{p}{a}$		5. $\tan P = \frac{\sin p}{\cos a}$	
6. $\tan B = \frac{b}{a}$		6. $\tan B = \frac{\sin b}{\cos a}$	
7. $\sin P = \cos B$		7. $\sin P = \frac{\cos b}{\cos h}$	
8. $\sin B = \cos P$		8. $\sin B = \frac{\cos p}{\cos h}$	
9. $\cos P = \cos A \cos B$		9. $\cos A = \cos a \cos b$	
10. $\cos A = \cos B \cos P$		10. $\cos A = \sin B \sin P$	

These formulas can be compared and arranged under Napier's principles by those who prefer to do so. The examples will assist the memory.

129. Species of the Parts.

Two parts of a spherical triangle are of the *same* species when both are less than 90° or both greater than 90° .

Two parts of a spherical triangle are of *different* species when one part is less than 90° and the other part greater than 90° .

We shall, at present, consider those triangles only whose parts do not exceed 180° .

Let it be remembered that the sine is positive from 0° to 180° , and that the co-sine, the tangent, and the co-tangent are positive from 0° to 90° and negative from 90° to 180° . Hence, if the co-sines, tangents, or co-tangents of two parts have like signs, these parts will be of the same species; if they have unlike signs, these parts will be of different species.

$$\sin P = \frac{\cos B}{\cos b} \text{ and } \sin B = \frac{\cos P}{\cos p} \quad \text{Art. 128, 7, 8.}$$

Since neither P nor B exceeds 180° , $\sin P$ and $\sin B$ are both positive; hence, $\cos B$ and $\cos b$ have like signs, so also have $\cos P$ and $\cos p$. Therefore, B and b are of the same species; so also are P and p .

Hence, *The sides adjacent to the right angle are of the same species as their opposite angles.*

$$\cos h = \cos b \cos p. \quad \text{Art. 128, 9.}$$

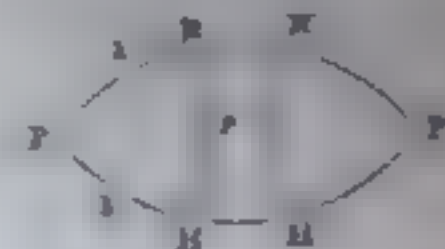
If $h < 90^\circ$, $\cos h$ is positive; hence, $\cos b \cos p$ is positive; $\therefore \cos b$ and $\cos p$ have like signs; $\therefore b$ and p are of the same species; $\therefore B$ and P are of the same species.

Hence, *If the hypotenuse is less than 90° , the two sides adjacent to the right angle are of the same species; so also are their opposite angles.*

If $h > 90^\circ$, $\cos h$ is negative; hence, $\cos b \cos p$ is negative; $\therefore \cos b$ and $\cos p$ have unlike signs; $\therefore b$ and p are of different species; $\therefore B$ and P are of different species.

Hence, *If the hypotenuse is greater than 90° , the two sides adjacent to the right angle are of different species; so also are their opposite angles.*

Let us now investigate the case in which a side adjacent to the right angle and its opposite angle are given.



Let p and P be given. Produce the sides PH and PB till they meet in P' . The angles P and P' are equal, since each is the angle included by the planes of the arcs PHP' and PBP' . Take $P'H' = PH = b$ and $P'B' = PB = h$. The two triangles, PHB and $P'H'P'$, have the two sides PH and PB and the included angle P of the one, equal to $P'H'$ and $P'B'$ and the included angle P' of the other; hence, they are equal in all their corresponding parts; $\therefore H' = H$, $B' = B$, and $H'B' = HB$. But H is a right angle; $\therefore H'$ is a right angle. Hence, the triangle $PH'B'$ or $PH'P'$, will answer to the given conditions.

Since $P'H'$ and PH are equal, and $P'H'$ and PH' are supplements of each other, PH and PH' are supplements of each other. In like manner it may be shown that PB and PB' are supplements of each other.

When, therefore, a side adjacent to the right angle and an opposite angle are given, there are *apparently* two solutions. The conditions of the problem, however, may be such as to render the two solutions impossible, reduce them to one, or render any solution impossible.

Let us now proceed to investigate these conditions.

1. When $P < 90^\circ$ and $p < P$.

We have from Napier's principles,

$$\sin b = \tan p \tan (90^\circ - P), \text{ or } \sin b = \tan p \cot P$$

Since $P < 90^\circ$ and $p < P$, $\tan p < \tan P$; but we have $\tan P \cot P = 1$; $\therefore \tan p \cot P < 1$; hence, $\sin b < 1$; then $b < 90^\circ$ or $b > 90^\circ$; hence, b may be either of the supplementary arcs PH or PH' which have the same sine equal to $\tan p \cot P$.

If $b < 90^\circ$, since $p < 90^\circ$, $h < 90^\circ$; if $b > 90^\circ$, since $p < 90^\circ$, $h > 90^\circ$. Hence, if $P < 90^\circ$ and $p < P$, either triangle, PHB or $PH'B'$, will satisfy the conditions, and there will be two solutions.

2. When $P < 90^\circ$ and $p = P$.

We have $\sin b = \tan p \cot P$,
as before.

Since $p = P$, $\tan p \cot P = \tan P \cot P = 1$; therefore, $\sin b = 1$; $\therefore b = 90^\circ$, or $PH = 90^\circ$.

From Napier's principles, we have

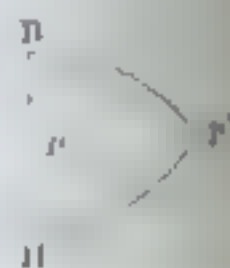
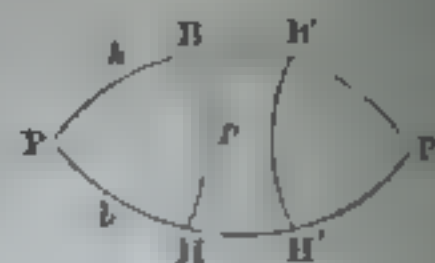
$$\sin (90^\circ - h) = \cos b \cos p, \text{ or } \cos h = \cos b \cos p.$$

Since $b = 90^\circ$, $\cos b = 0$; $\therefore \cos h \cos p = 0$; hence, $\cos h = 0$; $\therefore h = 90^\circ$, or $PH = 90^\circ$.

$\sin (90^\circ - B) = \tan p \tan (90^\circ - h)$, which reduces to $\cos B = \tan p \cot h$.

Since $h = 90^\circ$, $\cot h = 0$; $\therefore \tan p \cot h = 0$
 $\therefore \cos B = 0$; $\therefore B = 90^\circ$.

$$\begin{array}{lll} PH' & 180^\circ & PH & 90^\circ; \therefore PH' = PH. \\ PB' & 180^\circ & PB & 90^\circ; \therefore PB' = PB. \end{array}$$



Hence, if $P < 90^\circ$ and $p = P$, $b = 90^\circ$, $h = 90^\circ$, $B = 90^\circ$, the two triangles reduce to the bi-rectangular triangle PHB , and there is but one solution.

3. When $P < 90^\circ$ and $p > P$.

As before, we have $\sin b = \tan p \cot P$.

Since p and P are of the same species, $p > P$.

Then, if $p > P$, $\tan p > \tan P$; but $\tan P \cot P = 1$, $\therefore \tan p \cot P > 1$; $\therefore \sin b > 1$, which is impossible.

Hence, if $P < 90^\circ$ and $p > P$, no solution is possible.

4. When $P > 90^\circ$ and $p > P$.

We have $\sin b = \tan p \cot P$,
as before. $\tan p$ and $\cot P$ are

both negative, and $\tan p < \tan P$, numerically. But $\tan P \cot P = 1$; $\therefore \tan p \cot P < 1$; $\therefore \sin b < 1$; $\therefore b < 90^\circ$, or $b > 90^\circ$; hence, b may be either of the supplementary arcs PH or PH' which have the common sine equal to $\tan p \cot P$.

If $b < 90^\circ$, since $p > 90^\circ$, $h > 90^\circ$; if $b > 90^\circ$, since $p > 90^\circ$, $h < 90^\circ$.

Hence, if $P > 90^\circ$ and $p > P$, either triangle, PHB or $PH'B'$ will satisfy the conditions, and there will be two solutions.

5. When $P > 90^\circ$ and $p = P$.

We have $\sin b = \tan p \cot P$, as
before.

$$\sin b = \tan P \cot P = 1; \therefore b = 90^\circ$$

$$\cos b = 0; \therefore \cos h = \cos b \cos p = 0$$

$$\therefore \cot h = 0; \therefore \cos B = \tan p \cot h = 0;$$



Hence, if $P > 90^\circ$ and $p = P$, $b = 90^\circ$, $h = 90^\circ$, $B = 90^\circ$, the two triangles reduce to the bi-rectangular PHH , and there is but one solution.

6. When $P > 90^\circ$ and $p < P$.

As before, we have $\sin b = \tan p \cot P$.

Since p and P are of the same species, and since $P > 90^\circ$, $p > 90^\circ$; hence, $\tan p, \cot P$ are both negative, and $\tan p > \tan P$, numerically; but since $\tan P \cot P = 1$, $\tan p \cot P > 1$; $\therefore \sin b > 1$, which is impossible.

Hence, if $P > 90^\circ$ and $p < P$, there is no solution.

7. When $P = 90^\circ$.

$$\tan p = \frac{\sin b}{\cot P} = \frac{\sin b}{0} = \infty; \therefore p = 90^\circ.$$

$$\therefore \cos p = 0; \therefore \cos h = \cos b \cos p = 0; \therefore h = 90^\circ.$$

$$\sin b = \tan p \cot P = \infty \cdot 0; \therefore \sin b \text{ is indeterminate.}$$

$$\sin B = \frac{\cos P}{\cos p} = \frac{0}{0}; \therefore \sin B \text{ is indeterminate.}$$

Hence, if $P = 90^\circ$, then $p = 90^\circ$, $h = 90^\circ$, b and B are indeterminate; the triangle is bi-rectangular, and there is an infinite number of solutions.

Hence, the following results:

$$P < 90^\circ \text{ and } \begin{cases} p < P, & \text{Two solutions.} \\ p = P, & \text{One solution.} \\ p > P, & \text{No solution.} \end{cases}$$

$$P > 90^\circ \text{ and } \begin{cases} p > P, & \text{Two solutions.} \\ p = P, & \text{One solution.} \\ p < P, & \text{No solution.} \end{cases}$$

$$P = 90^\circ \text{ then } \begin{cases} p = 90^\circ, \\ h = 90^\circ, \\ b \text{ indeterminate,} \\ B \text{ indeterminate,} \end{cases} \left. \vphantom{\begin{matrix} p = 90^\circ, \\ h = 90^\circ, \\ b \text{ indeterminate,} \\ B \text{ indeterminate,} \end{matrix}} \right\} \begin{matrix} \text{Infinite number} \\ \text{of solutions} \end{matrix}$$

By a comparison of these results, we find,

1. If p differs more from 90° than P , there will be two solutions.

2. If $p = P$, and $P < 90^\circ$ or $P > 90^\circ$, there will be one solution.

3. If $p = P = 90^\circ$, there will be an infinite number of solutions.

4. If p differs less from 90° than P , there will be no solution.

130. Remarks.

1. Napier's principles render it unnecessary to divide the subject of right-angled spherical triangles into cases.

2. Two parts will be given, and three required.


3. These parts or their complements will be circular parts.

4. Take the two given parts, if they are circular parts, otherwise their complements, and any one part required, if it is a circular part, otherwise its complement, and observe which is the middle part, and whether the other parts are adjacent to, or opposite, the middle part: if adjacent, the first of Napier's principles will give the formula; if opposite, the second.

5. Introduce R and apply logarithms.

6. Apply the principles which determine the species of the required part.

131. Examples.

$$1. \text{ Given } \begin{cases} h = 110^\circ 30' \\ p = 50^\circ 45' \end{cases} \text{ Req } \begin{cases} b \\ B \\ P \end{cases}$$


1. To find b .

From the second of Napier's principles, we have

$$\sin (90^\circ - h) = \cos b \cos p, \text{ or } \cos h = \cos b \cos p.$$

Finding $\cos b$ and introducing R , we have

$$\cos b = \frac{R \cos h}{\cos p}$$

$$\therefore \log \cos b = 10 + \log \cos h - 1 - \log \cos p.$$

$$\log \cos h (110^\circ 30') = 9.54433$$

$$\log \cos p (50^\circ 45') = 9.80120$$

$$\log \cos b = 9.74313 - \therefore b = 123^\circ 36' 31''.$$

Since the hypotenuse is greater than 90° , the sides b and p are of different species; but $p < 90^\circ$; $\therefore b > 90^\circ$. But $\log \cos b$ corresponds to $56^\circ 23' 27''$, and to its supplement $123^\circ 36' 31''$ which must be taken, since $b > 90^\circ$.

The species of b can also be determined by the formula,

$$\cos h = \frac{\cos b}{\cos p}.$$

Since $h > 90^\circ$, $\cos h$ is negative, and since $p < 90^\circ$, $\cos p$ is positive, $\therefore \cos b$ is negative: $\therefore b > 90^\circ$. The signs of the functions may be conveniently indicated by placing the signs after their logarithms.

2. To find B .

$$\sin (90^\circ - B) = \tan p \tan (90^\circ - h),$$

$$\therefore \cos B = \frac{\tan p \cot h}{R}.$$

$$\therefore \log \cos B = \log \tan p + \log \cot h - 10.$$

$$\log \tan p (50^\circ 45') = 10.08776 +$$

$$\log \cot h (110^\circ 30') = 9.57274 -$$

$$\log \cos B = 9.66050 - \therefore B = 117^\circ 14'.$$

Since b and B are of the same species, and since $b > 90^\circ$, $B > 90^\circ$. The species of B can also be determined from the sign of $\cos B$.

3. To find P .

$$\sin p = \cos (90^\circ - h) \cos (90^\circ - P), \text{ or } \sin p = \sin h \sin P.$$

$$\therefore \sin P = \frac{R \sin p}{\sin h};$$

$$\log \sin P = 10 + \log \sin p - \log \sin h.$$

$$\log \sin p (50^\circ 45') = 9.88896 +$$

$$\log \sin h (110^\circ 30') = 9.97159 -$$

$$\log \sin P = 9.91737 - \therefore P = 55^\circ 45' 57''.$$

P is of the same species as p , and since $p < 90^\circ$, $P < 90^\circ$. The species of P can not be determined by the sign of $\sin P$, since the sign of $\sin P$ is plus from 0° to 180° .

$$2. \text{ Given } \begin{cases} h = 94^\circ 05' \\ p = 100^\circ 45' \end{cases} \text{ Req } \begin{cases} b \\ B \\ P \end{cases}$$

$$3. \text{ Given } \begin{cases} h = 110^\circ 46' 26'' \\ B = 80^\circ 10' 36'' \end{cases} \text{ Req } \begin{cases} b \\ p \\ P \end{cases}$$

$$4 \text{ Given } \begin{cases} b & 29^\circ 45' 08'' \\ p & 137^\circ 21' 21'' \end{cases} \text{ Req. } \begin{cases} B & 54^\circ 01' 15'' \\ h & 142^\circ 00' 12'' \\ p & 155^\circ 27' 55'' \end{cases}$$

$$5 \text{ Given } \begin{cases} b & 63^\circ 15' \\ p & 55^\circ 28' \end{cases} \text{ Req. } \begin{cases} h & 75^\circ 13' 01'' \\ B & 67^\circ 27' 01'' \\ p & 58^\circ 25' 45'' \end{cases}$$

$$6 \text{ Given } \begin{cases} B & 52^\circ 32' 55'' \\ p & 66^\circ 20' 40'' \end{cases} \text{ Req. } \begin{cases} h & 70^\circ 23' 41'' \\ b & 48^\circ 24' 18'' \\ p & 59^\circ 38' 27'' \end{cases}$$

$$7 \text{ Giv. } \begin{cases} P = 75^\circ 30' \\ p = 50^\circ 15' \end{cases} \therefore \begin{cases} b = 18^\circ 07' 02'' \text{ or } 161^\circ 52' 58'' \\ h = 52^\circ 34' 31'' \text{ or } 127^\circ 25' 29'' \\ B = 23^\circ 03' 06'' \text{ or } 156^\circ 56' 54'' \end{cases}$$

8. If a line make an angle of 40° with a fixed plane, and a plane embracing this line be perpendicular to the fixed plane, how many degrees from its first position must the plane embracing the line revolve about it in order that it may make an angle of 45° with the fixed plane? *Ans.* $67^\circ 22' 44''$ or $112^\circ 37' 16''$.

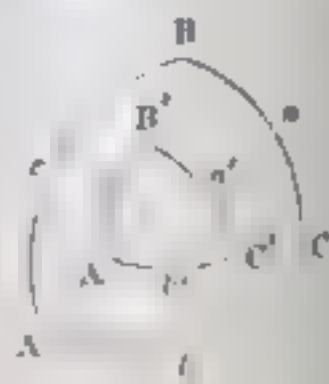
132. Polar Triangles.

The **polar triangle** of a given triangle is the triangle formed by the intersection of three arcs of great circles described about the vertices of the given triangle as poles.

If one triangle is the polar of another, the second is the polar of the first.

Thus, if $A'B'C'$ is the polar of the triangle ABC , then ABC is the polar of $A'B'C'$.

Each angle in one of two polar triangles is the supplement of the side lying opposite to it in the other;



and each side is the supplement of the angle lying opposite to it in the other. Thus,

$$\begin{aligned} A &= 180^\circ - a', & B &= 180^\circ - b', & C &= 180^\circ - c', \\ a &= 180^\circ - A', & b &= 180^\circ - B', & c &= 180^\circ - C', \\ A' &= 180^\circ - a, & B' &= 180^\circ - b, & C' &= 180^\circ - c, \\ a' &= 180^\circ - A, & b' &= 180^\circ - B, & c' &= 180^\circ - C. \end{aligned}$$

Cor.—If $a' = 90^\circ$, $A = 90^\circ$; hence, if one side of a triangle is 90° , one angle of its polar triangle is 90° .

133. Quadrantal Triangles.

A **quadrantal triangle** is a triangle one side of which is 90° .

By the corollary of the last article, it follows that the polar of a quadrantal triangle is a right-angled triangle.

A quadrantal triangle is solved by passing to its polar triangle, which is solved as a right-angled triangle, then by passing back to the quadrantal triangle, which is the polar of the right-angled triangle.

134. Examples.

$$1. \text{ Given } \begin{cases} H = 90^\circ, \\ P = 129^\circ 15', \\ h = 62^\circ 46' 01''. \end{cases} \text{ Req. } \begin{cases} H' = 69^\circ 30', \\ B' = 56^\circ 23' 30'', \\ p' = 124^\circ 14' 03'' \end{cases}$$

Passing to the polar triangle, which is right angled, we have

$$\text{Given } \begin{cases} H = 90^\circ, \\ p = 50^\circ 45', \\ B = 117^\circ 13' 59'', \end{cases} \therefore \begin{cases} h = 110^\circ 30', \\ b = 128^\circ 30' 30'', \\ P = 55^\circ 45' 57''. \end{cases}$$

Passing back to the quadrantal triangle, we find
 $H = 17^\circ 12' 23''$.

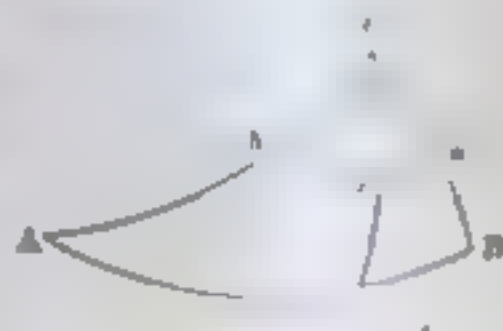
$$\left. \begin{array}{l} a = 74^\circ 26' \\ c = 108^\circ 05' 26'' \\ B = 31^\circ 29' 14'' \end{array} \right\} \text{Req. } \left\{ \begin{array}{l} A' = 74^\circ 26' \\ C' = 108^\circ 05' 26'' \\ B' = 31^\circ 29' 14'' \end{array} \right.$$

OBLIQUE TRIANGLES.

135. Proposition I.

The sines of the sides of a spherical triangle are proportional to the sines of their opposite angles.

Let ABC be a spherical triangle. From C draw p , the arc of a great circle perpendicular to the opposite side or to the opposite side produced.



In the first case we have, by Napier's principles,

$$\sin p = \cos(90^\circ - a) \cos(90^\circ - B) = \sin a \sin B.$$

$$\sin p = \cos(90^\circ - b) \cos(90^\circ - A) = \sin b \sin A.$$

$$\therefore \sin a \sin B = \sin b \sin A.$$

$$\therefore \sin a : \sin b :: \sin A : \sin B.$$

In the second case we have, by Napier's principles,

$$\sin p = \cos(90^\circ - a) \cos(90^\circ - B') = \sin a \sin B' = \sin a \sin B.$$

$$\sin p = \cos(90^\circ - b) \cos(90^\circ - A) = \sin b \sin A.$$

$$\therefore \sin a \sin B = \sin b \sin A.$$

$$\therefore \sin a : \sin b :: \sin A : \sin B.$$



In like manner other proportions may be deduced, giving the group,

$$(1) \sin a : \sin b :: \sin A : \sin B.$$

$$(2) \sin a : \sin c :: \sin A : \sin C.$$

$$(3) \sin b : \sin c :: \sin B : \sin C.$$

136. Proposition II.

The co-sine of any side of a spherical triangle is equal to the product of the co-sines of the other sides, plus the product of their sines into the co-sine of their included angle.

Let ABC be a spherical triangle, and O the center of the sphere.

Let CM be perpendicular to the plane AOB . Draw MD and ME , respectively perpendicular to OB and OA , and

draw CD and CE , which will be respectively perpendicular to OB and OA ; hence, the angle $CEM = A$, and $CDM = B$. Draw EF perpendicular to OB , and MN perpendicular to EF . Each of the angles MEN and EOF is the complement of OEF ; $\therefore MEN = EOF$.

$$OD = OF + NM.$$

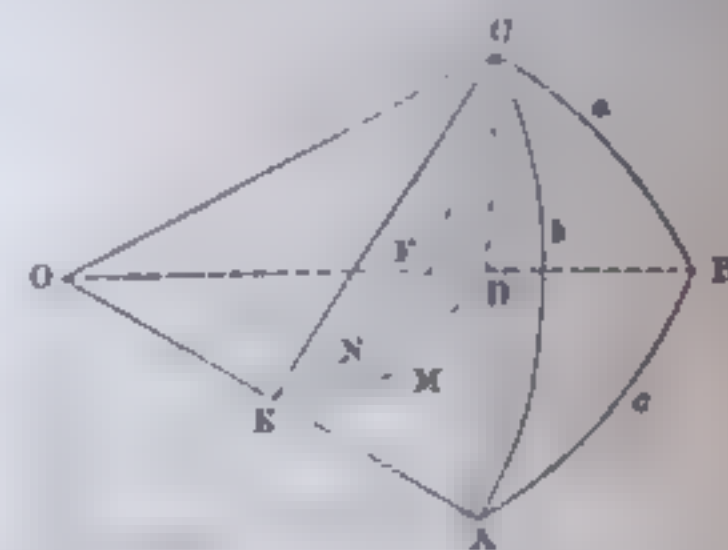
$$OD = \cos a.$$

$$OF = OE \cos EOF = \cos b \cos c.$$

$$NM = EM \sin MEN = \sin b \cos A \sin c.$$

Substituting the values of OD , OF , and NM , we have

$$\cos a = \cos b \cos c + \sin b \sin c \cos A.$$



Let a number other formulas may be deduced, giving the same result.

$$\begin{aligned} 1. \quad \cos a &= \cos b \cos c + \sin b \sin c \cos A, \\ 2. \quad \cos b &= \cos a \cos c + \sin a \sin c \cos B, \\ 3. \quad \cos c &= \cos a \cos b + \sin a \sin b \cos C. \end{aligned}$$

137. Proposition III.

The cosine of any angle of a spherical triangle is equal to the product of the sines of the other angles into the cosine of their included side, minus the product of the cosines of these angles.

The formulas for passing to the polar triangle are,

$$\begin{aligned} a &= 180^\circ - A', \quad b = 180^\circ - B', \quad c = 180^\circ - C', \\ A &= 180^\circ - a', \quad B = 180^\circ - b', \quad C = 180^\circ - c'. \end{aligned}$$

Substituting these values in the formulas of the preceding article and reducing, we have

$$\begin{aligned} -\cos A' &= \cos B' \cos C' - \sin B' \sin C' \cos a', \\ -\cos B' &= \cos A' \cos C' - \sin A' \sin C' \cos b', \\ -\cos C' &= \cos A' \cos B' - \sin A' \sin B' \cos c'. \end{aligned}$$

Changing the signs and omitting the accents, since the formulas are true for any triangle, we have

$$\begin{aligned} 1. \quad \cos A &= \sin B \sin C \cos a - \cos B \cos C, \\ 2. \quad \cos B &= \sin A \sin C \cos b - \cos A \cos C, \\ (3) \quad \cos C &= \sin A \sin B \cos c - \cos A \cos B. \end{aligned}$$

138. Proposition IV.

The cosine of one half of any angle of a spherical triangle is equal to the square root of the quotient obtained by

adding the sine of one-half the sum of the sides into the sine of one-half the sum minus the side opposite the angle, by the product of the sines of the adjacent sides.

The first formula of article 136 gives

$$\cos A = \frac{\cos a - \cos b \cos c}{\sin b \sin c}.$$

Adding 1 to both members, we have

$$1 + \cos A = \frac{\cos a + \sin b \sin c - \cos b \cos c}{\sin b \sin c}.$$

$$1 + \cos A = 2 \cos^2 \frac{1}{2} A. \quad \text{Article 95, (10).}$$

$$\sin b \sin c - \cos b \cos c = -\cos(b + c). \quad \text{Art. 89, (b).}$$

$$\therefore 2 \cos^2 \frac{1}{2} A = \frac{\cos a - \cos(b + c)}{\sin b \sin c}.$$

But by article 96, (8), we have

$$\cos a - \cos(b + c) = 2 \sin \frac{1}{2}(a + b + c) \sin \frac{1}{2}(b + c - a).$$

Substituting and dividing by 2, we have

$$\cos^2 \frac{1}{2} A = \frac{\sin \frac{1}{2}(a + b + c) \sin \frac{1}{2}(b + c - a)}{\sin b \sin c}.$$

Let $s = a + b + c$, then will $\frac{1}{2}s = \frac{1}{2}(a + b + c)$,
 $\frac{1}{2}s - a = \frac{1}{2}(b + c - a)$.

Substituting in the value of $\cos^2 \frac{1}{2} A$, and in the similar values for $\cos^2 \frac{1}{2} B$ and $\cos^2 \frac{1}{2} C$, and extracting the square root, we have

$$(1) \quad \cos \frac{1}{2} A = \sqrt{\frac{\sin \frac{1}{2}s \sin (\frac{1}{2}s - a)}{\sin b \sin c}}.$$

$$(2) \quad \cos \frac{1}{2} B = \sqrt{\frac{\sin \frac{1}{2}s \sin (\frac{1}{2}s - b)}{\sin a \sin c}}.$$

$$(3) \quad \cos \frac{1}{2} C = \sqrt{\frac{\sin \frac{1}{2}s \sin (\frac{1}{2}s - c)}{\sin a \sin b}}.$$

139. Proposition V.

The sine of one half of any side of a spherical triangle is equal to the square root of the quotient obtained by dividing the cosine of one-half the sum of the angles into the cosine of one-half the sum minus the angle opposite the side, by the product of the sines of the adjacent angles.

Taking the formulas of the last article, passing to the polar triangle, making $S = A' + B' + C'$, substituting in these formulas, reducing, and omitting the accents, we have

$$(1) \sin \frac{1}{2}a = \sqrt{\frac{-\cos \frac{1}{2}S \cos (\frac{1}{2}S - A)}{\sin B \sin C}}.$$

$$(2) \sin \frac{1}{2}b = \sqrt{\frac{-\cos \frac{1}{2}S \cos (\frac{1}{2}S - B)}{\sin A \sin C}}.$$

$$(3) \sin \frac{1}{2}c = \sqrt{\frac{-\cos \frac{1}{2}S \cos (\frac{1}{2}S - C)}{\sin A \sin B}}.$$

140. Proposition VI.

The cosine of one half of any angle of a spherical triangle is equal to the square root of the quotient obtained by dividing the sine of one-half the sum of the sides minus one adjacent side into the sine of one-half the sum minus the other adjacent side, by the product of the sines of the adjacent sides.

$$\cos A = \frac{\cos a - \cos b \cos c}{\sin b \sin c}. \quad \text{Article 136, (1).}$$

Subtracting both members from 1, we have

$$1 - \cos A = \frac{\cos b \cos c + \sin b \sin c - \cos a}{\sin b \sin c}.$$

$$1 - \cos A = 2 \sin^2 \frac{1}{2}A \quad \text{Article 95, (9).}$$

$$\cos b \cos c + \sin b \sin c = \cos (b - c). \quad \text{Article 91, (d).}$$

$$\therefore 2 \sin^2 \frac{1}{2}A = \frac{\cos (b - c) - \cos a}{\sin b \sin c}.$$

But by article 96, (8), we have

$$\cos (b - c) - \cos a = 2 \sin \frac{1}{2}(a + c - b) \sin \frac{1}{2}(a + b - c).$$

Substituting and dividing by 2, we have

$$\therefore \sin^2 \frac{1}{2}A = \frac{\sin \frac{1}{2}(a + c - b) \sin \frac{1}{2}(a + b - c)}{\sin b \sin c}.$$

$$\text{But } \frac{1}{2}(a + c - b) = \frac{1}{2}s - b \text{ and } \frac{1}{2}(a + b - c) = \frac{1}{2}s - c.$$

Substituting in the value of $\sin^2 \frac{1}{2}A$, and in the similar values for $\sin^2 \frac{1}{2}B$ and $\sin^2 \frac{1}{2}C$, and extracting the square root, we have

$$(1) \sin \frac{1}{2}A = \sqrt{\frac{\sin (\frac{1}{2}s - b) \sin (\frac{1}{2}s - c)}{\sin b \sin c}}.$$

$$(2) \sin \frac{1}{2}B = \sqrt{\frac{\sin (\frac{1}{2}s - a) \sin (\frac{1}{2}s - c)}{\sin a \sin c}}.$$

$$(3) \sin \frac{1}{2}C = \sqrt{\frac{\sin (\frac{1}{2}s - a) \sin (\frac{1}{2}s - b)}{\sin a \sin b}}.$$

141. Proposition VII.

The cosine of one half of any side of a spherical triangle is equal to the square root of the quotient obtained by dividing the cosine of one-half the sum of the angles minus one adjacent angle into the cosine of half the sum minus the other adjacent angle, by the product of the sines of the adjacent angles.

Taking the formulas of the last article, passing to the polar triangle, making $S = A' + B' + C'$, substituting, resolving, and omitting the accents, we have

$$(1) \cos \frac{1}{2} a = \sqrt{\frac{\cos (\frac{1}{2} S - B) \cos (\frac{1}{2} S - C)}{\sin B \sin C}},$$

$$(2) \cos \frac{1}{2} b = \sqrt{\frac{\cos (\frac{1}{2} S - A) \cos (\frac{1}{2} S - C)}{\sin A \sin C}},$$

$$(3) \cos \frac{1}{2} c = \sqrt{\frac{\cos (\frac{1}{2} S - A) \cos (\frac{1}{2} S - B)}{\sin A \sin B}}.$$

142. Proposition VIII.

The tangent of one-half of any angle of a spherical triangle is equal to the square root of the quotient obtained by dividing the sine of one-half the sum of the sides minus one adjacent side into the sine of one-half the sum minus the other adjacent side, by the sine of one-half the sum of the sides into the sine of one-half the sum minus the opposite side.

Dividing (1), (2), (3), article 140, respectively, by (1), (2), (3), article 138, we have

$$(1) \tan \frac{1}{2} A = \sqrt{\frac{\sin (\frac{1}{2} s - b) \sin (\frac{1}{2} s - c)}{\sin \frac{1}{2} s \sin (\frac{1}{2} s - a)}},$$

$$(2) \tan \frac{1}{2} B = \sqrt{\frac{\sin (\frac{1}{2} s - a) \sin (\frac{1}{2} s - c)}{\sin \frac{1}{2} s \sin (\frac{1}{2} s - b)}},$$

$$(3) \tan \frac{1}{2} C = \sqrt{\frac{\sin (\frac{1}{2} s - a) \sin (\frac{1}{2} s - b)}{\sin \frac{1}{2} s \sin (\frac{1}{2} s - c)}}.$$

143. Proposition IX.

The tangent of one half of any side of a spherical triangle is equal to the square root of the quotient obtained by dividing

minus the co-sine of one-half the sum of the angles into the co-sine of one-half the sum minus the angle opposite the side, by the co-sine of one-half the sum of the angles minus one adjacent angle into the co-sine of one-half the sum minus the other adjacent angle.

Dividing (1), (2), (3), article 139, respectively, by (1), (2), (3), article 141, we have

$$(1) \tan \frac{1}{2} a = \sqrt{\frac{1 - \cos \frac{1}{2} S \cos (\frac{1}{2} S - A)}{\cos (\frac{1}{2} S - B) \cos (\frac{1}{2} S - C)}},$$

$$(2) \tan \frac{1}{2} b = \sqrt{\frac{1 - \cos \frac{1}{2} S \cos (\frac{1}{2} S - B)}{\cos (\frac{1}{2} S - A) \cos (\frac{1}{2} S - C)}},$$

$$(3) \tan \frac{1}{2} c = \sqrt{\frac{1 - \cos \frac{1}{2} S \cos (\frac{1}{2} S - C)}{\cos (\frac{1}{2} S - A) \cos (\frac{1}{2} S - B)}}.$$

The reciprocals of (1), (2), (3), articles 142, 143, will give formulas for co-tangents, which may be written and expressed in words.

144. Napier's Analogies.

Dividing (1), article 142, by (2), we have

$$\frac{\tan \frac{1}{2} A}{\tan \frac{1}{2} B} = \frac{\sin (\frac{1}{2} s - b)}{\sin (\frac{1}{2} s - a)}.$$

This, as a proportion taken by composition and division, gives

$$\frac{\tan \frac{1}{2} A + \tan \frac{1}{2} B}{\tan \frac{1}{2} A - \tan \frac{1}{2} B} = \frac{\sin (\frac{1}{2} s - b) + \sin (\frac{1}{2} s - a)}{\sin (\frac{1}{2} s - b) - \sin (\frac{1}{2} s - a)},$$

$$\frac{\tan \frac{1}{2} A + \tan \frac{1}{2} B}{\tan \frac{1}{2} A - \tan \frac{1}{2} B} = \frac{\sin \frac{1}{2} A + \sin \frac{1}{2} B}{\cos \frac{1}{2} A - \cos \frac{1}{2} B}.$$

Multiplying both terms of the second member by $\cos \frac{1}{2} A \cos \frac{1}{2} B$,

$$\begin{aligned} \tan \frac{1}{2} A &= \tan \frac{1}{2} B \frac{\sin \frac{1}{2} A \cos \frac{1}{2} B + \cos \frac{1}{2} A \sin \frac{1}{2} B}{\sin \frac{1}{2} A \cos \frac{1}{2} B - \cos \frac{1}{2} A \sin \frac{1}{2} B} \end{aligned}$$

Reducing the second member by articles 89, (a), and 91, we

$$\frac{\tan \frac{1}{2} A + \tan \frac{1}{2} B}{\tan \frac{1}{2} A - \tan \frac{1}{2} B} = \frac{\sin \frac{1}{2}(A+B)}{\sin \frac{1}{2}(A-B)},$$

$$\frac{\sin(\frac{1}{2}s-b) + \sin(\frac{1}{2}s-a)}{\sin(\frac{1}{2}s-b) - \sin(\frac{1}{2}s-a)} = \frac{\tan \frac{1}{2}c}{\tan \frac{1}{2}(a-b)} \quad \text{Art. 96, (11).}$$

$$\therefore \frac{\sin \frac{1}{2}(A+B)}{\sin \frac{1}{2}(A-B)} = \frac{\tan \frac{1}{2}c}{\tan \frac{1}{2}(a-b)}.$$

$$\therefore (1) \sin \frac{1}{2}(A+B) : \sin \frac{1}{2}(A-B) :: \tan \frac{1}{2}c : \tan \frac{1}{2}(a-b).$$

The reciprocal of (1) \times (2), article 142, gives

$$\frac{1}{\tan \frac{1}{2} A \tan \frac{1}{2} B} = \frac{\sin \frac{1}{2} s}{\sin(\frac{1}{2}s-c)}.$$

By division and composition, we have

$$\frac{1 - \tan \frac{1}{2} A \tan \frac{1}{2} B}{1 + \tan \frac{1}{2} A \tan \frac{1}{2} B} = \frac{\sin \frac{1}{2} s - \sin(\frac{1}{2}s-c)}{\sin \frac{1}{2} s + \sin(\frac{1}{2}s-c)}.$$

Reducing both members as before, we have

$$\frac{\cos \frac{1}{2}(A+B)}{\cos \frac{1}{2}(A-B)} = \frac{\tan \frac{1}{2}c}{\tan \frac{1}{2}(a+b)}.$$

$$\therefore (2) \cos \frac{1}{2}(A+B) : \cos \frac{1}{2}(A-B) :: \tan \frac{1}{2}c : \tan \frac{1}{2}(a+b).$$

Passing from (1) and (2) to the polar triangle, we have

$$(3) \sin \frac{1}{2}(a+b) : \sin \frac{1}{2}(a-b) :: \cot \frac{1}{2}C : \tan \frac{1}{2}(A-B).$$

$$(4) \cos \frac{1}{2}(a+b) : \cos \frac{1}{2}(a-b) :: \cot \frac{1}{2}C : \tan \frac{1}{2}(A+B).$$

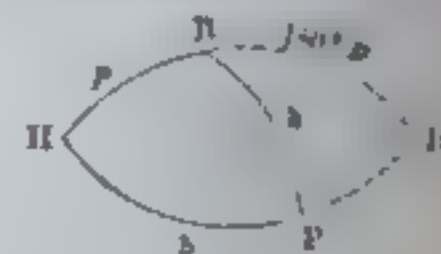
145. Proposition.

In a right-angled spherical triangle, as b increases from 0° to 90° , from 90° to 180° , from 180° to 270° , and from 270° to 360° , if $p < 90^\circ$, h increases from p to 90° , from 90° to $180^\circ - p$, decreases from $180^\circ - p$ to 90° , and from 90° to p ; if $p > 90^\circ$, h decreases from p to 90° , from 90° to $180^\circ - p$, increases from $180^\circ - p$ to 90° , and from 90° to p ; if $p = 90^\circ$, $h = 90^\circ$ for all values of b .

1. $p < 90^\circ$; $\therefore \cos p$ is positive.

$$\cos h = \cos b \cos p.$$

If $b = 0$, $\cos b = 1$; therefore,
 $\cos h = \cos p$; $\therefore h = p$.



As b increases from 0° to 90° , $\cos b$ is positive, and diminishes from 1 to 0; $\therefore \cos h$ is positive, and diminishes from $\cos p$ to 0; $\therefore h$ increases from p to 90° .

As b increases from 90° to 180° , $\cos b$ is negative, and increases numerically from 0 to -1 ; $\therefore \cos h$ is negative, and increases numerically from 0 to $-\cos p$; $\therefore h$ increases from 90° to $180^\circ - p$, and the triangle becomes the lune HH' .

As b increases from 180° to 270° , $\cos b$ is negative, and decreases numerically from -1 to 0; $\therefore \cos h$ is negative, and decreases numerically from $-\cos p$ to 0; $\therefore h$ decreases from $180^\circ - p$ to 90° .

As b increases from 270° to 360° , $\cos b$ is positive, and increases from 0 to 1; $\therefore \cos h$ is positive, and increases from 0 to $\cos p$; $\therefore h$ decreases from 90° to p , and the triangle becomes the hemisphere.

2. $p = 90^\circ$; $\therefore \cos p$ is negative.

$$\cos h = \cos b \cos p.$$

If $b = 0$, $\cos b = 1$, therefore,

$$\cos h = \cos p; \therefore h = p.$$



As b increases from 0° to 90° , $\cos b$ is positive, and decreases from 1 to 0; $\therefore \cos h$ is negative, and decreases numerically from $\cos p$ to 0; $\therefore h$ decreases from p to 90° .

As b increases from 90° to 180° , $\cos b$ is negative, and increases numerically from 0 to -1 ; $\therefore \cos h$ is positive, and increases from 0 to $-\cos p$; $\therefore h$ decreases from 90° to $180^\circ - p$, and the triangle becomes the lune HH' .

As b increases from 180° to 270° , $\cos b$ is negative, and decreases numerically from -1 to 0; $\therefore \cos h$ is positive, and decreases from $-\cos p$ to 0; $\therefore h$ increases from $180^\circ - p$ to 90° .

As b increases from 270° to 360° , $\cos b$ is positive, and increases from 0 to 1; $\therefore \cos h$ is negative, and increases numerically from 0 to $\cos p$; $\therefore h$ increases from 90° to p , and the triangle becomes the hemisphere.

3. $p = 90^\circ$; $\therefore \cos p = 0$.

$$\therefore \cos h = \cos b \cos p = 0; \therefore h = 90^\circ.$$

Cor.—Since B and b are of the same species, B may be substituted for b in the preceding proposition.

In the application of these principles to the discussion of Case I, in which two sides and an angle opposite one of them are given, a corresponds to b , and HB to b .

146. Case I.

Given two sides of a spherical triangle, and the angle opposite one of them; required the remaining parts.

Let a and b be the given sides and A the given angle.



1. $A < 90^\circ$; $\therefore p < 90^\circ$.

$$\sin p = \sin b \sin A.$$

1. $a = p$.

B coincides with H , and the triangle ABC becomes the right triangle AHC .

2. $a < 90^\circ$ and $a > p$.

By the last proposition the point B lies in the first or fourth quadrant, estimated from H .

3. $a = 90^\circ$.

$HB = 90^\circ$ or 270° , and $HCB = 90^\circ$ or 270° .

4. $a > 90^\circ$ and $a < 180^\circ - p$.

B lies in the second or third quadrant from H .

5. $a = 180^\circ - p$.

$HB = 180^\circ$, and $ABC = AHC + \frac{1}{2}$ the hemisphere.

6. $a = 180^\circ - b$.

$HB = HA'$ or $360^\circ - HA'$, and then the first triangle becomes the lune AA' .

7. $a = b$.

$HB = AH$ or $360^\circ - AH$, and the second triangle becomes the hemisphere.

$$8. \ a < p \text{ or } a > 180^\circ - p.$$

The triangle is impossible, since p is the least, and $180^\circ - p$ is the greatest value of a .

$$11. \ A < 90^\circ; \therefore p > 90^\circ.$$

$$\sin p = \sin b \sin A.$$



$$1. \ a = p.$$

B coincides with H , and ABC becomes AHC .

$$2. \ a > 90^\circ \text{ and } a < p.$$

B lies in the first or fourth quadrant from H .

$$3. \ a = 90^\circ.$$

$HB = 90^\circ$ or 270° , and $HCB = 90^\circ$ or 270° .

$$4. \ a < 90^\circ \text{ and } a > 180^\circ - p.$$

B lies in the second or third quadrant from H .

$$5. \ a = 180^\circ - p.$$

$HB = 180^\circ$, and $ABC = AHC + \frac{1}{2}$ the hemisphere.

$$6. \ a = 180^\circ - b.$$

$HB = HA$ or $360^\circ - HA$, and the first triangle becomes the lune AA' .

$$7. \ a = b.$$

$HB = AH$ or $360^\circ - AH$, and the second triangle becomes the hemisphere.

$$8. \ a > p \text{ or } a < 180^\circ - p.$$

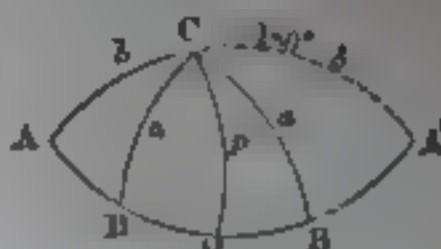
The triangle is impossible, since p is the greatest, and $180^\circ - p$ is the least value of a .

$$\text{III. } A = 90^\circ.$$

The triangle is right-angled, and is solved as in article 131.

147. Examples.

$$1. \text{ Given } \begin{cases} a = 60^\circ 20'. \\ b = 80^\circ 35'. \\ A = 38^\circ 25'. \end{cases} \text{ Req. } \begin{cases} B. \\ C. \\ c. \end{cases}$$



$$A < 90^\circ; \therefore p < 90^\circ.$$

$$\sin p = \sin b \sin A, \therefore p = 37^\circ 48' 26''.$$

Since $a > p$ and $a < 180^\circ - p$, the triangle is possible.

Since $a < b$ and $a < 180^\circ - b$, B lies between H and A or H and A' .

$$\sin p = \sin a \sin B, \therefore B = 44^\circ 52' 05''.$$

$$\cos HCB = \tan p \cot a, \therefore HCB = 63^\circ 46' 18''.$$

$$\cos a = \cos p \cos HB, \therefore HB = 51^\circ 12' 41''.$$

$$\cos ACH = \tan p \cot b, \therefore ACH = 82^\circ 36' 25''.$$

$$\cos b = \cos p \cos AH, \therefore AH = 78^\circ 02' 54''.$$

$$C = ACH + HCB = 146^\circ 22' 43'' \text{ or } 18^\circ 50' 07''.$$

$$c = AH \pm HB = 129^\circ 15' 35'' \text{ or } 26^\circ 50' 13''.$$

$$\text{In } ACB, ABC = 180^\circ - HBC = 135^\circ 07' 55''.$$

We can also find B from the proportion,

$$\sin a : \sin b :: \sin A : \sin B.$$

C and c can be found from the proportions,

$$\sin \frac{1}{2}(b + a) : \sin \frac{1}{2}(b - a) :: \cot \frac{1}{2}C : \tan \frac{1}{2}(B - A).$$

$$\sin A : \sin C :: \sin a : \sin c.$$

2. Given.

Required.

$$\begin{cases} a = 63^\circ 50'. \\ b = 80^\circ 19'. \\ A = 51^\circ 30'. \end{cases} \begin{cases} B = 59^\circ 16' 00'' \text{ or } 120^\circ 44' 00''. \\ C = 131^\circ 29' 42'' \text{ or } 24^\circ 37' 30''. \\ c = 120^\circ 47' 50'' \text{ or } 28^\circ 32' 44''. \end{cases}$$

3. Given.	Required.
$\left\{ \begin{array}{l} a = 75^\circ 38', \\ b = 14^\circ 22', \\ A = 65^\circ 28'. \end{array} \right\}$	$\left\{ \begin{array}{l} B = 65^\circ 28' \text{ or } 114^\circ 32', \\ C = 180^\circ \text{ or } 57^\circ 03' 32'', \\ c = 180^\circ \text{ or } 63^\circ 20' 18''. \end{array} \right\}$

4. Given.	Required.
$\left\{ \begin{array}{l} a = 60^\circ 10' 48'', \\ b = 64^\circ 23' 15'', \\ A = 95^\circ 38' 01''. \end{array} \right\}$	$\left\{ \begin{array}{l} B = 114^\circ 26' 50'' \text{ or } 65^\circ 33' 10'', \\ C = 236^\circ 51' 27'' \text{ or } 97^\circ 27' 13'', \\ c = 236^\circ 01' 51'' \text{ or } 100^\circ 49' 49''. \end{array} \right\}$

5. Given.	Required.
$\left\{ \begin{array}{l} a = 100^\circ, \\ b = 85^\circ, \\ A = 50^\circ. \end{array} \right\}$	$\left\{ \begin{array}{l} B = 50^\circ 47' 41'' \text{ or } 129^\circ 12' 19'', \\ C = 186^\circ 05' 16'' \text{ or } 312^\circ 03' 12'', \\ c = 187^\circ 50' 09'' \text{ or } 336^\circ 39' 45''. \end{array} \right\}$

6. If $A < 90^\circ$, what is the relation of a to p , or to $180^\circ - p$, when there is no solution?

7. If $A > 90^\circ$, what is the relation of a to p , or to $180^\circ - p$, when there is no solution?

148. Proposition.

In a right-angled spherical triangle, as B increases from 0° to 90° , from 90° to 180° , from 180° to 270° , and from 270° to 360° ; if $p < 90^\circ$, P decreases from 90° to p , increases from p to 90° , increases from 90° to $180^\circ - p$, and decreases from $180^\circ - p$ to 90° ; if $p > 90^\circ$, P increases from 90° to p , decreases from p to 90° , decreases from 90° to $180^\circ - p$, and increases from $180^\circ - p$ to 90° ; if $p = 90^\circ$, $P = 90^\circ$, for all values of B .

1. $p < 90^\circ$; $\therefore \cos p$ is positive.

$$\cos P = \cos p \sin B.$$

If $B = 0^\circ$, $\sin B = 0$; $\therefore \cos P = 0$; $\therefore P = 90^\circ$.



As B increases from 0° to 90° , $\sin B$ is positive, and increases from 0 to 1; $\therefore \cos P$ is positive, and increases from 0 to $\cos p$; $\therefore P$ decreases from 90° to p .

As B increases from 90° to 180° , $\sin B$ is positive, and decreases from 1 to 0; $\therefore \cos P$ is positive, and decreases from $\cos p$ to 0; $\therefore P$ increases from p to 90° , and the triangle becomes the lune HH' .

As B increases from 180° to 270° , $\sin B$ is negative, and increases numerically from 0 to -1 ; $\therefore \cos P$ is negative, and increases numerically from 0 to $-\cos p$; $\therefore P$ increases from 90° to $180^\circ - p$.

As B increases from 270° to 360° , $\sin B$ is negative, and decreases numerically from -1 to 0; $\therefore \cos P$ is negative, and decreases numerically from $-\cos p$ to 0; $\therefore P$ decreases from $180^\circ - p$ to 90° , and the triangle becomes the hemisphere.

2. $p > 90^\circ$; $\therefore \cos p$ is negative.

$$\cos P = \cos p \sin B.$$

If $B = 0^\circ$, $\sin B = 0$; $\therefore \cos P = 0$; $\therefore P = 90^\circ$.

As B increases from 0° to 90° , $\sin B$ is positive, and increases from 0 to 1; $\therefore \cos P$ is negative, and increases numerically from 0 to $\cos p$; $\therefore P$ increases from 90° to p .

As B increases from 90° to 180° , $\sin B$ is positive, and decreases from 1 to 0; $\therefore \cos P$ is negative, and decreases numerically from $\cos p$ to 0; $\therefore P$ decreases from p to 90° , and the triangle becomes the lune.

As B increases from 180° to 270° , $\sin B$ is negative, and increases numerically from 0 to -1 ; $\therefore \cos P$ is positive, and increases from 0 to $-\cos p$; $\therefore P$ decreases from 90° to $180^\circ - p$.

As B increases from 270° to 360° , $\sin B$ is negative, and decreases numerically from -1 to 0 ; $\therefore \cos P$ is positive, and decreases numerically from $-\cos p$ to 0 , P increases from $180^\circ - p$ to 90° , and the triangle becomes the hemisphere.

$$3. \quad p = 90^\circ, \therefore \cos p = 0$$

$$\therefore \cos P = \cos p \sin B = 0; \therefore P = 90^\circ.$$

Cor. — Since b and B are of the same species, b may be substituted for B in the preceding proposition.

149. Case II.

Given two angles of a spherical triangle and the side opposite one of them; required the remaining parts.

Let A and B be the given angles, and b the given side.

$$1. \quad A < 90^\circ; \therefore p < 90^\circ.$$

$$\sin p = \sin b \sin A.$$

$$1. \quad B > p \text{ and } B < 90^\circ.$$

By the last proposition, the point B lies in the first or second quadrant estimated from H as origin.

$$2. \quad B = p.$$

The angle $HCB = 90^\circ$, and the arc $HB = 90^\circ$.

$$3. \quad B < 180^\circ - p, \text{ and } B > 90^\circ.$$

B lies in the third or fourth quadrant from H .

$$4. \quad B = 180^\circ - p.$$

The angle $HCB = 270^\circ$, and the arc $HB = 270^\circ$.



$$5. \quad B = 90^\circ.$$

$HB = 0^\circ, 180^\circ$, or 360° , and the triangle becomes ACH , $ACH + \frac{1}{2}$ of a hemisphere, or a hemisphere + ACH .

$$6. \quad B = A.$$

B lies in the first or second quadrant from H , and one of the triangles becomes the lune AA' .

$$7. \quad B = 180^\circ - A.$$

B lies in the third or fourth quadrant from H , and one of the triangles becomes the hemisphere.

$$8. \quad B < p \text{ or } B > 180^\circ - p.$$

The triangle is impossible, since p is the least, and $180^\circ - p$ is the greatest value of B .

$$11. \quad A > 90^\circ; \therefore p > 90^\circ.$$

$$\sin p = \sin b \sin A.$$

$$1. \quad B < p \text{ and } B > 90^\circ.$$

B lies in the first or second quadrant from H .

$$2. \quad B = p.$$

The angle $HCB = 90^\circ$, and the arc $HB = 90^\circ$.

$$3. \quad B > 180^\circ - p \text{ and } B < 90^\circ.$$

B lies in the third or fourth quadrant from H .

$$4. \quad B = 180^\circ - p.$$

The angle $HCB = 270^\circ$, and the arc $HB = 270^\circ$.

$$5. \quad B = 90^\circ.$$

$HB = 0^\circ, 180^\circ$, or 360° , and the triangle becomes ACH , $ACH + \frac{1}{2}$ of a hemisphere, or a hemisphere + ACH .

6. $B = A$

B lies in the first or second quadrant from H , and one of the triangles becomes the lune AA' .

$$7. B = 180^\circ - A.$$

B lies in the third or fourth quadrant from H , and one of the triangles becomes the hemisphere.

$$8. B > p \text{ or } B < 180^\circ - p.$$

The triangle is impossible, since p is the greatest, and $180^\circ - p$ is the least value of B .

$$\text{III. } A = 90^\circ$$

The triangle is right-angled, and is solved as in article 131.

150. Examples.

$$1. \text{ Given } \begin{cases} A = 75^\circ 30'. \\ B = 80^\circ 40'. \\ b = 70^\circ 50'. \end{cases} \text{ Required } \begin{cases} a. \\ c. \end{cases}$$



$$A < 90^\circ; \therefore p < 90^\circ.$$

$$\sin p = \sin b \sin A; \therefore p = 66^\circ 07' 56''$$

Since $B > p$ and $< 180^\circ - p$, the triangle is possible.

Since $B < 90^\circ$ and $> p$, B lies in the first or second quadrant from H .

$$\sin p = \sin a \sin B, \therefore a = \begin{cases} 67^\circ 56'. \\ 112^\circ 04'. \end{cases}$$

The second value of a , the supplement of the first, is taken when B lies in the second quadrant from H .

$$\cos B = \cos p \sin HCB, \therefore HCB = \begin{cases} 23^\circ 37' 44''. \\ 156^\circ 22' 16''. \end{cases}$$

$$\sin HB = \tan p \cot B, \therefore HB = \begin{cases} 21^\circ 48' 19''. \\ 158^\circ 11' 41''. \end{cases}$$

$$\cos ACH = \tan p \cot b, \therefore ACH = 38^\circ 13' 36'.$$

$$\cos b = \cos p \cos AH, \therefore AH = 35^\circ 46'.$$

$$C = ACH + HCB = 61^\circ 51' 20'' \text{ or } 194^\circ 35' 52''.$$

$$c = AH + HB = 57^\circ 34' 19'' \text{ or } 193^\circ 57' 41''.$$

We can find a , c , and C from the proportions,

$$\sin B : \sin A :: \sin b : \sin a.$$

$$\sin \frac{1}{2}(B + A) : \sin \frac{1}{2}(B - A) :: \tan \frac{1}{2}c : \tan \frac{1}{2}(b - a).$$

$$\sin b : \sin c :: \sin B : \sin C.$$

2. Given.

Required.

$$\begin{cases} A = 33^\circ 15'. \\ B = 31^\circ 34'. \\ b = 70^\circ 40'. \end{cases} \left\{ \begin{array}{l} a = 80^\circ 03' 25'' \text{ or } 99^\circ 56' 35''. \\ c = 161^\circ 24' 52'' \text{ or } 173^\circ 30' 52''. \\ e = 145^\circ 03' 13'' \text{ or } 168^\circ 18' 23''. \end{array} \right.$$

3. Given.

Required.

$$\begin{cases} A = 132^\circ 16'. \\ B = 139^\circ 44'. \\ b = 127^\circ 30'. \end{cases} \left\{ \begin{array}{l} a = 65^\circ 16' 30'' \text{ or } 114^\circ 43' 30''. \\ C = 165^\circ 41' 46'' \text{ or } 126^\circ 40' 44''. \\ c = 162^\circ 20' 55'' \text{ or } 100^\circ 07' 25''. \end{array} \right.$$

4. Given.

Required.

$$\begin{cases} A = 48^\circ 50'. \\ B = 131^\circ 10'. \\ b = 75^\circ 48'. \end{cases} \left\{ \begin{array}{l} a = 75^\circ 48' \text{ or } 104^\circ 12'. \\ C = 360^\circ \text{ or } 328^\circ 39' 28''. \\ c = 360^\circ \text{ or } 317^\circ 56' 42''. \end{array} \right.$$

Scholium.—In the two preceding cases some of the parts are found to be greater than 180° ; but the corresponding triangles conform to the conditions of the problem, and are therefore true solutions.

Parts greater than 180° are usually excluded, in which case the principles of the following article will apply to determining the species of the parts.

The principles established in Geometry are given without demonstration.

131. Principles.

1. Each part of a spherical triangle is less than 180° .
2. The greater side is opposite the greater angle, and conversely.
3. Each side is less than the sum of the other sides.
4. The sum of the sides is less than 360° .
5. The sum of the angles is greater than 180° , and less than 540° .
6. Each angle is greater than the difference between 180° and the sum of the other angles.

For, $A + B + C > 180^\circ$. Principle 5.

$$\therefore A > 180^\circ - (B + C).$$

The last formula is always algebraically true; but in case $B + C > 180^\circ$, it might be doubted whether it is numerically true.

Passing to the polar triangle, we have, by principle 3.

$$a' < b' + c'.$$

$$\text{or } 180^\circ - A < 180^\circ - B + 180^\circ - C.$$

$$\text{or } -A < 180^\circ - (B + C).$$

$$\therefore A > B + C - 180^\circ.$$

7. A side differing more from 90° than another side is of the same species as its opposite angle.

By article 136, we have

$$\cos a = \cos b \cos c + \sin b \sin c \cos A.$$

$$\therefore \cos A = \frac{\cos a - \cos b \cos c}{\sin b \sin c}.$$

But $\sin b \sin c$ is positive, since b and c are each less than 180° .

If a differs more from 90° than b or c , then we shall have

$$\cos a > \cos b, \text{ or } \cos a > \cos c, \text{ numerically;}$$

and since neither $\cos b$ nor $\cos c$ exceeds 1, we have

$$\cos a > \cos b \cos c.$$

$\therefore \cos A$ and $\cos a$ have the same sign, $\therefore A$ and a are of the same species.

8. An angle differing more from 90° than another angle is of the same species as its opposite side.

By article 137, we have

$$\cos A = \sin B \sin C \cos a - \cos B \cos C.$$

$$\therefore \cos a = \frac{\cos A + \cos B \cos C}{\sin B \sin C}.$$

If A differs more from 90° than B or C , then, as before, $\cos A$ and $\cos a$ have the same sign, or A and a are of the same species.

9. Two sides, at least, are of the same species as their opposite angles, and conversely.

If each of two sides differs more from 90° than the remaining side, they will be of the same species as their opposite angles, as is evident from principle 7.

If the triangle is isosceles, and the equal sides less than 90° , the perpendicular from the vertex to the third side will be less than 90° , since one half the

third side is less than 90° , and the angles opposite this perpendicular will be less than 90° , article 129, or of the same species as their opposite sides.

If the equal sides are greater than 90° , the perpendicular will be greater than 90° , since one half the third side is less than 90° , and the angles opposite the perpendicular will be greater than 90° , article 129, or of the same species as their opposite sides.

If one side exceeds 90° by as much as 90° exceeds another side, and the third side is greater or less than each of the other sides, this third side is of the same species as its opposite angle by principle 7.

If the greater of the two sides is of the same species as its opposite angle, then we shall have two sides of the same species as their opposite angles.

If the greater of the two sides is not of the same species as its opposite angle, this angle will be of the same species as the other side, or less than 90° ; but the angle opposite this other side is less than the angle opposite the greater side, and hence less than 90° , or of the same species as its opposite side, and again we have two sides of the same species as their opposite angles.

10. The sum of two sides is greater than, equal to, or less than, 180° , according as the sum of their opposite angles is greater than, equal to, or less than, 180° .

$$\tan \frac{1}{2}(a+b) \cos \frac{1}{2}(A+B) = \tan \frac{1}{2}c \cos \frac{1}{2}(A-B). \text{ Art. 144.}$$

But $c < 180^\circ$, $\therefore \frac{1}{2}c < 90^\circ$, $\tan \frac{1}{2}c > 0$,

and $A+B < 180^\circ$, $\therefore \frac{1}{2}(A+B) < 90^\circ$, $\cos \frac{1}{2}(A+B) > 0$.

$\therefore \tan \frac{1}{2}c \cos \frac{1}{2}(A-B) > 0$, $\tan \frac{1}{2}(a+b) \cos \frac{1}{2}(A+B) > 0$.

$\therefore \tan \frac{1}{2}(a+b)$ and $\cos \frac{1}{2}(A+B)$ have like signs.

\therefore If $\frac{1}{2}(A+B) > 90^\circ$, or $< 90^\circ$, $\frac{1}{2}(a+b) > 90^\circ$, or $< 90^\circ$.

\therefore If $A+B > 180^\circ$, or $< 180^\circ$, $a+b > 180^\circ$, or $< 180^\circ$.

152. Case III.

Given two sides and the included angle of a spherical triangle; required the remaining parts.

$$1 \text{ Given } \begin{cases} a = 85^\circ 31' 30'' \\ b = 65^\circ 41' 28'' \\ c = 50^\circ 10' 10'' \end{cases} \text{ Req. } \begin{cases} A \\ B \\ C \end{cases}$$



We have, article 144,

$$\cos \frac{1}{2}(a+b) : \cos \frac{1}{2}(a-b) :: \cot \frac{1}{2}C : \tan \frac{1}{2}(A+B)$$

$$\sin \frac{1}{2}(a+b) : \sin \frac{1}{2}(a-b) :: \cot \frac{1}{2}C : \tan \frac{1}{2}(A-B)$$

$$\begin{aligned} \frac{1}{2}(a+b) &= 75^\circ 36' 25'' & \frac{1}{2}(a-b) &= 9^\circ 45' 50'' \\ \frac{1}{2}C &= 25^\circ 05' 05'' & \frac{1}{2}(A+B) &= 42^\circ 48' 19'' \end{aligned}$$

We also have, article 144,

$$\sin \frac{1}{2}(A+B) : \sin \frac{1}{2}(A-B) :: \tan \frac{1}{2}c : \tan \frac{1}{2}(a-b)$$

$$\frac{1}{2}c = 46^\circ 43' 00'', \therefore c = 93^\circ 26' 14''.$$

We can also find c from the proportion,

$$\sin a : \sin c :: \sin A : \sin C.$$


But the angle c is more readily determined from the proportion employed; for if we take the supplement of $46^\circ 43' 00''$, then c would be greater than 180° .

Again, all the known terms of the proportion are positive; hence, $\tan \frac{1}{2}c$ is positive, $\therefore \frac{1}{2}c < 90^\circ$.

$$2 \text{ Given } \begin{cases} a = 125^\circ 31' 30'' \\ b = 70^\circ 21' 28'' \\ c = 80^\circ 10' 10'' \end{cases} \text{ Req. } \begin{cases} A \\ B \\ C \end{cases}$$

153. Case IV.

Given two angles and the included side of a spherical triangle; required the remaining parts.

$$1. \text{Giv. } \begin{cases} A = 62^\circ 54'. \\ B = 48^\circ 30'. \\ c = 114^\circ 29' 58''. \end{cases} \text{Req. } \begin{cases} a. \\ b. \\ C. \end{cases}$$


We have, article 144,

$$\begin{aligned} \cos \frac{1}{2}(A+B) : \cos \frac{1}{2}(A-B) &:: \tan \frac{1}{2}c : \tan \frac{1}{2}(a+b), \\ \sin \frac{1}{2}(A+B) : \sin \frac{1}{2}(A-B) &:: \tan \frac{1}{2}c : \tan \frac{1}{2}(a-b) \\ \therefore \begin{cases} \frac{1}{2}(a+b) = 69^\circ 55' 48'', \\ \frac{1}{2}(a-b) = 13^\circ 16' 18''. \end{cases} \therefore \begin{cases} a = 83^\circ 12' 06'', \\ b = 56^\circ 39' 30''. \end{cases} \end{aligned}$$


We also have, article 144,

$$\begin{aligned} \sin \frac{1}{2}(a+b) : \sin \frac{1}{2}(a-b) &:: \cot \frac{1}{2}C : \tan \frac{1}{2}(A+B), \\ \therefore \frac{1}{2}C = 62^\circ 40', \therefore C = 125^\circ 20'. \end{aligned}$$

$$2. \text{Given } \begin{cases} A = 126^\circ 35' 02'', \\ B = 61^\circ 43' 58'', \\ c = 57^\circ 30'. \end{cases} \text{Req. } \begin{cases} a = 115^\circ 19' 57'', \\ b = 8^\circ 27' 59'', \\ C = 48^\circ 31' 38''. \end{cases}$$

154. Case V.

Given the three sides of a spherical triangle; required the angles.

$$1. \text{Giv. } \begin{cases} a = 100^\circ 49' 30'', \\ b = 99^\circ 40' 48'', \\ c = 64^\circ 23' 15''. \end{cases} \text{Req. } \begin{cases} A. \\ B. \\ C. \end{cases}$$


By article 138, we have

$$\cos \frac{1}{2}A = \sqrt{\frac{\sin \frac{1}{2}b \sin \frac{1}{2}(b+c-a)}{\sin b \sin c}},$$

Introducing R and applying logarithms, we have

$$\log \cos \frac{1}{2}A = \frac{1}{2}[\log \sin \frac{1}{2}b + \log \sin \frac{1}{2}(b+c-a) - a.c. \log \sin b - a.c. \log \sin c].$$


$$\therefore \frac{1}{2}A = 48^\circ 43' 14'', \therefore A = 97^\circ 26' 28''$$

$$\text{In like manner we find } \begin{cases} B = 95^\circ 38' 04'', \\ C = 65^\circ 12' 04''. \end{cases}$$

$$2. \text{Given } \begin{cases} a = 85^\circ 30', \\ b = 65^\circ 47', \\ c = 93^\circ 26' 18''. \end{cases} \text{Req. } \begin{cases} A = 83^\circ 20' 08'', \\ B = 65^\circ 14' 20'', \\ C = 65^\circ 20' 00''. \end{cases}$$

155. Case VI.

Given the two sides and the included angle of a spherical triangle; required the sides.

$$1. \text{Given } \begin{cases} A = 110^\circ 15', \\ B = 70^\circ 29', \\ C = 48^\circ 38'. \end{cases} \text{Req. } \begin{cases} a. \\ b. \\ c. \end{cases}$$


By article 141, we have

$$\cos \frac{1}{2}a = \sqrt{\frac{\cos \frac{1}{2}B \sin A \sin C}{\sin B \sin C}}$$

Introducing R and applying logarithms, we have

$$\log \cos \frac{1}{2}a = \frac{1}{2}[\log \cos \frac{1}{2}B + \log \sin A + \log \sin C - \log \sin B - a.c. \log \sin C]$$

$$\therefore \frac{1}{2}a = 76^\circ 11' 31'', \therefore a = 152^\circ 23' 02''$$

$$\text{In like manner we find } \begin{cases} b = 80^\circ 16' 54'', \\ c = 72^\circ 20' 00''. \end{cases}$$

$$2. \text{Given } \begin{cases} A = 121^\circ 36' 34'', \\ B = 42^\circ 45' 13'', \\ C = 34^\circ 15' 00''. \end{cases} \text{Req. } \begin{cases} a = 76^\circ 38' 00'', \\ b = 50^\circ 10' 00'', \\ c = 40^\circ 00' 00''. \end{cases}$$

MENSURATION.

156. Definition and Classification.

Mensuration is the art of calculating the values of geometrical magnitudes.

Mensuration is divided into two branches — *Mensuration of surfaces* and *Mensuration of volumes*.

MENSURATION OF SURFACES.

157. Unit of Superficial Measure.

A unit of superficial measure is a square each side of which is a linear unit.

Thus, according to the object to be accomplished, a square inch, a square foot, a square yard, an acre, etc., is the superficial unit taken.

158. Problem.

To find the area of a rectangle.

Let k denote the area, b the base, and a the altitude of a rectangle.

There are a rows of b superficial units each.



Since there are b superficial units in one row, in a such rows there will be a times b or ab superficial units.

$$\therefore (1) \quad k = ab.$$

The above demonstration applies only in case the base and altitude are commensurable, or have a common unit.

If the base and altitude are incommensurable, denote the area by k' , the base by b' , and the altitude by a' . Then, since by Geometry any two rectangles are to each other as the products of their bases and altitudes, we have

$$k : k' :: ab : a'b'.$$

$$\text{But } k = ab, \therefore k' = a'b'.$$

159. Problem.

To find the area of a parallelogram.

1. When the base and altitude are given.

Let k denote the area, b the base, and a the altitude of a parallelogram.

Since a parallelogram is equal to a rectangle, having the same base and altitude, and since the area of the rectangle is equal to the product of its base and altitude, the area of the parallelogram is equal to the product of its base and altitude.

$$(1) \quad k = ab.$$

2. When two sides and their included angle are given.

$$a = c \sin A.$$

$$(2) \quad k = bc \sin A.$$



160. Problem.

To find the area of a triangle.

1. When the base and altitude are given.

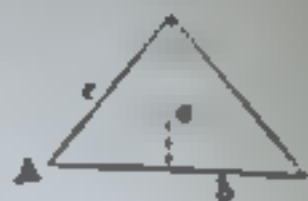
Since a triangle is one-half the parallelogram having the same base and altitude, we have for the triangle,

$$(1) \quad k = \frac{1}{2} ab.$$



2 When two sides and their included angle are given.

Since a triangle is one-half the parallelogram, having an equal angle and equal adjacent sides, we have for the triangle,



$$(2) \quad k = \frac{1}{2} bc \sin A.$$

3. When two angles and a side are given

The third angle is equal to 180° minus the sum of the given angles.

Let, then, the angles and the side b be given.



By the last case, we have

$$k = \frac{1}{2} bc \sin A.$$

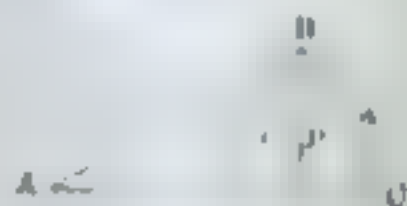
But $\sin B : \sin C :: b : c$, $\therefore c = \frac{b \sin C}{\sin B}$.

Substituting this value of c , we have

$$(3) \quad k = \frac{b^2 \sin A \sin C}{2 \sin B}.$$

4 When two sides and an angle opposite one of them are given.

Let a and c be the given sides, and A the given angle.



In case of one or two solutions determined by article 72, find the value or values of C and B from the formulas,

$$\sin C = \frac{c \sin A}{a}, \text{ and } B = 180^\circ - (A + C).$$

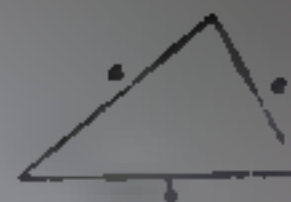
Then, by (2), we have

$$(4) \quad k = \frac{1}{2} ac \sin B.$$

5 When the three sides are given

Let p = the perimeter $= a + b + c$

Then, by article 102, we have



$$(5) \quad k = \sqrt{\frac{1}{4} p \left(\frac{1}{4} p - a \right) \left(\frac{1}{4} p - b \right) \left(\frac{1}{4} p - c \right)}.$$

6. When the perimeter and angles are given.

Let p be the perimeter, and A, B , and C the angles.



By article 98, (10), (11), (12),

$$\frac{1}{2} p^2 \tan \frac{1}{2} A \tan \frac{1}{2} B \tan \frac{1}{2} C = \frac{1}{2} p \left(\frac{1}{4} p - a \right) \left(\frac{1}{4} p - b \right) \left(\frac{1}{4} p - c \right).$$

$$\therefore (6) \quad k = \frac{1}{4} p^2 \tan \frac{1}{2} A \tan \frac{1}{2} B \tan \frac{1}{2} C.$$

7. When the perimeter and radius of the inscribed circle are given

Let $p = a + b + c$, and r be the radius of the inscribed circle.



$$ABC = BOC + AOC + AOB.$$

$$ABC = k, \quad BOC = \frac{1}{2} ar, \quad AOC = \frac{1}{2} br, \quad AOB = \frac{1}{2} cr.$$

$$\therefore k = \frac{1}{2} (a + b + c) r, \text{ or } k = \frac{1}{2} pr.$$

$$(7) \quad k = \frac{1}{2} pr.$$

161. Examples.

1. Find the area of a triangle whose base is 75 ft and altitude is 24 ft. Ans. 900 sq. ft.

2. Two sides of a triangle are 25 yds and 30 yds respectively, and their included angle is 30° ; find the area. Ans. 257.565 sq. yds.

3. In a triangle, $b = 100$ ft., $A = 50^\circ$, $C = 60^\circ$;
required the area. *Ans.* 3529.9 sq. ft.

4. In a triangle, $a = 40$ yds., $c = 50$ yds., $A = 40^\circ$;
required the area. *Ans.* 998.18, or 232.83 sq. yds.

5. In a triangle, $a = 12$ ft., $b = 15$ ft., $c = 17$ ft.;
required k . *Ans.* 87.75 sq. ft.

6. In a triangle the perimeter is 20 ft., and the
angles are 50° , 60° , and 70° , respectively; required
the area. *Ans.* 18.85 sq. ft.

7. In a triangle the perimeter is 60 ft., and the
radius of the inscribed circle is 5 ft.; required the
area. *Ans.* 150 sq. ft.

162. Problem.

To find the area of a quadrilateral.

1. When two opposite sides and the perpendiculars
to these sides from the vertices of the angles at the
extremities of a diagonal are given

Let b and b' be two opposite sides,
and a and a' the perpendiculars to
these sides from the vertices of the
angles D and B .

$$ABCD = ABD + DCB.$$

$$ABCD = k, \quad ABD = \frac{1}{2}ab, \quad DCB = \frac{1}{2}a'b'.$$

$$\therefore (1) \quad k = \frac{1}{2}ab + \frac{1}{2}a'b'.$$

Corollary 1.—If b' is parallel to b , the quadrilateral
becomes a trapezoid, $a' = a$, and (1) becomes

$$(2) \quad k = \frac{1}{2}a(b + b').$$

Corollary 2.—If $b' = b$, the trapezoid becomes a
parallelogram, and (2) becomes

$$(3) \quad k = ab.$$

Corollary 3.—If $b' = 0$, the trapezoid becomes a tri-
angle, and (2) becomes

$$(4) \quad k = \frac{1}{2}ab.$$

2. When a diagonal and the perpendiculars to the
diagonal from the vertices of the opposite angles are
given.

Let d denote the diagonal, and p
and p' the perpendiculars.

$$ABCD = \triangle ABC + \triangle ADC.$$

$$ABCD = k, \quad \triangle ABC = \frac{1}{2}dp, \quad \triangle ADC = \frac{1}{2}dp'.$$

$$k = \frac{1}{2}d(p + p').$$



3. When the sides and a diagonal are given.

Let the areas of the triangles be de-
noted by k' and k'' , which are found
by article 160, (5)

$$(6) \quad k = k' + k''.$$



4. When the sides and one angle are given.

Draw the diagonal opposite the given
angle, and call the areas of the tri-
angles k' and k'' .

In one triangle we have two sides
and their included angle, from which we find the area
and the diagonal.



Then, in the other triangle, we have the three sides, from which we find the area.

$$\therefore (7) \quad k = k' + k''.$$

5. When the diagonals and their included angle are given.

Let d and d' denote the diagonals p and q , r and s their segments, and A their included angle.



The angles at A are equal or supplementary; hence their sines are equal.

$$BCDE = BAC + CAD + DAE + EAB.$$

$$BCDE = k, \quad BAC = \frac{1}{2} pr \sin A, \quad CAD = \frac{1}{2} qs \sin A$$

$$DAE = \frac{1}{2} qr \sin A, \quad EAB = \frac{1}{2} pr \sin A.$$

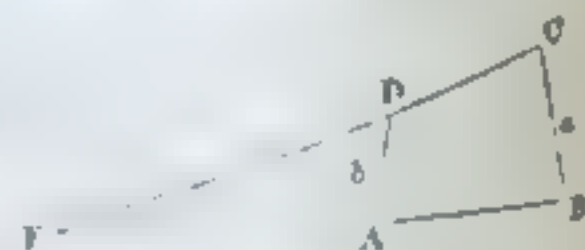
$$\therefore k = \frac{1}{2} (pr + qs + qr + pr) \sin A.$$

$$\text{But } pr + qs + qr + pr = (p + q)(r + s) = dd'.$$

$$\therefore (8) \quad k = \frac{1}{2} dd' \sin A.$$

6. When the angles and two opposite sides are given.

Let $a = BC$, and $b = AD$.
 $E = 180^\circ - (B + C).$



The angles at A being supplementary, their sines are equal. The same is true of the angles at D .

$$ABCD = BCE + ADE, \quad ABCD = k.$$

$$BCE = \frac{a^2 \sin B \sin C}{2 \sin E}, \quad ADE = \frac{b^2 \sin A \sin D}{2 \sin E}.$$

$$\therefore (9) \quad k = \frac{a^2 \sin B \sin C}{2 \sin E} + \frac{b^2 \sin A \sin D}{2 \sin E}.$$

7. When three sides and their included angles are given.

Let a , b , and c be the given sides, and A and B their included angles.



$$ABCD = ABD + DBC.$$

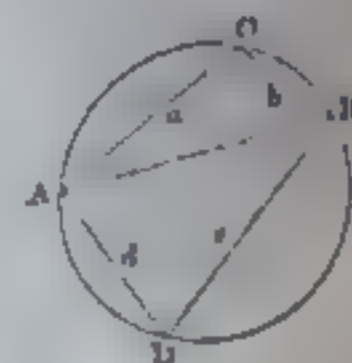
$$ABCD = k, \quad ABD = \frac{1}{2} ab \sin A.$$

$$\text{Find } B' \text{ and } d, \quad B' = B - B', \quad DBC = \frac{1}{2} cd \sin B'.$$

$$\therefore (10) \quad k = \frac{1}{2} ab \sin A + \frac{1}{2} cd \sin B'.$$

8. When the sides of a quadrilateral inscribed in a circle are given.

Let a , b , c , d be the given sides.



$$ACBD = ACB + ADB.$$

$$ACBD = k, \quad ACB = \frac{1}{2} ab \sin C.$$

$$ADB = \frac{1}{2} cd \sin D = \frac{1}{2} cd \sin C,$$

$$\text{since } D = 180^\circ - C.$$

$$\therefore k = \frac{1}{2} (ab + cd) \sin C.$$

$$\overline{AB}^2 = a^2 + b^2 - 2ab \cos C, \text{ article 97.}$$

$$\overline{AB}^2 = c^2 + d^2 - 2cd \cos D = c^2 + d^2 + 2cd \cos C.$$

$$\therefore c^2 + d^2 + 2cd \cos C = a^2 + b^2 - 2ab \cos C.$$

$$\cos C = \frac{a^2 + b^2 - c^2 - d^2}{2(ab + cd)}.$$

$$\sin C = \sqrt{1 - \cos^2 C}, \quad \text{Let } s = a + b + c + d.$$

$$\therefore \sin C = \frac{2 \sqrt{(s-a)(s-b)(s-c)(s-d)}}{ab + cd}.$$

$$\therefore (11) \quad k = \frac{1}{2} (s-a)(s-b)(s-c)(s-d).$$

163. Examples.

1. Two opposite sides of a quadrilateral are 35 rds. and 25 rds., and the perpendiculars to these sides from the extremities of the diagonal are, respectively, 12 rds. and 18 rds.; required the area.

Ans. 410 sq. rds.

2. Find the area of a trapezoid whose bases are 15 rds. and 20 rds., and whose altitude is 18 rds.

Ans. 315 sq. rds.

3. Two adjacent sides of a parallelogram are 30 rds. and 40 rds., and their included angle is 30° ; required the area.

Ans. 600 sq. rds.

4. The diagonal of a quadrilateral is 40 rds., and the two perpendiculars to the diagonal from the vertices of the opposite angles are 10 rds. and 15 rds., respectively; required the area.

Ans. 500 sq. rds.

5. The sides of a quadrilateral are 30 rds., 40 rds., 50 rds., and 60 rds., and the diagonal drawn from the intersection of the sides whose lengths are 30 rds. and 40 rds., is 70 rds.; required the area.

Ans. 1874.22 sq. rds.

6. The sides of a quadrilateral are 25 rds., 35 rds., 45 rds., 55 rds., and the angle included by the sides whose lengths are 35 rds. and 45 rds., is 50° ; required the area.

Ans. 927.47 sq. rds.

7. The diagonals of a quadrilateral are 30 rds. and 40 rds., and their included angle is 30° ; required the area.

Ans. 300 sq. rds.

8. The angles of a quadrilateral are 80° , 110° , 88° , 82° , the side included by the first and second of these angles is 25 rds., and the side included by the third and fourth angles is 45 rds.; required the area.

Ans. 4105.08 sq. rds.

9. Three sides of a quadrilateral are 20 rds., 30 rds., 40 rds., the angle included by the first and second is 60° , and between the second and third, 80° ; required the area.

Ans. 593.58 sq. rds.

10. The sides of a quadrilateral inscribed in a circle are 40 rds., 50 rds., 60 rds., 70 rds.; required the area.

Ans. 2898.28 sq. rds.

11. The area of a parallelogram is 47 055 sq. ft., the sides are 6 ft. and 8 ft.; required the diagonal.

Ans. 9 ft., or 10.906 ft.

12. If the adjacent sides of a parallelogram are b and c , and their included angle A , find A and k when k is a maximum.

Ans. $A = 90^\circ$, $k = bc$.

13. The sides and angles being expressed as in the last example, find A and k when k is a minimum.

Ans. $A = 0^\circ$ or 180° , $k = 0$.

14. If only two adjacent sides, b and c , of a parallelogram be given, prove that k is indeterminate between the limits 0 and bc .

15. Prove that the diagonals of a parallelogram divide it into four equal triangles.

164. Problem.

To find the area of an irregular polygon.

1. When the sides and diagonals from the same vertex are given.

The diagonals divide the polygon into triangles whose sides are given.

The areas of these triangles, k , k' , k'' , ... are found by article 160, (5).

$$\therefore (1) \quad k = k' + k'' + k''' + \dots$$



2. When the diagonals from the same vertex, and the perpendiculars to these diagonals from the opposite vertices are given.

$$(2) \quad k = \frac{1}{2}dp + \frac{1}{2}d'p' + \frac{1}{2}d''p'' + \dots$$



3. When the perpendiculars to a diagonal from the vertices of the opposite angles and the segments of the diagonal made by these perpendiculars are given.

The polygon is divided into right triangles and trapezoids, whose areas k', k'', k''', \dots are found by article 162, (2), (4).

$$(3) \quad k = k' + k'' + k''' + \dots$$



4. When one side of a figure is a straight line, and the opposite side is an irregular curve or broken line.

Let the straight line be divided into the parts a, a', a'', \dots

Let the perpendiculars to p, q, r, s, \dots dividing the figure into part which may be considered trapezoids.



$$(4) \quad k = \frac{1}{2}a(p+q) + \frac{1}{2}a'(q+r) + \frac{1}{2}a''(r+s) + \dots$$

If $a' = a$ and $a'' = a$, (4) becomes,

$$(5) \quad k = \frac{1}{2}a(p + 2q + 2r + s + \dots)$$

165. Examples.

1. Find the area of the annexed polygon if $p = 10$ rds., $d = 6$ rds., $r = 6$ rds., $s = 7$ rds., $t = 15$ rds., $d' = 14$ rds., $d'' = 16$ rds.



Ans. 11686 sq. rds.

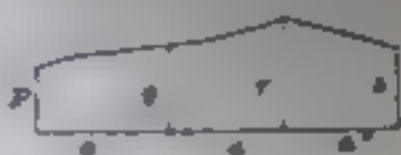
2. Find the area of the annexed polygon if $p = 3$ rds., $d = 9$ rds., $p' = 4$ rds., $d' = 12$ rds., and $p'' = 5$ rds. Ans. 67.5 sq. rds.



3. Find the area of the annexed polygon if $p = 3$ ft., $p' = 5$ ft., $p'' = 4$ ft., $a = 5$ ft., $b = 6$ ft., $c = 6$ ft., $d = 9$ ft., $e = 8$ ft. Ans. 80.5 sq. ft.



4. Find the area of the annexed figure. $p = 2$ rds., $q = 3$ rds., $r = 4$ rds., $s = 3$ rds., $a = a' = a'' = 5$ rds.



Ans. 47.5 sq. rds.

166. Problem.

To find the area of a regular polygon.

1. When the perimeter and apothem are given.

Let p be the perimeter, a the apothem, and s one side of the polygon.

$$k = \frac{1}{2}as + \frac{1}{2}as + \frac{1}{2}as + \frac{1}{2}as + \dots$$

$$k = \frac{1}{2}a(s + s + s + s + \dots)$$

$$\therefore (1) \quad k = \frac{1}{2}ap.$$



2. When the value of each side and the number of sides are given.

Let s be one side, n the number of sides, a the apothem, and p the perimeter.

$$p = ns \quad \text{DOB} = \frac{360^\circ}{2n} = \frac{180^\circ}{n}$$

$$OD = OB \cot \text{DOB, or } a = \frac{1}{2}s \cot \frac{180^\circ}{n}$$



$$\therefore (2) \quad k = \frac{1}{2} ns^2 \cot \frac{180^\circ}{n}.$$

$$\text{If } s = 1, \text{ then } (3) \quad k = \frac{1}{2} n \cot \frac{180^\circ}{n}.$$

From (3) calculate the areas of the regular polygons each of whose sides is 1, as given in the table subjoined.

167. Table.

Triangle = 0.4330127.	Octagon = 4.8284271.
Square = 1.0000000.	Enneagon = 6.1818242.
Pentagon = 1.7204774.	Decagon = 7.6942088.
Hexagon = 2.5980762.	Hendecagon = 9.3656399.
Heptagon = 3.6339124.	Dodecagon = 11.1961524.

168. Application of the Table.

Denoting the area of a regular polygon whose side is s by k , and the area of a similar polygon whose side is 1, as given in the table by k' , and applying the principle that the areas of similar polygons are to each other as the squares of the homologous sides, we have the proportion,

$$k : k' :: s^2 : 1^2. \quad \therefore k = k's^2.$$

169. Examples.

1. What is the area of a regular hexagon each of whose sides is 6? *Ans.* 93.5307432.

2. What is the area of a regular pentagon each of whose sides is 10? *Ans.* 172.04774.

3. What is the area of a regular decagon each of whose sides is 20? *Ans.* 3077.68352.

4. What is the area of a regular dodecagon each of whose sides is 100? *Ans.* 111961.524.

5. What is the area of a regular enneagon each of whose sides is 30? *Ans.* 5563.64178.

170. Formulas for the Circle.

Let r be the radius, d the diameter, c the circumference, and k the area of a circle, then, by Geometry, we have

$$d = 2r, \quad c = \pi d, \quad k = \frac{1}{2}rc.$$

From which verify the following table of formulas:

1. $r = \frac{1}{2}d$	7. $c = 2\pi r$
2. $r = \frac{c}{2\pi}$	8. $c = \pi d$
3. $r = \sqrt{\frac{k}{\pi}}$	9. $c = 2\sqrt{k\pi}$
4. $d = 2r$	10. $k = \pi r^2$
5. $d = \frac{c}{\pi}$	11. $k = \frac{1}{4}\pi d^2$
6. $d = 2\sqrt{\frac{k}{\pi}}$	12. $k = \frac{c^2}{4\pi}$

171. Examples.

1. Given the radius of a circle = 10 rds; required d , c , and k .

2. Given the diameter of a circle = 20 rds.; required r , c , and k .

3. Given the circumference of a circle = 150 rds.; required r , d , and k .

4. Given the area of a circle = 1000 sq. rds.; required r , d , and c .

5. Find the diameter of a circle whose area is equal to that of a regular decagon, each side of which is 10 ft. Ans. 31.5

6. The radius of a circle is 10 ft., the diagonals of an equal parallelogram are 24 ft. and 30 ft.; required their included angle. Ans. $60^\circ 46' 17''$.

7. The radii of two concentric circles are r and r' , find the area of the ring included by their circumferences. Ans. $\pi(r+r')(r-r')$.

172. Problem.

To find the area of a sector of a circle.

Let a be the arc of a sector, d the degrees in the arc, r the radius, and k the area.



By Geometry, (1) $k = \frac{1}{2} ar$.

$\pi r =$ the semi-circumference,

$\frac{\pi r}{180} =$ the arc of 1° . $\therefore \frac{d\pi r}{180} =$ the arc of d° .

(2) $a = \frac{d\pi r}{180}$. \therefore (3) $k = \frac{d\pi r^2}{360}$.

173. Examples.

1. Find the area of a sector whose arc is 40° and radius is 10 ft. Ans. 34.907 sq. ft.

2. Find the area of a sector whose arc is $60^\circ 24' 30''$ and radius is 100 rds. Ans. 5271.64 sq. rds.

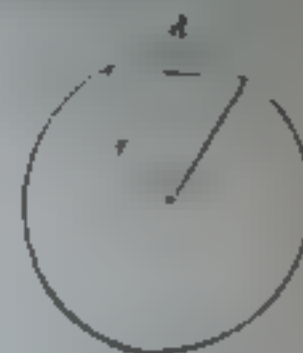
3. The area of a sector is 345 sq. ft., the radius is 20 ft.; required the arc. Ans. $98^\circ 50' 06''$.

4. The area of a sector is 1000 sq. rds., the arc is 30° ; required the radius. Ans. 61.04 rds.

174. Problem.

To find the area of a segment of a circle.

Let d be the degrees in the arc of the segment, r the radius, and k the area.



By the last problem,

$\frac{d\pi r^2}{360}$ the area of the sector.

$\frac{1}{2} r^2 \sin d$ the area of the triangle.

$\therefore k = \frac{d\pi r^2}{360} - \frac{1}{2} r^2 \sin d$.

If d is greater than 180 , $\sin d$ is negative, and the second term in the value of k becomes positive, as it should, since, in this case, the segment is equal to the corresponding sector plus the triangle.

175. Examples.

1. Find the area of the segment of a circle whose arc is 36° and radius 10 ft. Ans. 2.027 sq. ft.

2. Find the area of a segment whose chord is 36 ft. and radius 30 ft. Ans. 147.30 sq. ft.

3. Find the area of a segment whose altitude is 36 rds and radius 50 rds. Ans. 2545.85 sq. rds.

1 The area of a segment is 2545.85 sq. rds., the radius is 50 rds.; required the number of degrees in the arc.

176. Problem.

To find the area of an ellipse

Let a be the semi-major axis, and b the semi-minor axis.



Then, Ray's Analytic Geometry, article 446,

$$k = \pi ab.$$

177. Examples.

1. The semi-axes of an ellipse are 10 in. and 7 in.; required the area. *Ans.* 219.912 sq. in.

2. The area of an ellipse is 125 sq. rds.; find the axes if they are to each other as 3 is to 2.

Ans. 15.45; 10.30.

178. Problem.

To find the area of the entire surface of a right prism

Let p be the perimeter of the base, a the altitude, s one side of the base, K the area of a polygon similar to the base, each side of which is unity, article 167, and k the area of the entire surface.



ap the convex surface

$2 Ks^2$ = the areas of the bases Article 168

$$\therefore k = ap + 2 Ks^2.$$

179. Examples.

1. What is the entire surface of a right prism whose altitude is 20 ft., and base a regular octagon each side of which is 10 ft.?

Ans. 2565.68542 sq. ft.

2. What is the entire surface of a right hexagonal prism whose altitude is 12 ft., and each side of the base is 6 ft.?

Ans. 619.0614864 sq. ft.

3. What is the entire surface of a right prism whose altitude is 15 in., and base a regular triangle each side of which is 3 in.?

Ans. 142.7942286 sq. in.

180. Problem.

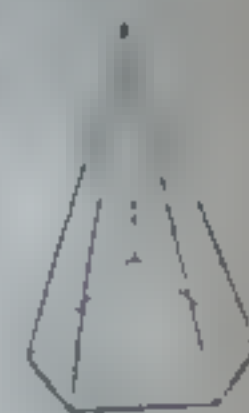
To find the area of the surface of a regular pyramid.

Let p be the perimeter of the base, a the slant height, s one side of the base, K and k as in the last problem.

$\frac{1}{2} ap$ = the convex surface.

Ks^2 = the area of the base.

$$\therefore k = \frac{1}{2} ap + Ks^2.$$



181. Examples.

1. What is the entire surface of a regular pyramid whose slant height is 12 ft., and base a regular triangle each side of which is 5 ft.?

Ans. 100.82532 sq. ft.

2. What is the entire surface of a right pyramid whose slant height is 100 ft., and base a regular hexagon each side of which is 20 ft.?

Ans. 13077.68352 sq. ft.

182. Problem.

To find the entire surface of a frustum of a right pyramid.

Let p be the perimeter of the lower base, p' the perimeter of the upper base, a the slant height, s one side of the lower base, s' one side of the upper base, k and k' as in Art. 178.



$\frac{1}{2}a(p + p') =$ the convex surface.

$k's^2 =$ the area of lower base.

$k's'^2 =$ the area of upper base.

$$\therefore k = \frac{1}{2}a(p + p') + k'(s^2 + s'^2).$$

183. Examples.

1. What is the entire surface of a frustum of a pyramid whose slant height is 12 ft., and the bases regular decagons whose sides are 8 ft and 5 ft. respectively? *Ans.* 1464.78458 sq. ft.

2. What is the entire surface of a frustum of a pyramid whose slant height is 15 ft., and the bases regular hexagons whose sides are 10 ft and 6 ft. respectively? *Ans.* 1073.338 sq. ft.

184. Problem.

To find the area of the entire surface of a cylinder

Let r be the radius of the cylinder, a its altitude, and k the area of the entire surface.

$2\pi r a =$ the convex surface.

$2\pi r^2 =$ the area of the bases.

$$\therefore k = 2\pi r(a + r).$$



185. Examples.

1. What is the entire surface of a cylinder whose altitude is 6 ft. and radius 2 ft.?

Ans. 100.5312 sq. ft.

2. What is the entire surface of a cylinder whose altitude is 100 ft. and radius 20 ft.?

Ans. 15079.68 sq. ft.

186. Problem.

To find the area of the entire surface of a cone

Let r be the radius of the base of the cone, a the slant height, and k the area of the entire surface.

$\pi r a =$ the convex surface.

$\pi r^2 =$ the area of the base.

$$\therefore k = \pi r(a + r).$$



187. Examples.

1. What is the entire surface of a cone whose slant height is 10 ft. and radius 5 ft.? *Ans.* 235.62 sq. ft.

2. What is the entire surface of a cone whose altitude is 100 ft. and radius 25 ft.?

Ans. 10059.1675 sq. ft.

188. Problem.

To find the area of the entire surface of the frustum of a cone.

Let r be the radius of the lower base, r' be the radius of the upper base, a the slant height, and k the area of the entire surface.

radius of the upper base, a the slant height, and k the area of the entire surface.

$\pi(r + r')$ the convex surface.

πr^2 the area of the lower base.

$\pi r'^2$ the area of the upper base.

$$\therefore k = \pi[a(r + r') + r^2 + r'^2].$$



189. Examples.

1. Find the entire surface of the frustum of a cone of which the radius of the lower base is 10 ft., the radius of the upper base is 6 ft., and slant height is 20 ft.
Ans. 1432.5696 sq. ft.

2. Find the entire surface of the frustum of a cone of which the radius of the lower base is 25 in., the radius of the upper base 12 in., and the slant height 36 in.
Ans. 45.8368 sq. ft.

190. Problem.

To find the area of the surface of a sphere.

Let r be the radius, d the diameter, c the circumference, and k the area. Then, by Geometry,

$$(1) \quad k = 4\pi r^2. \quad (2) \quad k = \pi d^2.$$

$$(3) \quad k = \frac{c^2}{\pi}. \quad (4) \quad k = cd.$$

191. Examples.

1. The radius of a sphere is 10 ft.; required the area.
Ans. 1256.64 sq. ft.

2. The diameter of a sphere is 25 ft.; required the area.
Ans. 1963.5 sq. ft.

3. The circumference of a sphere is 100 in.; required the area.
Ans. 3183.0914 sq. in.

4. The circumference of a sphere is 62.832, and diameter 20; required the area.
Ans. 1256.64.

192. Problem.

To find the area of a zone.

By Geometry, the area of a zone is equal to the circumference of a great circle multiplied by the altitude of the zone.

Let a denote the altitude of the zone, r the radius of the sphere, and k the area of the zone.

$$\therefore k = 2\pi ra.$$

193. Examples.

1. What is the area of the torrid zone, calling its width $46^\circ 50'$ and the earth a perfect sphere whose radius is 3956.5 mi?
Ans. 78333333. sq. mi.

2. What is the area of the two frigid zones if the polar circles are $23^\circ 28'$ from the poles?
Ans. 16270370. sq. mi.

3. What is the area of the two temperate zones?

Ans. 102109933. sq. mi.

194. Problem.

To find the area of a spherical triangle.

Let $s = A + B + C$, and $\frac{1}{2}\pi r^2$ = the tri-rectangular triangle.

Then, by Geometry,

$$k = \frac{1}{2}\pi r^2 \left(\frac{s}{90^\circ} - 2 \right).$$



In this formula, $\frac{1}{180}^\circ$ 2 is to be regarded as an abstract number. Minutes and seconds are to be reduced to the decimal of a degree.

195. Examples.

1. Find the area of the spherical triangle whose angles are 60° , 80° , 100° , and the radius 3956.5 mi.

Ans. 16392592 sq. mi.

2. Find the area of a spherical triangle whose sides are 70° , 90° , 100° , respectively, and radius 100 in.

Ans. 10942 1928 sq. in.

196. Problem.

To find the area of a spherical polygon.

Let s be the sum of the angles, n the number of sides, k the area of the polygon, and r the radius of the sphere.

Then, by Geometry,

$$k = \frac{1}{2} \pi r^2 \left[\frac{s}{90^\circ} - 2(n - 2) \right]$$

197. Examples.

1. The sum of the angles of a spherical hexagon is 800° , the radius is 100 ft.; required the area.

Ans. 13963. sq. ft.

2. Each angle of a spherical pentagon is 120° , the radius is 50 ft.; required the area. *Ans.* 2618. sq. ft.

3. The angles of a spherical polygon are 90° , 100° , 110° , 150° , respectively, the radius is 10 ft.; required the area. *Ans.* 157.08 sq. ft.

4. Each angle of a spherical decagon is 150° , the radius is 1 ft.; required the area. *Ans.* 1.0472 ft.

198. Problem.

To find the area of the surface of a regular polyhedron.

Let e be one edge, n the number of faces, k' the area of a polygon whose side is 1, and similar to one face, and k the area of the entire surface.

$k'e^2$ = the area of one face. Article 168.

$$k = nk'e^2.$$

199. Examples.

1. What is the area of the entire surface of a tetrahedron whose edge is 10 ft? *Ans.* 173.20508 sq. ft.

2. What is the area of the entire surface of a hexahedron whose edge is 5 ft.? *Ans.* 150 sq. ft.

3. What is the area of the entire surface of an octahedron whose edge is 20 ft.? *Ans.* 1385.64064 sq. ft.

4. What is the area of the entire surface of a dodecahedron whose edge is 15 in? *Ans.* 32 25895 sq. ft.

5. What is the area of the entire surface of an icosa-hedron whose edge is 100 in.? *Ans.* 601.4065 sq. ft.

MEASUREMENT OF VOLUMES.

200. Problem.

To find the volume of a prism.

Let k be the area of the base, a the altitude, and v the volume. Then, by Geometry,

$$v = ak$$

201. Examples.

1. What is the volume of a regular hexagonal prism whose altitude is 20 ft., and each side of the base 10 ft.?

Ans. 5196.1524 cu. ft.

2. What is the volume of a triangular prism whose altitude is 6 ft., and the sides of its base 3 ft., 4 ft., and 5 ft., respectively?

Ans. 36 cu. ft.

3. What is the volume of a regular octagonal prism whose altitude is 120 ft., and each side of the base 20 ft.?

Ans. 21,764.5008 cu. ft.

202. Problem.

To find the volume of a pyramid.

Let k be the area of the base, a the altitude, and v the volume.

$$v = \frac{1}{3}ak.$$

203. Examples.

1. What is the volume of a pyramid whose altitude is 15 ft., and whose base is a regular heptagon each side of which is 5 ft.?

Ans. 454.23905 cu. ft.

2. What is the volume of a pyramid whose altitude is 21 in., and whose base is a triangle each side of which is 30 in.?

Ans. 2727.98 cu. in.

204. Problem.

To find the volume of the frustum of a pyramid.

Let k and k_1 be the areas of the bases, a the altitude, and v the volume. Then, by Geometry,

$$(1) \quad v = \frac{1}{3}a(k + k_1 + \sqrt{kk_1}).$$

If the bases are regular polygons whose sides are s and s' , we shall have, by article 168, $k = Ks^2$, and $k_1 = Ks'^2$, in which K is given in the table of article 167, and (1) becomes

$$(2) \quad v = \frac{1}{3}a(s^2 + s'^2 + ss')K.$$

205. Examples.

1. What is the volume of the frustum of a pyramid whose altitude is 9 ft., and whose bases are regular triangles, one side of the lower being 8 ft., and one side of upper, 5 ft.?

Ans. 167.576 cu. ft.

2. What is the volume of the frustum of a pyramid whose altitude is 27 in., and the bases regular hexagons, the sides of which are 10 in. and 6 in., respectively?

Ans. 4583.0064 cu. in.

206. Problem.

To find the volume of a cylinder.

Let r represent the radius, a the altitude, and v the volume.

$$v = a\pi r^2.$$

207. Examples.

1. What is the volume of a cylinder whose altitude is 50 in., and radius 15 in.?

Ans. 20433 cu. ft.

2. What is the volume of a cylinder whose altitude is 25 ft., and radius 4 ft.?

Ans. 1256.64 cu. ft.

208. Problem.

To find the volume of a cone.

Let r be the radius of the base, a the altitude, and v the volume.

$$v = \frac{1}{3} a \pi r^2.$$

209. Examples.

1. What is the volume of a cone whose altitude is 21 in., and radius 10 in.? *Ans.* 2199.12 cu. in.

2. What is the volume of a cone whose altitude is 30 ft., and radius is 10 ft.? *Ans.* 31416. cu. ft.

210. Problem.

To find the volume of the frustum of a cone.

Let r and r' be the radii of the bases, a the altitude, and v the volume.

$$v = \frac{1}{3} a \pi (r^2 + r'^2 + rr')$$

211. Examples.

1. What is the volume of the frustum of a cone whose altitude is 15 ft., and the radii of whose bases are 9 ft. and 4 ft., respectively? *Ans.* 2089.164 cu. ft.

2. How many barrels will that cistern contain whose altitude is 8 ft., the diameter at the bottom 4 ft., and at the top 6 ft.? *Ans.* 37.8 bbl.

212. Formulas for the Sphere.

Let r be the radius, d the diameter, c the circumference, k the area of the surface, and v the volume

of a sphere, then, by Geometry, we have

$$d = 2r, \quad c = \pi d, \quad k = 4\pi r^2, \quad v = \frac{4}{3} \pi r^3.$$

From which verify the following table of formulas:

1. $r = \frac{1}{2} d.$	11. $c = \pi \sqrt{k}.$
2. $r = \frac{c}{2\pi}.$	12. $c = \sqrt[3]{6\pi v}.$
3. $r = \frac{1}{2} \sqrt{\frac{k}{\pi}}.$	13. $k = 4\pi r^2.$
4. $r = \frac{1}{2} \sqrt{\frac{6v}{\pi}}.$	14. $k = \pi d^2.$
5. $d = 2r.$	15. $k = \frac{c^2}{\pi}.$
6. $d = \frac{c}{\pi}.$	16. $k = \sqrt[3]{36\pi v}.$
7. $d = \sqrt{\frac{k}{\pi}}.$	17. $v = \frac{4}{3} \pi r^3.$
8. $d = \sqrt[3]{\frac{6v}{\pi}}.$	18. $v = \frac{1}{6} \pi d^3.$
9. $c = 2\pi r.$	19. $r = \frac{c}{2\pi}.$
10. $c = \pi d.$	20. $r = \frac{k}{6} \sqrt{\frac{k}{\pi}}.$

213. Examples.

1. Calling the diameter of the earth 7913 mi., and the diameter of the sun 856,000, find the ratio of their surfaces, also the ratio of their volumes.

2. What is the volume of the shell of a hollow sphere whose radius is 8 ft. 4 in., and the thickness of the shell 3 ft. 6 in.? *Ans.* 1951.1081 cu. ft.

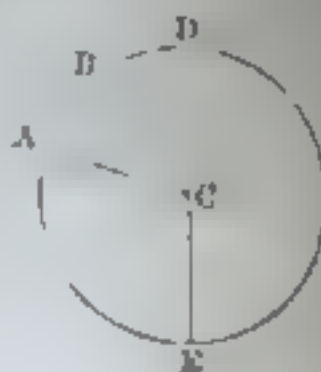
214. Problem.

To find the volume of a spherical sector.

A spherical sector is the volume generated by the revolution of any circular sector, ABC , about any diameter, DE . By Geometry, the volume of a spherical sector is equal to the zone which forms its base, multiplied by one-third of the radius.

Let a be the altitude of the zone, and r the radius.

$$\therefore v = \frac{2}{3} \pi r^2 a.$$



215. Examples.

1. The altitude of the zone which forms the base of a sector is 6 ft., the radius is 12 ft.; required the volume.
Ans. 1809.5616 cu. ft.

2. The angle BCD , in the diagram of last article, is 20° . ACB is 35° , $r = 20$ ft.; required the volume.
Ans. 6134.25 cu. ft.

216. Problem.

To find the volume of a spherical segment.

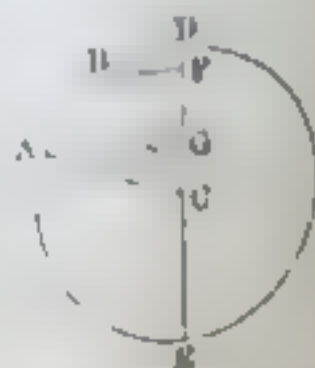
A spherical segment is the portion of a sphere included between two parallel planes.

Let $r' = BF$ perpendicular to DE , and $r'' = AG$ perpendicular to DE .

r = the radius, $d' = CF$, and $d'' = CG$.

v = the vol. generated by $ABFG$.

v' = the vol. generated by $ABC = \frac{2}{3} \pi r^2 a$.



v'' = the vol. generated by $BFC = \frac{1}{3} d' \pi r'^2$.

v''' = the vol. generated by $AGC = \frac{1}{3} d'' \pi r''^2$.

$$v = v' + v'' \mp v'''.$$

The sign of v''' is — or + according as AG is on the same or opposite side of the center as BF .

$$\therefore v = \frac{1}{3} \pi (2 ar^2 + d' r'^2 + d'' r''^2).$$

217. Examples.

1. $r = 12$ in., $r' = 3$ in., $r'' = 10$ in.; required v .

2. Two parallel planes divide a sphere whose diameter is 36 in. into three equal segments; required the altitude of each. *Ans.* 13.93 in.; 8.14 in.; 13.93 in.

218. Problem.

To find the volume generated by the revolution of a circular segment about a diameter exterior to it.

Let v = vol. generated by ADB .

v' = vol. generated by $ADBC$.

v'' = vol. generated by ABC .

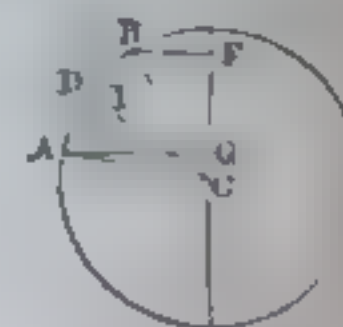
$$v = v' - v''.$$

Let $a = FG$, $c = AB$, $p = CI$, perpendicular to AB .

$$v' = \frac{2}{3} \pi ar^2, \quad v'' = \frac{2}{3} \pi ap^2.$$

$$\therefore v = v' - v'' = \frac{2}{3} \pi a (r^2 - p^2) = \frac{1}{3} \pi ac^2.$$

$$v = \frac{1}{3} \pi ac^2.$$



219. Examples.

1. $a = 5$ in., $c = 8$ in.; find v . *Ans.* 167.552 cu. in.

2. A sphere 6 in. in diameter is bored through the center with a 3-inch auger; required the volume remaining.

Ans. 73.457 cu. in.

3. Prove that the volume generated by the segment whose altitude is a and chord c is to the sphere whose diameter is c as $a : c$.

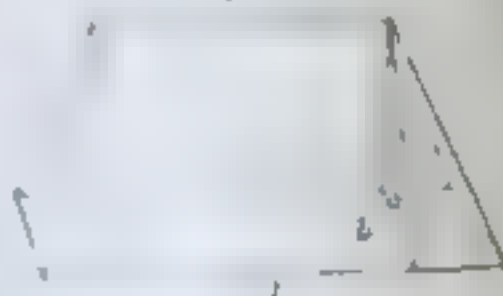
4. Prove that if c is parallel to the diameter about which it is revolved, the volume generated by the segment is equal to the volume of a sphere whose diameter is c .

220. Problem.

To find the volume of a wedge.

The base is a rectangle, the sides are trapezoids, the ends, triangles.

Let c be the edge, l the length of base, b the breadth of base, and a the altitude.



Passing planes through the extremities of the edge perpendicular to the base, we have a triangular prism and two pyramids. These pyramids may fall within or without the wedge, or one or both of the pyramids may vanish.

But in all cases the formula is the same.

$\frac{1}{2}abe =$ the volume of the prism.

$\frac{1}{3}a(l - e)b =$ the volume of the pyramids.

$$\therefore v = \frac{1}{6}ab(2l + e).$$

221. Examples.

1. The edge of a wedge is 6 in., the altitude 12 in., the length of base 9 in., and the breadth of base 5 in.; what is the volume?

Ans. 240 cu. in.

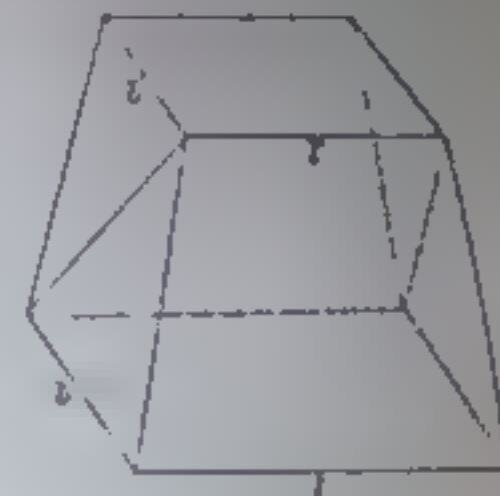
2. The edge of a wedge is 20 ft., the altitude 24 ft., the length of base 15 ft., the breadth of base 10 ft.; what is the volume?

Ans. 2000 cu. ft.

222. Problem.

To find the volume of a rectangular prismoid.

The bases are parallel rectangles, the other faces are trapezoids.



Let l and b be the length and breadth of the lower base, l' and b' the length and breadth of the upper base, and a the altitude.

Passing the plane as indicated, the prismoid is divided into two wedges.

$\frac{1}{6}ab(2l + l') =$ the vol. of wedge whose base is bl .

$\frac{1}{6}ab'(2l' + l) =$ the vol. of wedge whose base is $b'l'$.

$$\therefore v = \frac{1}{6}a[b(2l + l') + b'(2l' + l)].$$

223. Examples.

1. The length and breadth of the lower base of a rectangular prismoid are 25 ft. and 20 ft., the length and breadth of the upper base are 15 ft. and 10 ft., and the altitude is 18 ft.; what is the volume?

Ans. 5550 cu. ft.

2. The length and breadth of the lower base of a rectangular prismoid are 15 yds. and 10 yds., the length and breadth of the upper base are 9 yds. and 6 yds., and the altitude is 18 yds.; what is the volume?

Ans. 1764 cu. yds.

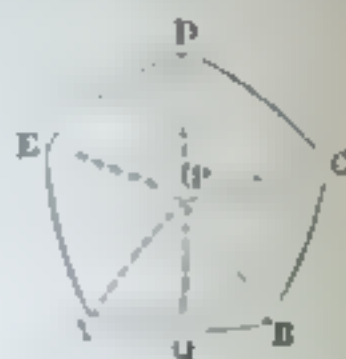
224. Problem.

To find the dihedral angle included by the faces of a regular polyhedron.

Conceive a sphere whose radius is 1 so placed that its center shall be at any vertex of the polyhedron.

The faces of the polyhedral angle will intersect the surface of the sphere in a regular polygon whose sides measure the plane angles that include the polyhedral angle, and whose angles are each equal to the required dihedral angle.

Let $ABCD$ be such a polygon, P the pole of a small circle passing through A, B, C, D, E . Join P with the vertices and with the middle of AB by arcs of great circles.



Let n denote the number of sides of the polygon, $s =$ one side, and $A =$ a dihedral angle.

$$\therefore APQ = \frac{360^\circ}{2n} = \frac{180^\circ}{n}, \text{ and } AQ = \frac{1}{2}s.$$

By Napier's circular parts, we have

$$\sin(90^\circ - APQ) = \cos AQ \cos(90^\circ - PAQ).$$

$$\text{or } \sin\left(90^\circ - \frac{180^\circ}{n}\right) = \cos \frac{1}{2}s \cos\left(90^\circ - \frac{1}{2}A\right).$$

$$\text{or } \cos \frac{180^\circ}{n} = \cos \frac{1}{2}s \sin \frac{1}{2}A.$$

$$\therefore \sin \frac{1}{2}A = \frac{\cos \frac{1}{n}180^\circ}{\cos \frac{1}{2}s}.$$

In the Tetrahedron, $n = 3$, and $s = 60^\circ$,

$$\therefore \sin \frac{1}{2}A = \frac{\cos 60^\circ}{\cos 30^\circ} \therefore A = 70^\circ 31' 42''.$$

In the Hexahedron, $n = 3$, and $s = 90^\circ$,

$$\therefore \sin \frac{1}{2}A = \frac{\cos 60^\circ}{\cos 45^\circ} \therefore A = 90^\circ,$$

In the Octahedron, $n = 4$, and $s = 60^\circ$,

$$\therefore \sin \frac{1}{2}A = \frac{\cos 45^\circ}{\cos 30^\circ} \therefore A = 109^\circ 28' 18''.$$

In the Dodecahedron, $n = 3$, and $s = 108^\circ$,

$$\therefore \sin \frac{1}{2}A = \frac{\cos 60^\circ}{\cos 54^\circ} \therefore A = 116^\circ 33' 54''.$$

In the Icosahedron, $n = 5$, and $s = 60^\circ$,

$$\therefore \sin \frac{1}{2}A = \frac{\cos 36^\circ}{\cos 30^\circ} \therefore A = 138^\circ 11' 23''.$$

225. Problem.

To find the volume of a regular polyhedron.

If planes be passed through the edges of the polyhedron and the center, they will bisect the dihedral angles and divide the polyhedron into as many pyramids as it has faces. The faces will be the bases of the pyramids, the center will be their common vertex, the line drawn from the center of the polyhedron to the center of any base will be perpendicular to the base, and will be the altitude of the pyramid.

From the foot of the perpendicular draw a perpendicular to one side of the base, and join the foot of this perpendicular with the center. We thus have a right triangle whose perpendicular is the altitude of the pyramid, the base the apothem of one face of the polyhedron, the angle opposite the perpendicular one-half the dihedral angle of the polyhedron.

Let p be the perpendicular, a the apothem of one face, $\frac{1}{2}A$ one-half of a dihedral angle, n the number of sides of one face, and e one edge.

$$p = a \tan \frac{1}{2} A, \quad a = \frac{1}{2} e \cot \frac{1}{2} 180^\circ. \quad \text{Article 166.}$$

$$\therefore p = \frac{1}{2} e \cot \frac{1}{2} 180^\circ \tan \frac{1}{2} A.$$

Let K , n , and k be the same as in article 198.

Then, $\frac{1}{3} p k =$ the volume of the polyhedron.

$$\therefore v = \frac{1}{3} n k e^3 \cot \frac{1}{2} 180^\circ \tan \frac{1}{2} A.$$

Let $e = 1$, and verify the table subjoined:

226. Table.

Names.	Surfaces.	Volume
Tetrahedron	1.7320508	0.1178513
Hexahedron	6.0000000	1.0000000
Octahedron	3.4641016	0.4714045
Dodecahedron	20.6457288	7.6631189
Icosahedron	8.6602540	2.1816950

227. Application of the Table.

Let v' and v denote similar regular polyhedrons whose edges are 1 and e , respectively. Then we have

$$v' : v :: 1^3 : e^3. \quad \therefore v = v' e^3.$$

228. Examples.

1. What is the volume of a tetrahedron whose edge is 10 ft.?

Ans. 117.8513 cu. ft.

2. The volume of a hexahedron is 134217728 cu. in.; what is its surface?

Ans. 1572864 sq. in.

SURVEYING.

229. Definition and Classification.

Surveying is the art of laying out, measuring, and dividing land, and of representing on paper its boundaries and peculiarities of surface.

There are three branches—*Plane*, *Geodesic*, and *Topographical*.

Plane surveying is that branch in which the portion surveyed is regarded as a plane, as is the case in small surveys.

Geodesic surveying is that branch in which the curvature of the surface of the earth is taken into consideration, as is the case in all extensive surveying.

Topographical surveying is that branch in which the slope and irregularities of the surface, the course of streams, the position and form of lakes and ponds, the situation of trees, marshes, rocks, buildings, etc., are considered and delineated.

INSTRUMENTS.

230. Classification.

The instruments employed in surveying may be classed as *Field instruments* and *Plotting instruments*.

The principal field instruments are the *chain* and *tally pins*, *marking tools*, *field-book* and *pencil*, the

compass, the solar compass, the transit compass, the level, and the theodolite.

The principal plotting instruments are the divider, the ruler and triangle, parallel rulers, the diagonal scale, the semicircular protractor.

231. The Chain and Tally Pins.

The chain is 4 rods or 66 feet in length, and is divided into 100 links, each equal to 7.92 inches.

After every tenth link from each end is a piece of brass, notched so as to indicate the number of links from the end of the chain, thus facilitating the counting of the links.

A half-chain of 50 links is sometimes used, especially in rough or hilly districts.

The tally pins are made of iron or steel, about 12 inches in length and one-eighth of an inch in thickness, heavier toward the point, with a ring at the top in which is fastened a piece of cloth of some conspicuous color.

These pins are conveniently carried by stringing them on an iron ring attached to a belt which is passed over the right shoulder, leaving the pins suspended at the left side.

In Government surveys eleven tally pins are used.

232. Marking Tools.

A surveying party will need an *ax* for cutting notches, cutting and driving stakes and posts; a *spade* or *mattock* for planting or finding corners; *knives*, or other tools, for cutting letters or figures; and a *file* and *whetstone* for keeping the tools in order.

233. Field-Book and Pencil.

In ordinary practice one field-book will be sufficient; but in surveying the public lands, four different books are required—one for meridian and base lines, another for standard parallels or correction lines, another for exterior or township lines, and another for subdivision or section lines, as designated on the title-page.

A good pencil, number 2 or 3, well sharpened, should be used, so that the notes may be legible.

A temporary book may be used on the ground, and the notes taken with a pencil. These notes can then be carefully transcribed with pen and ink into the permanent field-book.

234. The Magnetic Compass.

The vernier magnetic compass is exhibited in the drawing on page 189.

The needle turns on a pivot at the center, and settles in the magnetic meridian.

The compass circle is divided, on its upper surface, to half-degrees, numbered from 0° to 90° each side of the line of zero.

The eight standards are firmly fastened at right angles to the plate by screws, and have slits cut through nearly their whole length, terminated at intervals by apertures through which the object toward which the sights are directed can be readily found.

Two spirit levels at right angles to each other are attached to the plate.

Tangent scales are scales on the right and left sides of the north sight standard, the one on the right is

ing used in taking angles of elevation, and the one on the left in taking angles of depression.

Eye-pieces are placed on the right and left sides of the south sight standard—the one on the right near the bottom, the one on the left near the top—each on a level, when the compass is level, with the zero of its tangent scale. These eye-pieces are centers of arcs tangent to the tangent scales at the zero point.

The **vernier** is a scale movable by the side of another scale, and divided into parts each a little greater or a little less than a part of the other and having a known ratio to it. In the drawing the vernier is represented on the plate near the south sight.

The **needle lifter** is a concealed spring, moved from beneath the main plate, by which the needle may be lifted to avoid blunting the point of the pivot in transporting the instrument.

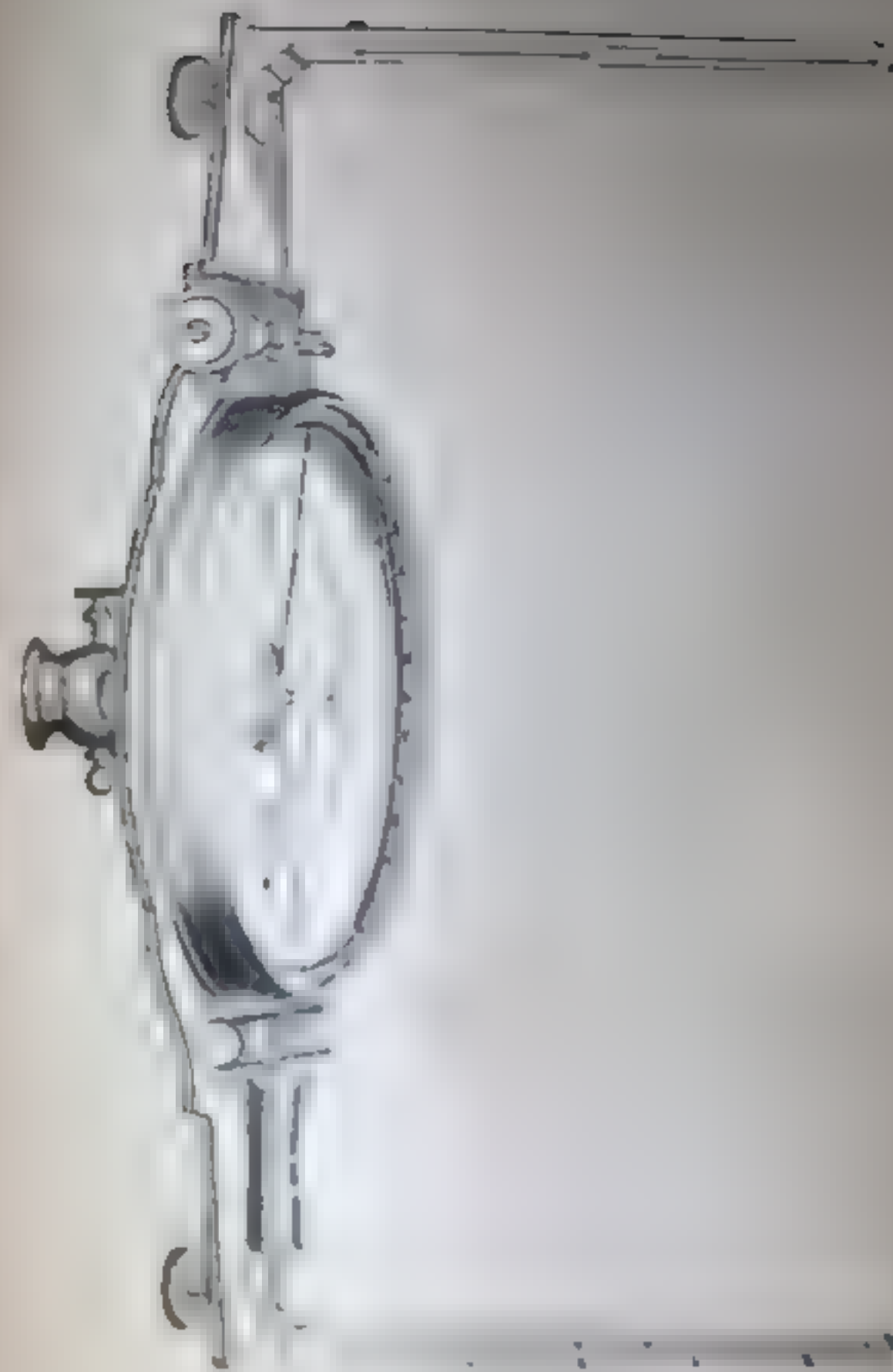
The **out-keeper** is a small dial plate, having an index turned by a milled head, and is used in keeping tally in chaining.

The **ball spindle** is a small shaft, slightly conical, to which the compass is fitted, having on its lower end a ball confined in a socket by a light pressure, so that the ball can be moved in any direction in leveling the instrument.

The **clamp screw** is a screw in the side of the hollow cylinder or socket, which fits to the ball spindle, by which the compass may be clamped to the spindle in any position.

A **spring catch**, fitted to the socket, slips into a groove when the instrument is set on the spindle, and secures it from slipping from the spindle when carried.

THE MAGNETIC COMPASS.



The **Jacob staff** is a single staff to support the compass, about 5½ feet long, having at the upper end a ball and socket joint, and terminating at the lower end in a sharp steel point, so as to be set easily in the ground.

The **tripod** is a three-legged support sometimes used instead of the Jacob staff.

235. Adjustments of the Compass.

1. **To adjust the level.**—Bring the bubbles to the center of the tubes by pressing the plates so as to turn the ball slightly in its sockets. Turn the compass half-way round, and if either bubble runs to one end of its tube, that end is the higher. Loose the screw under the lower end, and tighten the one at the higher end till the bubble is brought half-way back. Level the plate again, and repeat the operation till the bubble will remain in the center during an entire revolution of the compass.

2. **To adjust the sights.**—Observe through the slits a fine thread made plumb by a weight. If both sights do not exactly range with the thread, file a little off the under surface of the highest side.

3. **To adjust the needle.**—Bring the eye nearly in the same plane with the graduated circle, move with a splinter one end of the needle to any division of the circle, and observe whether the other end corresponds with the division 180° from the first; if so, the needle is said to cut opposite degrees; if not, bend the center pin with a small wrench about one-eighth of an inch below the point, till the ends of the needle cut opposite degrees. Hold the needle in the same direction, turn the compass half-way round, and again see

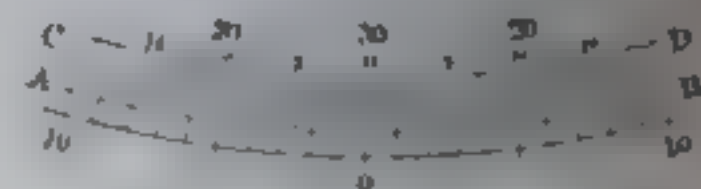
whether the needle cuts opposite degrees; if not, correct half the error by bending the needle, and the remainder by bending the center pin, and repeat the operation till perfect reversion is secured in the first position.

Try the needle in another quarter, and correct by bending the center pin only, since the needle was straightened by the previous operation, and repeat the operation in different quarters.

The adjustments are made by the maker of the instrument, but the instrument can be re-adjusted by the surveyor when necessary.

236. Nature of the Vernier.

Let the arc or limb *AB*, on the main plate of the instrument, be graduated to one-half degrees or 30', numbered each way from 0 at the middle; and let the vernier *CD*, attached to the compass box, which is movable around the main plate, be so graduated that 30 spaces of the vernier shall be equal to 31 spaces of the limb, that is, equal to $31 \times 30'$; then 1 space of the vernier will be equal to 31', and the difference between one space of the vernier and one space of the limb will be $31' - 30' = 1'$.



The vernier is numbered in two series: the lower, nearer the spectator, who is supposed to stand at the south end of the instrument, is numbered 5, 10, 15, each way from 0; the upper series has 80 above the 0, from the observer, and 20 each way above the 10 of the lower series.

Let, now, the 0 points of the vernier and limb coincide; then, if the vernier be moved forward 1 to

the right, which is done by means of a tangent screw, the first division line of the vernier at the left of its 0 will coincide with the first division line of the limb at the left of its 0; if the vernier be moved forward 2 to the right, then the second division line of the vernier at the left of its 0 will coincide with the second division line of the limb at the left of its 0.

If the vernier be moved to the right so that its fifteenth division line at the left of its 0 shall coincide with the fifteenth division line of the limb at the left of its 0, the vernier will have moved forward 15'.

If the vernier be moved more than 15', the excess over 15' is found by reading the division line, in the vernier, which coincides with a division line of the limb, from the upper row of figures on the vernier, on the other side of 0, and so on, up to 30', when the 0 of the vernier will coincide with the first division line from the 0 of the limb.

If the vernier is moved more than 30', the excess over 30', up to 15' and then to 30' is found as before.

If the 0 of the vernier coincides with a division line of the limb, the reading of the division line of the limb will be the true reading.

If the 0 of the vernier has passed one or more division lines of the limb, and does not coincide with any, read the limb from its 0 point up to its division next preceding the 0 of the vernier; to this add the reading of the vernier, and the sum will be the true reading.

If the vernier be moved to the left, the minutes must be read off on the vernier scale to the right.

Sometimes the spaces of the vernier are less than the spaces of the limb; then if the vernier be moved

either way, the minutes must be read off the same way from the 0 of the vernier. Verniers may be so graduated as to read to any appreciable angle; but the graduation which reads to minutes is the most common.

237. Uses of the Vernier.

1. To turn off the variation.—Let the instrument be placed on some definite line of an old survey, and the tangent screw be turned till the needle indicates the same bearing for the line as that given in the field notes of the original survey.

Then will the reading of the limb and vernier indicate the variation.

2. To retrace an old survey.—Turn off the variation as above, and screw up the clamping nut beneath, then old lines can be retraced from the original notes without further change of the vernier.

3. To run a true meridian.—The absolute variation of the needle being known, not simply its change since a given date, move the vernier to the right or left according as the variation is west or east, till the given variation is turned off, screw up the clamping nut beneath, and turn the compass till the needle is made to cut zero, then will the line of sights indicate a true meridian.

Such a change in the position of the vernier is necessary in subdividing the public lands, after the principal lines have been truly run with the solar compass.

4. To read the needle to minutes.—Note the degrees given by the needle, then turn back the compass circle, with the tangent screw, till the nearest whole degree mark coincides with the point of the needle: the space

passed over by the vernier will be the minutes which, added to the degrees, will give the reading of the line in minutes.

This operation is simplified when the 0 of the vernier is first made to coincide with the 0 of the limb, otherwise the difference of the two readings of the vernier must be taken.

239. Uses of the Compass.

1. **To take the bearing of a line.** Place the compass on the line, turn the north end in the direction of the course, and, standing at the south end direct the sights to some well-defined object, as a flag-staff, in the course. Read the bearing from the north end of the needle, which can be done accurately to quarter-degrees by observing the position of the point of the needle, since the compass circle is divided into half-degrees.

It will be observed that the letters *E* and *W*, on the face of the compass, are reversed from their true position. This is as it should be; for if the sights are turned toward the west, the north end of the needle is turned toward the letter *W*. If the north end of the needle is turned toward *E*, the sights will be turned toward the east. If the north end of the needle point exactly to either letter *E* or *W*, the sights will range east or west.

In general, to guard against error, let the surveyor turn the letter *S* toward himself, and read the arc cut off by the north end of the needle from the nearest zero of the compass circle. If, for example, the nearest 0 is at *S*, and the north end of the needle is turned toward *E*, cutting off 25° from this 0, then the course is *S* 25° *E*.

If it is desired to find the bearing to minutes, the vernier must be used.

2. **To run from a given point a line having a given bearing.**—Place the compass over the point, and turn it so that the reading of the needle shall be the given bearing; the line of sights observed from the south end of the compass will be the required line.

3. **To take angles of elevation.** Level the compass, bring the south end toward you, place the eye at the eye-piece on the right side of the south sight, and, with the hand, fix a card on the front surface of the north sight, so that its top edge shall be at right angles to the divided edge and coincide with the zero mark; then, sighting over the top of the card, note upon a flag-staff the height cut by the line of sight, move the staff up the elevation, and carry the card along the sight until the line of sight again cuts the same height on the staff, read off the degrees and half-degrees passed over by the card, and the result will be the angle required.

4. **To take angles of depression.**—Proceed in the same manner, using the eye-piece and scale on the opposite sides of the sights, and reading from the top of the standard.

239. Surveyor's Transit.

The Surveyor's transit exhibited in the drawing on page 197 is, in fact, a *transit theodolite*, combining the advantages of the ordinary transit and the theodolite.

The vernier plate, carrying two horizontal verniers, two spirit levels at right angles, the telescope and attachments, moves around a circle graduated to half-degrees, so that, by the vernier, horizontal angles can be taken to minutes, and any variation turned off.

The telescope and its attachments, the clamp and tangent screw, the vertical circle, the level and the sights, give to this instrument a great advantage over the ordinary compass.

The cross wires, two fine fibers of spider's web, extending across the tube at right angles, intersect in a point which, when the wires are adjusted, determines the optical axis or line of collimation of the telescope, and enables the surveyor to fix it upon an object with great precision.

The clamp and tangent screw consist of a ring encircling the axis of the telescope, having two projecting arms—the one above, slit through the middle, holding the clamp screw; the other, longer, connected below with the tangent screw.

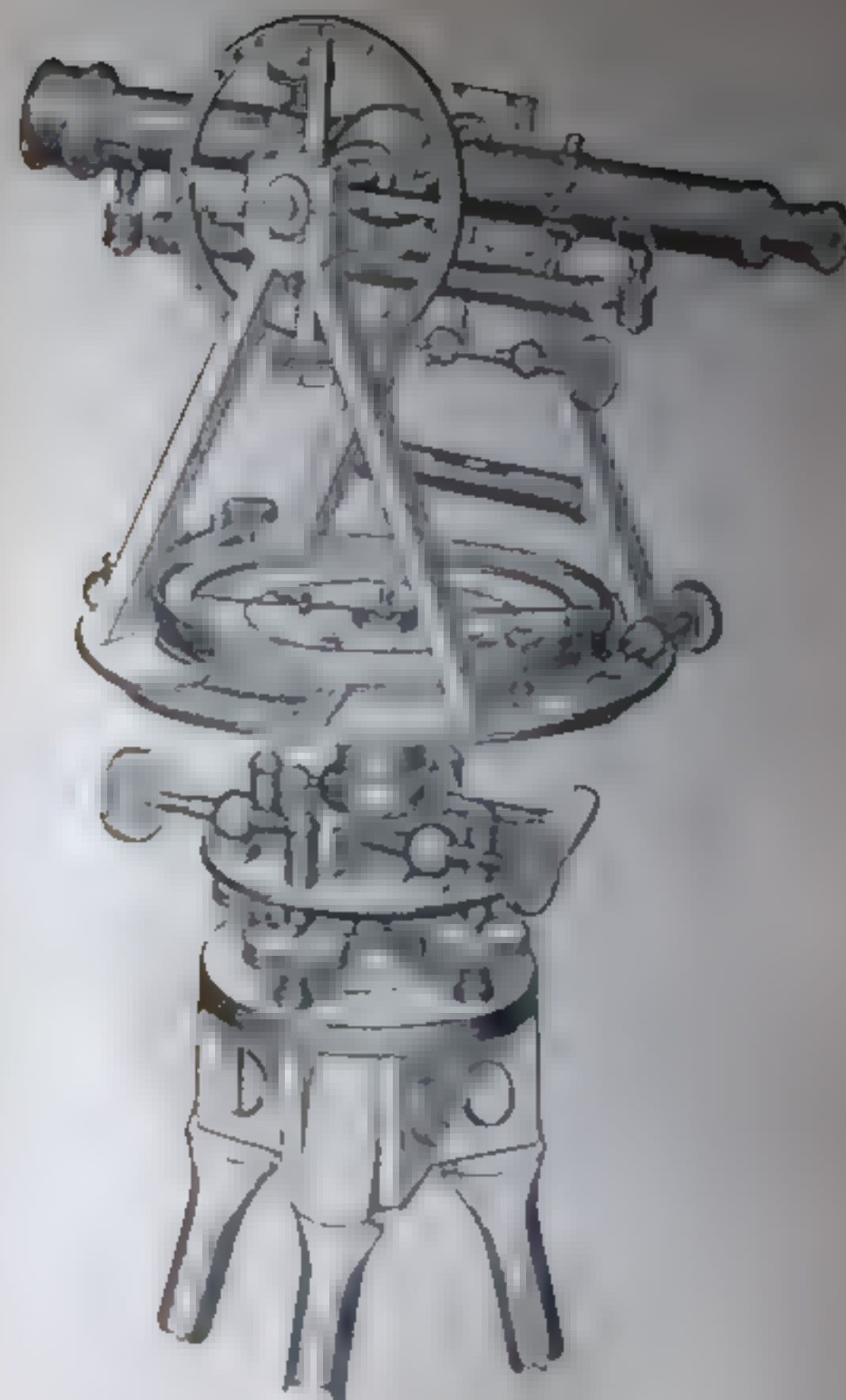
The ring is brought firmly around the axis by means of the clamp screw, and the telescope can be moved up or down by turning the tangent screw.

The vertical circle, graduated to half-degrees, is attached to the axis of the telescope, and, in connection with the vernier, gives the means of measuring vertical angles to minutes with great facility.

The level attached to the telescope enables the surveyor to run horizontal lines, or to find the difference of level between two points.

Sights on the telescope are useful in taking backsights without turning the telescope, and in sighting through bushes or woods.

Sights for right angles attached to the plate of the instrument, or to the standards supporting the telescope, afford the means of laying off right angles, or running out offsets without changing the position of the instrument.



SURVEYOR'S TRANSIT.

240. Adjustments.

1 The levels are adjusted in the same manner as those of the compass, and when adjusted should keep their position if the two plates are clamped together and turned on a common socket.

2 The needle is adjusted as in the compass.

3 The line of the collimation is adjusted by bringing the intersection of the wires into the optical axis of the telescope, which is accomplished as follows:

Set the instrument firmly on the ground and level it carefully, then, having brought the wires into the focus of the eye-piece, adjust the object glass on some well defined object, as the edge of a chimney, at a distance of from two to five hundred feet. Determine whether the vertical wire is plumb by clamping the instrument firmly to the spindle, and applying the wire to the vertical edge of a building, or observing if it will move parallel to a point a little to one side; if it does not, loosen the cross-wire screws, and, by the pressure of the hand on the head outside the tube, move the ring within the tube to which the wires are attached, gently around till the error is corrected.

The wires being thus made respectively horizontal and vertical, fix their point of intersection on the object selected, clamp the instrument to the spindle, and, having revolved the telescope, find or place some object in the opposite direction, at about the same distance from the instrument as the first object.

Great care should be taken in turning the telescope not to disturb the position of the instrument upon the spindle.

Having found an object which the vertical wire bisects, unclamp the instrument, turn it half-way round,

and direct the telescope to the first object selected, and having bisected this with the wires, again clamp the instrument, revolve the telescope and note if the vertical wire bisects the second object observed; if so, the wires are adjusted, and the points bisected are, with the center of the instrument, in the same straight line.

If the vertical wire does not bisect the second point, the space which separates this wire from that point is double the distance of that point from a straight line drawn through the first point and the center of the instrument, as is shown thus:



Let *A* represent the center of the instrument, *BC* the line on whose extremities, *B* and *C*, the line of collimation is to be adjusted, *B* the first object, and *D* the point which the wires bisected after the telescope was made to revolve on its axis. The side of the telescope which was up when the object glass was directed to *B*, is down when the object glass is turned toward *D*. When the telescope is unclamped from its spindle and turned half-way round its vertical axis, and again directed to *B*, the side of its tube which was down when the object glass was first directed to *B* will now be up. Then clamping the instrument, and revolving the telescope about its axis, and directing it toward *D*, the side of its tube which was down when the object glass was first turned toward *D* will now be up, or the telescope will virtually have revolved about its optical axis, and the vertical wire will appear at *E* as far on one side of *C* as *D* is on the other side.

To move the vertical wire to its true position, turn the adjusting screws on the sides of the telescope, remembering that the eye piece inverts the position of the wire, and, therefore, that in loosening one of the screws and in tightening the other the operator must proceed as if to increase the error. Having moved back the vertical wire, as nearly as can be judged, so as to bisect the space *ED*, unclamp the instrument, direct the telescope as at first, so that the cross wires bisect *B*, proceed as before, and continue the operation till the two points *D* and *E* coincide at *C*.

4. The standards must be of the same height, in order that the wires may trace a vertical line when the telescope is turned up or down. To ascertain this, and to make the correction, proceed as follows:

Having the line of collimation previously adjusted, set the instrument in a position where points of observation, such as the point and base of a lofty spire, can be selected, giving a long range in a vertical direction.

Level the instrument, fix the wires on the top of the object, and clamp to the spindle; then bring the telescope down till the wires bisect some good point, either found or marked at the base; turn the instrument half around, fix the wires on the lower point, clamp to the spindle, and raise the telescope to the highest object, and if the wires bisect it, the vertical adjustment is effected.

If the wires are thrown to one side, the standard opposite that side is higher than the other.

The correction is made by turning a screw underneath the sliding piece of the bearing of the movable axis.

5. The vertical circle is adjusted thus: First carefully level the instrument, bring the zeros of the wheel and vernier into line, and find or place some well defined point which is cut by the horizontal wire; then turn the instrument half-way around, revolve the telescope, fix the wire on the same point as before, note if the zeros are again in line.

If not, loosen the screws, move the zero over half the error, and again bring the zeros into coincidence, and proceed as before till the error is corrected.

6. The level on the telescope can be adjusted thus: First level the instrument carefully, and with the clamp and tangent movement to the axis make the telescope horizontal as nearly as possible with the eye. Then, having the line of collimation previously adjusted, drive a stake at a distance of from one to two hundred feet, and note the height cut by the horizontal wire upon a staff set on the top of the stake.

Fix another stake in the opposite direction, at the same distance from the instrument, and, without disturbing the telescope, turn the instrument upon its spindle, set the staff upon the stake and drive in the ground till the same height is indicated as in the first observation.

The top of the two stakes will then be in the same horizontal line, whether the telescope is level or not.

Now remove the instrument to a point on the same side of both stakes, in a line with them, and from fifty to one hundred feet from the nearest one; again level the instrument, clamp the telescope as nearly horizontal as possible, and note the heights indicated on the staff placed first on the nearest, then on the more distant stake.

If both agree, the telescope is level; if they do not agree, turn with the tangent screw move the wire over nearly the whole error, as shown at the distant stake, and repeat the operation just described till the horizontal wire will indicate the same height at both stakes, when the telescope will be level. Bring the wire into the center by the leveling nuts at the end, taking care not to disturb the position of the telescope, and the adjustment will be completed.

The adjustments above described are always made by the maker of the instrument, but the instrument may need re-adjusting.

241. Uses of the Transit.

1. **The transit** may be used for all the purposes for which the compass is employed, and, in general, with much greater precision.

2. **Horizontal angles** can be taken by the needle, or without reference to the needle, as follows: Level the plate set the limb at zero, direct the telescope so that the intersection of the wires shall pass upon one of the objects selected, clamp the instrument firmly to the spindle, unclamp the vernier plate turn it with the hand till the intersection of the wires is nearly upon the second object, then clamp to the limb, and with the tangent screw fix the intersection of the wires precisely upon the second object. The reading of the vernier will give the angle whose vertex is at the center of the instrument, and whose sides pass through the objects respectively.

3. **Vertical angles** can be measured thus: Level the instrument, fix the zeros of the vertical circle and vernier in a line, note the height cut upon the staff

by the horizontal wire, carry the staff up the elevation or down the depression, fix the wire again upon the same point, and the angle will be read off by the vernier. Sometimes, of course, it will be impossible to carry the staff up the elevation, as in taking the angle of elevation of the top of a steeple from a given point in a horizontal plane.

4. **Horizontal lines** can be run, or the difference of level easily found, by means of the level attached to the telescope.

242. The Solar Compass.

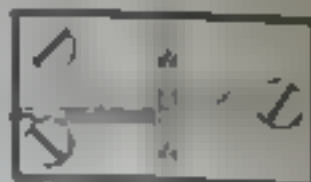
Burt's solar compass, represented in the drawing on page 205, includes the essential parts of the magnetic compass, together with the solar apparatus, which consists mainly of three arcs of circles by which the latitude of the place, the declination of the sun, and the hour of the day can be set off.

The **latitude arc**, *a*, graduated to quarter-degrees and read to minutes by a vernier, has its center of motion in two pivots, one of which is seen at *d*, and is moved by the tangent screw, *f*, up or down a fixed arc of similar curvature through a range of about 35° .

The **declination arc**, *b*, having a range of about 24° , is graduated to quarter-degrees and read to minutes by the vernier *c* fixed to the movable arm, *b*, which has its center of motion in the center of the declination arc at *g*. The vernier may be set to any reading by the tangent screw, *k*, and the arm clamped in any position by a screw concealed in the engraving.

A **solar lens**, set in a rectangular block of brass at each end of the arm, *b*, has its focus at the inside of

the opposite block on the surface of a silver plate on which are drawn certain lines, as shown in the annexed figure. The lines *bb*, called hour lines, and the lines *cc*, called equatorial lines, intersect each other at right angles. The rectangular space between the lines is just sufficient to include the circular image of the sun formed by the solar lens on the opposite end of the arm.



The three other lines below the equatorial lines are five minutes apart, and are used in making allowance for refraction.

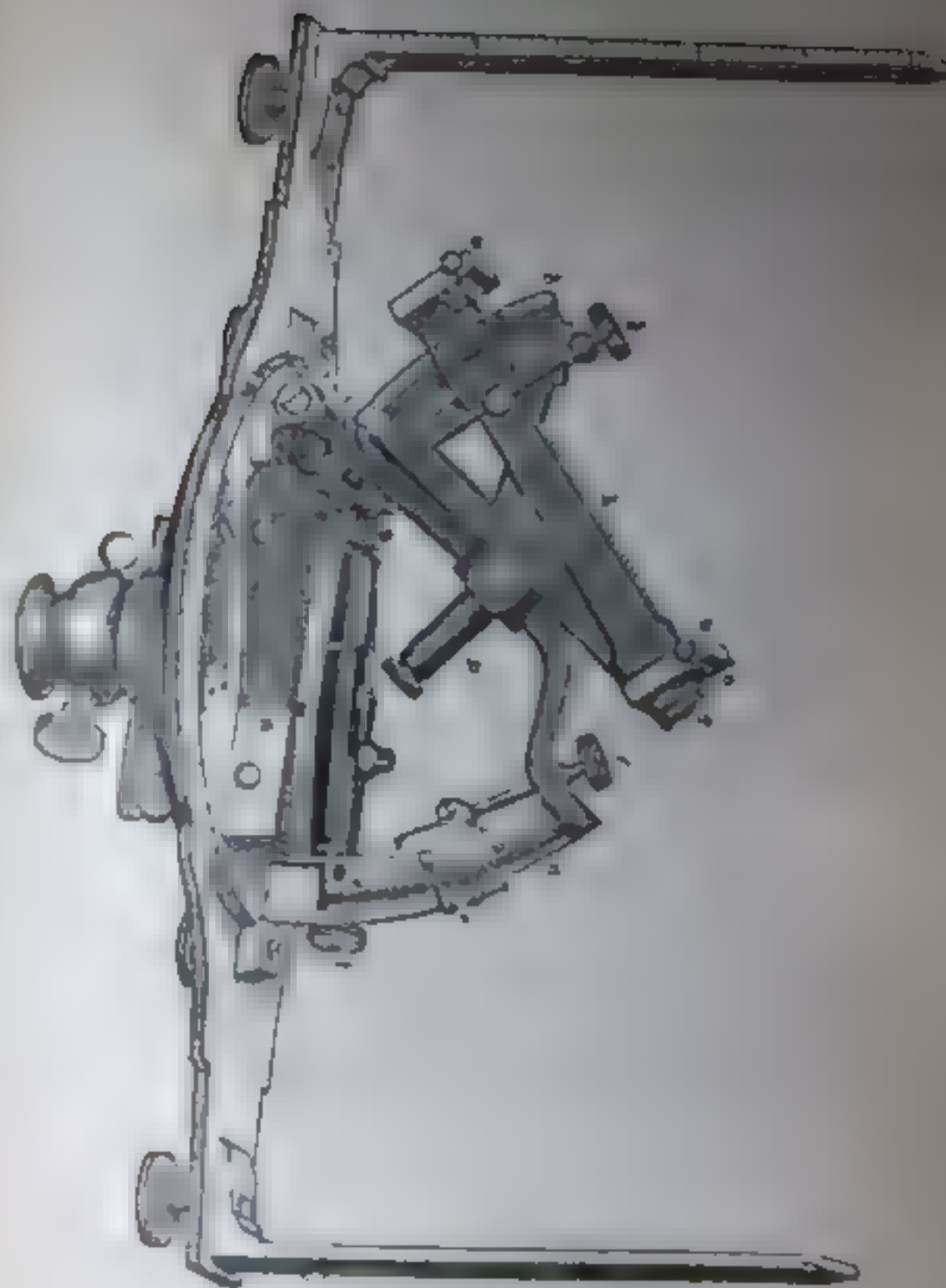
An equatorial sight, used in adjusting the solar apparatus, is placed on the top of each rectangular block by a small milled head screw, so as to be detached at pleasure.

The hour arc, *e*, supported by the pivots of the latitude arc, and connected with that arc by a curved arm, has a range of 120° , graduated to half-degrees and figured in two series, designating both the hours and the degrees; the middle division being marked 12 and 90 on either side of the graduated lines.

The polar axis, *p*, consists of a hollow socket containing the spindle of the declination arc, around which this arc can be moved over the hour arc, which is read by the lower edge of the graduated side of the declination arc. The declination arc may be turned half round, if required, and the hour arc read by a point below *q*.

The needle box, *n*, with an arc of 36° , graduated to half-degrees, and numbered from the center as zero, is attached by a projecting arm to a tangent screw, *t*, by which it is moved about its center, and its needle

THE SOLAR COMPASS.



it to a vane which may be read to minutes by the scale on the end of the arm.

The levels are similar to those of the ordinary compass.

Lines of refraction are drawn on the inside faces of the sights, graduated and figured to indicate the amount allowed for refraction when the sun is near the horizon.

The adjuster is an arm used in adjusting the instrument. It is not attached to the instrument, and is laid aside in the box when the adjustment is effected.

243. Adjustments.

1. The levels are adjusted by bringing the bubbles into the center of the tubes by the leveling screws of the tripod, reversing the instrument on the spindle, raising or lowering the ends of the tubes till the bubbles will remain in the center during a complete revolution.

2. The equatorial lines and solar lenses are adjusted as follows: First detach the arm, *h*, from the declination arc by withdrawing the screws, *a*, in the drawing from the ends of the posts, *b*, the tangent screw, *k*, and also the clamp screw, *a*, the conical pin with its small screws by which the arm and declination arc are connected.

Attach the adjuster in the place of the arm, *h*, by replacing the conical pin and screws, and insert the clamp screw so as to clamp the adjuster at any point on the declination arc.

Now level the instrument, place the arm, *h*, on the adjuster, with the same side resting against the surface of the declination arc as before it was detached,

turn the instrument on its spindle, so as to bring the solar lens to be adjusted in the direction of the sun, raise or lower the adjuster on the declination arc till it can be clamped in such a position as to bring the sun's image, as near as may be, between the equatorial lines on the opposite silver plate, and bring the image precisely into position by the tangent of the latitude arc, or the leveling screws of the tripod. Then carefully turn the arm half-way over, till it rests upon the adjuster by the opposite faces of the rectangular blocks, and again observe the position of the sun's image.

If it remains between the lines as before, the lens and plate are in adjustment; if not, loosen the three screws which confine the plate to the block, and move the plate under their heads till one-half the error in the position of the sun's image is removed.

Again bring the image between the lines, and repeat the operation till it will remain in the same situation in both portions of the arm, when the adjustment will be complete.

To adjust the other lens and plate, reverse the arm, end for end on the adjuster, and proceed as in the former case.

Remove the adjuster, and replace the arm, *h*, with its attachments.

In turning the screws over the silver plate, care must be taken not to move the plate.

3. The vernier of the declination arc is adjusted as follows: Having leveled the instrument, and turned its lens in the direction of the sun, clamp to the spindle, and set the vernier, *v*, of the declination arc at zero, by means of the tangent screw, *k*, and clamp to the arc.

Set the spirit level moves easily and truly in the axis of the instrument, and raise or lower the latitude are by turning the tangent screw, *f*, till the sun's image is brought between the equatorial lines on one of the plates. Clamp the latitude are by the screw, and bring the image precisely into position by the level screws of the tripod or socket, and without disturbing the instrument carefully revolve the arm, *h*, till the opposite lens and plate are brought in the direction of the sun, and note if the sun's image comes between the lines as before.

If the sun's image comes between the lines, there is no index error of the declination arc; if not, then with the tangent screw, *k*, move the arm till the sun's image passes over half the error, and again bring the image between the lines, and repeat the operation as before till the image will occupy the same position on both plates.

We shall now find that the zero marks on the arc and the vernier do not correspond. To remedy this error, the little flat-head screws at the vernier must be loosened till it can be moved, and then make the zeros coincide, when the operation will be complete.

4. The solar apparatus is adjusted to the sights as follows: First level the instrument, then with the clamp and tangent screws set the main plate at 90° by the verniers and horizontal limb. Then remove the clamp screw, and raise the latitude are till the polar axis is by estimation very nearly horizontal, and, if necessary, tighten the screws on the pivots of the arc so as to retain it in this position.

Fix the vernier of the declination arc at zero, and direct the equatorial sights to some distant and well-

marked object, and observe the same through the compass sights. If the same object is seen through both, and the verniers read to 90° on the limb, the adjustment is complete; if not, the correction must be made by moving the sights or changing the position of the verniers.

The adjustments are all made by the maker of the instrument, and, ordinarily, need not concern the surveyor, as the instrument is very little liable to derangement.

244. Use of the Solar Compass.

The declination of the sun, or its angular distance from the celestial equator, must be set off on the declination arc.

The declination of the sun for apparent noon at Greenwich, England, is given from year to year in the Nautical Almanac.

To determine the declination for another place and hour, allowance must be made for the difference of time arising from longitude, and for the change of declination from hour to hour.

The longitude of the place can be determined with sufficient accuracy by reference to that of given prominent places which are situated nearly on the same meridian.

The difference of longitude, divided by 15, will, by changing degrees, minutes, and seconds into hours, minutes, and seconds, give the difference of time, which is usually taken to the nearest hour, as it will be sufficiently accurate.

In practice, surveyors in states just east of the Mississippi allow a difference of 6 hours for longitude;

7 1/2 hours west of the longitude of Santa Fe; 8 hours east of Santa Fe and 6 hours for the eastern part of the United States.

Having found the hour at any place from its longitude, when it is noon at Greenwich, the declination for noon at Greenwich will be the declination for the remaining hour at the given place.

To find the declination for the following hours of the day, add or subtract, for each succeeding hour, the difference of declination for 1 hour, as given in the almanac.

Thus, let it be required to find the declination of the sun for the different hours of May 20th, 1873. W. lon. 95° . $95^{\circ} = 6$ h. 20 m., practically 6 h.

Sun's dec., Greenwich, noon	$= 20^{\circ} 3' 11'' 6$
\therefore Sun's dec., lon. 95° , 6 A. M.	$= 20^{\circ} 3' 11'' 6$
Add difference for 1 h.	$11'' 03$
Sun's dec. 7 A. M.	$= 20^{\circ} 3' 22'' 63$
Add difference for 1 h.	$11'' 03$
Sun's dec. 8 A. M.	$= 20^{\circ} 3' 33'' 66$

In like manner proceed for the remaining hours.

Such a calculation should be made to begin the work of the day.

Refraction, or the bending of the sun's rays as they pass obliquely through the atmosphere, affects its declination by increasing its apparent altitude.

The amount of refraction depends upon the altitude, being less as the altitude is greater. At the horizon the refraction is $35'$; at the altitude of 45° , $1'$; at the zenith, 0.

Meridional refraction, by increasing the apparent altitude of the sun, when on the meridian, increases or

diminishes its apparent declination according as it is north or south of the equator.

To find the amount of meridional refraction, we must first find the meridional altitude of the sun for the given latitude, which is equal to the complement of the latitude, plus or minus the declination, according as the sun is north or south of the equator.

The meridional altitude of the sun being given, the tables will give the refraction.

The meridional refraction, being quite small, may be disregarded in practice except when great accuracy is required, as in running great standard meridians or base lines.

Incidental refraction, as affected by the hour of the day and the state of the atmosphere, can not, in practice, be determined by a precise calculation.

It will about compensate for incidental refraction to keep the image of the sun square between the equinoctial lines for the middle of the day, but toward morning or evening, to run the image, which is then hazy round the edge, so that the hazy edge shall overlap one or two lines of the spaces below.

To set off the latitude, find the declination of the sun for the given day at noon, and set it off on the declination arc, and clamp the arm firmly to the arc.

Find in the almanac the equation of time for the given day, in order to ascertain the time when the sun will reach the meridian.

About twenty minutes before noon, set up the instrument, level it carefully, fix the divided surface of the declination arc at 12 on the hour circle, and turn the instrument on its spindle till the solar lens is brought into the direction of the sun.

When the clamp screw of the latitude arc, raised by the tangent screw, is brought precisely between the equatorial lines, and turn the instrument so as to keep the image between the hour lines on the plate.

As the sun ascends, in approaching the meridian, the image will move below the lines, and the arc must be moved to follow it. Keep the image between the two sets of lines till it begins to pass above the equatorial, which is the moment after it passes the meridian.

Read off the vernier of the arc, and we have the latitude of the place which is to be set off on the latitude arc.

To run lines with the solar compass. Having adjusted the instrument and set off the declination and latitude, the surveyor places the instrument over the station, levels it carefully, clamps the plates at zero on the horizontal limb, and directs the sights north and south, approximately, by the needle.

The solar lens is then turned toward the sun, and with one hand on the instrument, and the other on the revolving arm, both are moved from side to side till the image of the sun is made to appear on the silver plate, and is brought precisely within the equatorial lines, when the line of sights will indicate the true meridian.

In running an east and west line, the verniers of the horizontal limb are set at 90° , and the sun's image kept between the equatorial lines.

The needle is made to indicate zero on the arc of the compass box by turning the tangent screw. Lines can then be run by the needle in the temporary disappearance of the sun.

The variation of the needle, which should be noted at every station, is read off to minutes on the arc along the edge of which the vernier of the needle box moves.

Since the limb must be clamped at 0 when the sun's image is in position, in order that the sights may indicate the meridian, it is evident that the bearing of any line may be found by the solar compass, as well as by the compass or transit.

In running long lines, allowance must be made for the curvature of the earth. Thus, in running north or south the latitude changes $1'$ for 92.30 ch., and six miles, or one side of a township, requires a change of $5' 12''$ on the latitude arc.

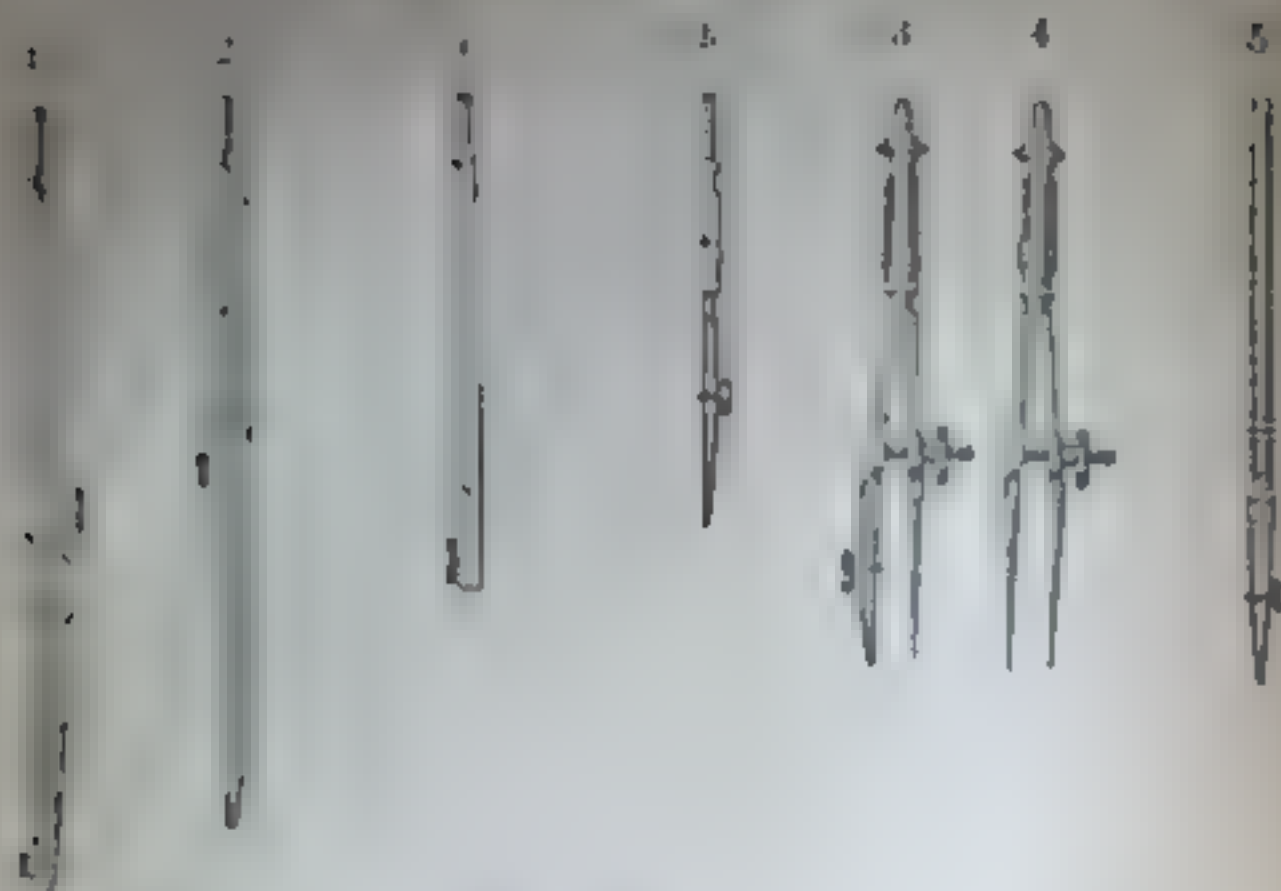
In running east and west lines, the sights are set at 90° on the limb, and the line run at right angles to the meridian; but this line, if sufficiently produced, would cross the equator. Hence, at the next station, a backsight is taken, and one-half the error is set off for the next foresight on the side toward the pole.

The most favorable season for using the solar compass is the summer; and the most favorable time of day, between 8 and 11 A. M., and 1 and 5 P. M.

A solar telescope compass is sometimes used; and, in this case, the telescope is placed at one side of the center. All error from this position of the telescope is avoided by an offset from the flag-staff.

The solar compass, while indispensable in the survey of public lands, can be used, in common practice, with considerable advantage over ordinary needle instruments, since lines can be run by it without regard to the variation of the needle or local attraction, and the bearings being taken from the true meridian will remain constant for all time.

245. Dividers and Pens.



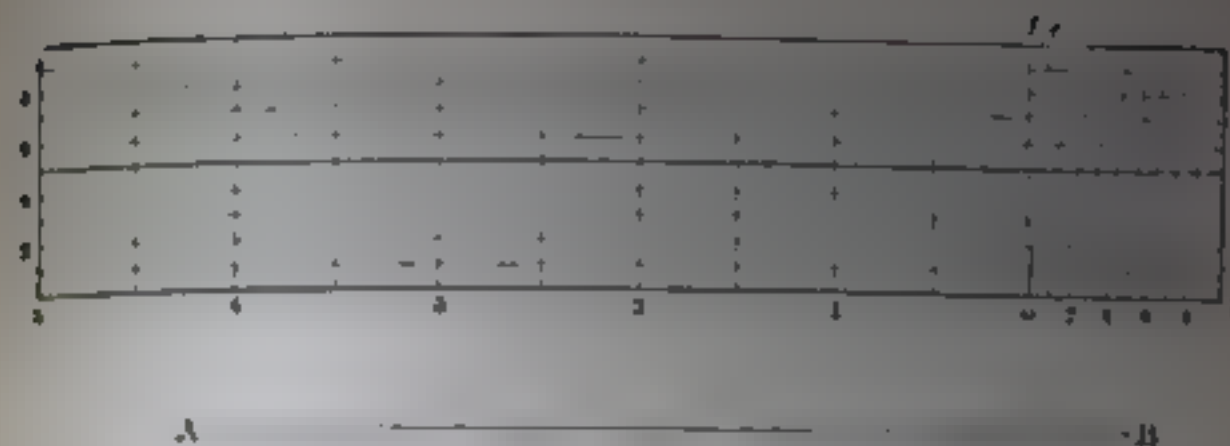
1. Dividers with lead-pencil.
2. Hair dividers with one leg movable by screw.
- a, b. Lengthening bar and pen which may be inserted together or the pen alone instead of pencil.
3. Bow pen with spring and adjustable screw.
4. Spacing dividers.
5. Drawing pen.

246. Parallel Rulers.



1. Parallel ruler for drawing parallel lines.
2. Sliding parallel ruler with scales.

247. Diagonal Scale.



Let de be .1, then the distance from ad to ac on the first line above ab is .01, on the second line .02, etc.

Let it be required to lay off on AB 4.63.

Place one foot of the dividers at the intersection of the diagonal line, 6, and the horizontal line, 3. Extend the other foot till the horizontal line, 3, intersects the vertical line, 4, then will the distance from one point of the dividers to the other be 4.63.

Now place one foot of the dividers at A , and the other at B , then AB will be 4.63.

248. Protractors.



These protractors are used in laying off or measuring angles. The vertex of the angle is at the center, and one side is made to coincide with the horizontal line passing through the center; then, counting the degrees from the horizontal line round the circumference till the required degree is reached, and drawing

... to the center, we shall have ...

... these instruments will give angles to ... and the second, by means of a ver ...

... may be multiplied indefinitely, but the ... of using them will be readily discovered by ... operator.

SURVEY OF PUBLIC LANDS.

249. Division into Townships.

In the rectangular system of surveying the public lands, adopted by the government, two principal lines—an east and west line, called a *base line*, and a north and south line, called a *principal meridian*—are established before the survey of the town-

Six miles to the north of the base line another east and west line is run, and six miles to the north of this another, and so on.

Every fifth parallel from the base is called a *standard parallel*, or *correction line*.

Six miles to the west of the principal meridian, measured on the base line, another north and south line is run to the first standard parallel, and six miles to the west of this another, and so on.

The intersection of the east and west with the north and south lines divides the tract into *townships*, which would be exactly six miles square were it not for the convergence of the meridians.

To preserve as nearly as possible the form and size of the townships, the standard parallels before men-

tioned are established, which serve as base lines for the townships north up to the next standard parallel.

Tiers of townships north and south are called *ranges*, and are numbered east or west, as the case may be, from the principal meridian.

Lines running north and south, bounding the townships on the east and west, are called *range lines*.

Lines running east and west, bounding the townships on the north and south, are called *township lines*.

A township marked thus, *T. 5 N., R. 4 W.*, read township five north, range four west, would be in the fifth tier north of the base line, and in the fourth tier west of the principal meridian.

Townships are divided into *sections*, or *square miles*, containing 360 acres; each section into four *quarter sections*, each quarter section into two *half-quarter sections*, and each half-quarter section into two *quarter-quarter sections*. These are called legal subdivisions, and are the only divisions recognized by the government, except pieces made fractional by water-courses or other natural agencies.

On base lines and standard parallels two sets of corners are established.

1. **Standard corners**, established when these lines are run, embracing township, section, and quarter-section corners, common to two townships, sections, or quarter sections north of the base line or standard parallels.

2. **Closing corners**, established when exterior and subdivision lines close on them from the south, embracing township and section corners, common to two townships or sections south of the standard parallels.

In consequence of the convergence of the meridians, the north and south lines, produced to the standard

be set close on the standard corners provided the course will strike the standard parallels east or west of the standard corners, making the corner east or west of the standard corner, according as the direction of operation is west or east of the principal meridian.

The following diagram will illustrate the subject.

AB is the base line.

AC, the principal meridian.

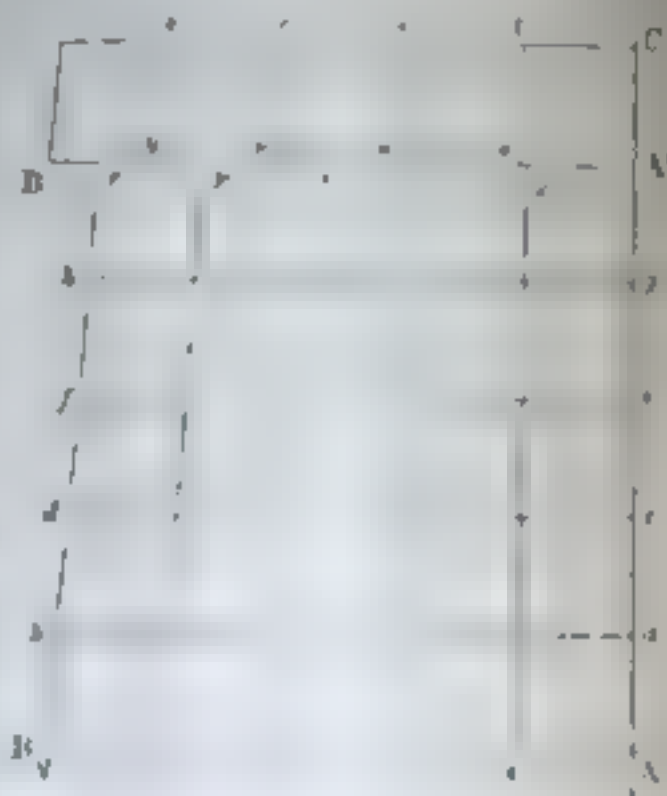
AB', a standard parallel.

ad, *ad'*, etc., township lines.

ij, *kl*, etc., range lines.

a, *u*, *w*, etc., standard corners.

j, *l*, *z*, etc., closing corners.



The distances *ja*, *lu*, etc., are measured and recorded in the field book.

The details of running lines will be given after describing the methods of perpetuating corners, the process of chaining, and the method of marking lines.

Burt's improved solar compass is used in surveying standard and township lines, but the ordinary compass may be used in subdividing.

250. Methods of Perpetuating Corners.

1. Corner trees.—A sound tree, five inches or more in diameter, standing exactly at a corner, is the best monument.

2. Corner stones.—A stone, at least 14 inches long and 6 inches square, set from two-thirds to three-fourths in the ground, is preferred to other monuments, except a tree.

3. Posts and witness trees.—In the absence of corner trees and stones, when trees are near, a post may be planted and witnessed by taking the bearing and distance of two or more trees in different directions from the corner. These trees are marked by a blaze in which is marked the number of the township, range, and section. A notch is cut in the lower end of the blaze, under which another blaze is made in which are cut the letters *B. T.*, signifying bearing tree.

4. Posts, mounds, and witness pits. When neither corner trees, stones, nor witness trees are available, corners may be marked by posts, mounds, and witness pits. The posts are planted 12 inches in the ground, and at the lower end, on the north or west side, according as the course is north or west, a marked stone, a small quantity of charcoal, or a charred stake must be deposited. Four pits are dug, 6 feet from the post, on opposite sides, 2 feet square and 1 foot deep, and the excavated earth packed round the post within 1 foot of the top. If sod is to be had, it is to be used in covering the mounds.

The method of marking the corner is to be carefully noted in the field book.

251. Township Corners.

1. Posts used in marking township corners must be 4 feet in length, and 5 inches, at least, in diameter. These posts are to be set 2 feet in the ground, and

the corner post is, and to receive the marks to be set on the lines.

If the corner is common to two townships, the post is set so as to present the face in the direction of the line; and the number of the township range, and section must be marked on the side facing, and six notches cut on each of the four edges.

If the township corner is on a base line or standard parallel, unless it is also on the principal meridian, it will be common to two townships only; and if these are on the north, the corner will be a standard corner. In this case, six notches are cut on the east, north, and west edges, but not on the south edge, and the letters S. C., signifying standard corner, are cut on the flat surface.

If the corner is common to two townships on the south, but not on the north, it will be a closing corner, and six notches are cut on the east, south, and west edges, but not on the north edge, and the letters C. C., signifying closing corner, are cut on the flat surface.

2. Township corner stones should be inserted at least 10 inches in the ground, with their sides facing the cardinal points of the compass, and small mounds of stones heaped against them.

These corner stones are notched in the same manner as posts in similar circumstances, but are not otherwise marked.

3. A tree of proper size on the corner is marked in the same manner as a post.

The mounds, when made round the posts, must be 5 feet in diameter at the base, and $2\frac{1}{2}$ feet high. The posts, therefore, must be $4\frac{1}{2}$ feet long, so as to be 1 foot in the ground and 1 foot above the top of the mound.

Witness pits for township corners must be 2 feet long, $1\frac{1}{2}$ feet wide, and 1 foot deep. If the corner is common to four townships, there will be four pits placed lengthwise on the lines; but if the corner is common to only two townships, only three pits are dug, and are placed lengthwise on the lines. Thus the kind of township corners are readily distinguished.

These pits are made only in the absence of witness trees, which are to be selected, if possible, one from each township.

252. Section Corners.

Section corners are established at intervals of 80 chains or 1 mile, and are perpetuated by the following methods:

1. Section corner posts are 4 feet in length, and at least 4 inches in diameter. They are planted 2 feet in the ground, and the part above the ground squared to receive the marks.

If the corner is common to four sections, the post is set cornerwise to the lines, the number of the section is marked on the side facing it, and the number of the township and range on the north-east face.

Mile-posts on township lines have as many notches on the corresponding edges as they are miles from the respective township corners.

Section posts within a township have as many notches on their south and east edges as they are miles from the south and east boundaries of the township. The notches are cut on the north and west edges.

Section posts must be witnessed by trees, one in each section, or, in the absence of trees, by pits 18 inches square and 12 inches deep.

2. **Section corner mounds** are 4½ feet in diameter at the base, and 3 feet high. The post must be 4 feet long, 1 foot in the ground, and 1 foot high above the mound, and at least 3 inches square.

At corners common to four sections, the edges are in the direction of the cardinal points; but at corners common only to two sections, the flattened sides face the cardinal points.

Section posts in mounds are to be marked and witnessed in the same manner as the post without the mound.

3. **Stones** used to mark section corners on township lines are set with their edges in the direction of the line; but for interior sections they face the north. They are witnessed in the same manner as posts, but are not marked except by notches.

4. **Section corner trees** are marked and witnessed the same as posts.

253. Quarter Section Corners.

Quarter section corners are established at intervals of 40 chains or half a mile, except in the north or west tiers of sections of a township.

In subdividing these sections, the quarter post is placed 40 chains from the interior section corner, so

that the excess or deficiency shall fall in the last half mile.

Quarter section corners are not required to be established on base or standard parallel lines on the north.

The methods of perpetuating these corners are the following:

1. **Quarter section posts**, 4 feet in length and 4 inches in diameter, are planted or driven 2 feet into the ground, and the part above the ground squared and marked $\frac{1}{4}$ S., signifying quarter section. These corners are witnessed by two bearing trees.

2. **Quarter section mounds** are, like section mounds, packed round the posts, and pits may be used in the absence of witness trees.

3. **Quarter section stones** have $\frac{1}{4}$ cut on the west side of north and south lines, and on the north side of east and west lines, and are witnessed by two bearing trees or pits.

4. **A quarter section tree** is marked and witnessed in the same manner as a post.

254. Meander Corners.

Meander corners are the intersections of township or section lines with the banks of lakes, bayous, or navigable rivers.

These corners are marked by the following methods:

1. **Meander posts** of the same size as section posts, are planted firmly in the ground, and witnessed by two bearing trees or pits, but are not marked.

2. **Mounds** of the same size as those for section corners are, in the absence of witness trees, formed round

the posts, and a pit dug exactly on the line, 8 links farther from the water than the mound.

Stones or trees, witnessed in the same manner as posts, may be employed.

255. Chaining.

Eleven tally pins are employed, ten of which are taken by the fore chainman, or leader, and the remaining one by the hind chainman, or follower, who sticks it at the beginning of the course, and against it brings the handle at one end of the chain.

The leader, holding the other handle of the chain and one pin in his right hand, draws out the chain to its full length in the direction of the course; both taking care that the chain is free from kinks.

The leader standing to the left of the line, so as not to obstruct the range, with his right arm extended, draws the chain tight, brings the pin into line according to the order "right" or "left," from the follower, sticks it at the order "down" by pressing his left hand on the top of the pin, and replies "down."

The follower then withdraws his pin, and both advance, the leader drawing the chain in the direction of the course, but a little to one side to avoid dragging out the pin, till the follower comes up to the pin, against which he brings the handle at his end of the chain, and directs the sticking of another pin, as before, and so on.

When the leader has stuck his last pin, he cries "tally," which is repeated by the other, and each registers the tally by slipping a ring on a belt.

The follower then comes forward, and counting in presence of his fellow, to avoid mistake, the pins taken

up, takes the forward end of the chain and proceeds, as the leader, for another tally.

If a whole chain is employed, a tally is ten chains; and accordingly four tallies make half a mile, and eight tallies a mile.

If a half-chain is employed, a tally is five chains, eight tallies are half a mile, and sixteen tallies a mile.

In measuring up or down a hill, the chain must be kept horizontal, so that it is often necessary to use but a portion of the chain.

The chain employed in the field must be compared, from day to day, with a *standard chain* furnished by the Surveyor-General, and any variation promptly corrected.

256. Marking Lines.

Line trees, called also "station trees," or "sight trees," are marked by two notches on each side of the tree, in the direction of the line.

The line is marked, so as to be easily followed, by blazing a sufficient number of trees near the line on two sides quartering toward the line.

Saplings near the line are cut partly off by a blow from the ax at the usual height of blazes, and bent at right angles to the line.

Random lines are not marked by blazing trees, but to enable the surveyor to retrace the line on his return, bushes are lopped and bent in the direction of the line, and stakes are driven every ten chains, which are pulled up when the true line is established.

Insurmountable objects, such as ponds, marshes, etc., are passed by making right-angled offsets, or by trigonometrical

metrical operations, a complete record of which must be made in the field book.

257. Initial Point and Principal Lines.

1. The initial point, which is usually some permanent natural object, as the confluence of two rivers, or an isolated mountain, is first selected.

2. Principal meridians are run from the initial points due north or due south, and the quarter section, section, and township corners on these lines are accurately located and perpetuated.

The following are the principal meridians already established:

1st. The first runs north from the mouth of the Great Miami river, between Ohio and Indiana, to the south line of Michigan.

2d. The second runs north from the mouth of the Little Blue river through the center of Indiana to its north line.

3d. The third runs north from the mouth of the Ohio river through Illinois to its north line.

4th. The fourth runs north from the Illinois river through the western part of Illinois and the center of Wisconsin to Lake Superior.

5th. The fifth runs north from the mouth of the Arkansas river through the eastern portion of Arkansas, Missouri, and Iowa, and regulates the surveys in Minnesota west of the Mississippi river, and the surveys in Dakota east of the Missouri river.

6th. The sixth commences on the Arkansas river, in Kansas, and runs north through the eastern part of Kansas and Nebraska to the Missouri river.

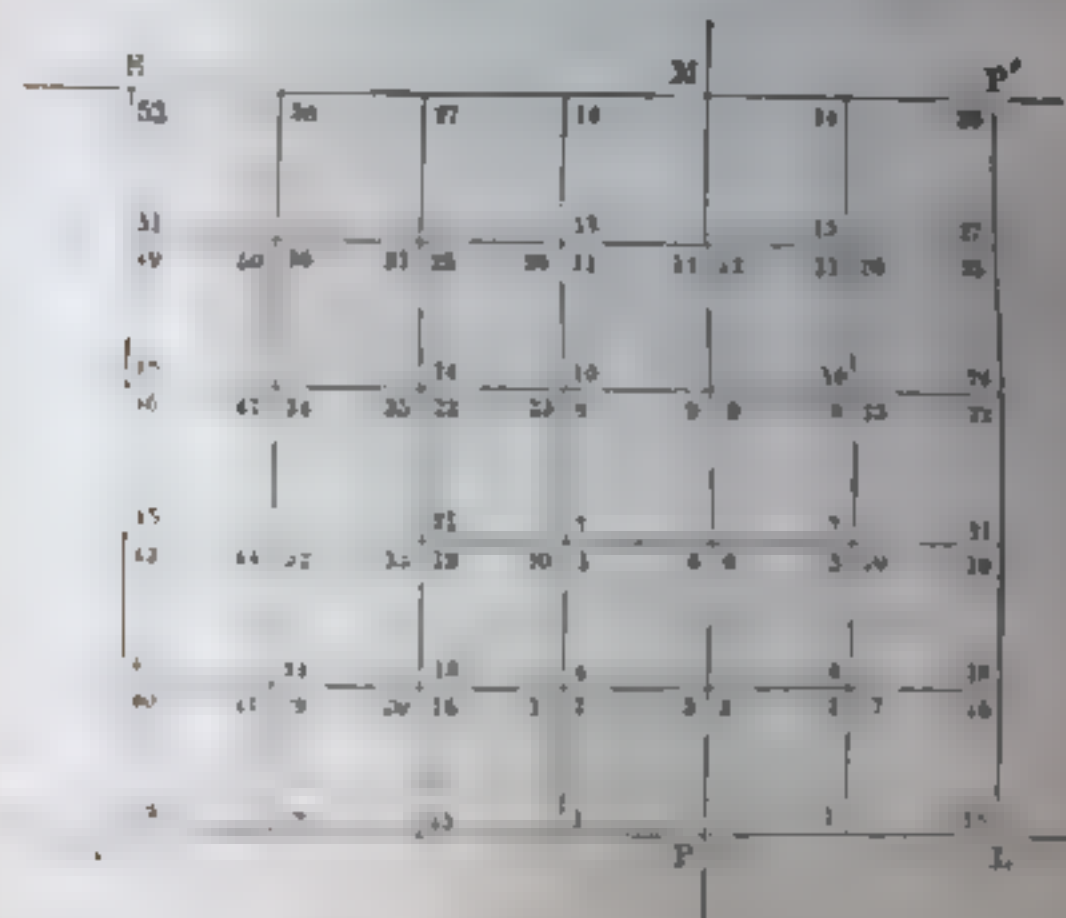
7th. *Independent meridians*—These are the *Independent* meridian of New Mexico, the *Salt Lake* meridian in Utah, the *Willamette* meridian of Oregon and Washington, and the *Humboldt* meridian, the *Mt. Diablo* meridian, and the *St. Bernardino* meridian of California.

3. **Base lines** are run from the initial points due east or due west, and the quarter section, section, and township corners, for the land north of the line, are accurately located, at full measure, and perpetuated.

4. **Standard parallels** are also run due east or due west thirty miles north of the base line or other standard parallel, and the corners located and perpetuated as on the base line.

5. **Range lines** are run between the ranges of townships due north from a base line or standard parallel to the next standard parallel.

258. Exterior or Township Lines.



In the above diagram let *P* denote the initial point, *PM* the principal meridian, *BL* the base line, *SP'* the

first standard parallel north, and let the squares denote **townships**.

1. For townships west of the meridian, begin at the first pre-established township corner on the base line west of the meridian. This is the S. W. corner of T. 1 N., R. 1 W., and is marked 1 in the diagram.

Measure thence due north 480 chains, establishing the quarter section and section corners, to 2, at which point establish the corner common to T.'s 1 and 2 N. and R.'s 1 and 2 W.; thence east on a random line, setting temporary quarter section and section stakes to 3.

If the random line should overrun, or fall short, or intersect the meridian north or south of the true corner, more than 3.50 chains, a material error has been committed, and the lines must be retraced.

If the random line should terminate within 3.50 chains of the corner, measure the distance at which the meridian is intersected north or south of the corner, calculate a course which will run a true line back from the corner to the point from which the random line started, measure westward to 4, which is the same point as 2, establish the permanent corners, obliterate the temporary corners on the random line, and throw the excess or defect, if any, on the west end of the line.

In like manner, measure from 4 to 5, from 5 to 6, from 6 to 7, and so on to 14, on the standard parallel, throwing the excess or deficiency on the last half mile. At the intersection with the standard parallel, establish the township closing corner, measuring and recording the distance to the nearest standard corner on said standard parallel.

If from any cause the standard parallel has not been run, the surveyor will plant the corner of the

township in place, subject to removal north or south when the standard parallel shall have been run.

The surveyor then proceeds to the S. W. corner of T. 1 N., R. 2 W., on the base line at 15, and proceeds in a similar manner with another range of townships, and so on.

2. For townships east of the meridian, begin at the S. E. corner of T. 1 N., R. 1 E., at 1 on the base line, and proceed as on the west of the meridian, except that the random lines are run west and the true lines east, throwing the excess over 480 chains, or the deficiency, on the west end of the line in measuring the first quarter section boundary on the north, the remaining distances will be exact half-miles and miles.

With the field notes of the exterior or township lines, a plot of the lines, run on a scale of 2 inches to the mile, must be submitted, on which are noted all objects of topography, which will illustrate the notes, as the direction of streams, by arrow-heads pointing down stream, the intersection of the lines by lines, streams, ponds, marshes, swamps, ravines, mountains, etc.

259. Subdivision or Section Lines.

The deputy employed to run the exterior lines of a township is not allowed to subdivide it, but another is employed to do this work, that the one may be a check to the other, thus securing greater accuracy.

Before subdividing a township, the surveyor must ascertain and note the change in the variation of the needle which has taken place since the township lines were run, and adjust his compass to a variation which will retrace the eastern boundary of the township.

He must also compare his own chaining with the correct by measuring the first mile both of the south and east lines of the township, and note the discrepancy, if any.

The following is a diagram of a township:

6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

The sections are designated by beginning at the N. E. corner and numbering west, 1, 2, ..., 6, then east on the next tier, 7, 8, ..., then west, and so on.

In running the subdivision lines, begin on the south line of the township, at the first section corner west of the east line, numbered 1 in the diagram, and common to sections 35 and 36.

Measure thence due north 40 chains, at which point establish a quarter section corner; thence due north another 40 chains to 2, where establish a section corner common to sections 5, 26, 35, and 36.

Run a random line from 2 due east to the township line, setting up a temporary quarter section stake 40 chains from 2.

If the random line intersect the township line precisely at the pre-established section corner at 3, it may be established as the true line by blazing back and making the quarter section corner permanent.

If the random line intersect the township line either north or south of the section corner, measure and note the distance of the intersection from said corner, and calculate a course which will run a true line from the corner back to 4, where the random line started.

Let A correspond to section corner 2, B to 3, and C to the intersection of the township and random lines, and north, for example, of B the section corner.

$$\text{Then, } \tan A = \frac{BC}{AB}.$$

Let l = the number of links in BC , and m the number of minutes in A . Then, practically, we shall have,

$$\text{If } AB = \frac{1}{2} \text{ mile, } m = l - \frac{1}{4}l.$$

$$\text{If } AB = 1 \text{ mile, } m = \frac{3}{2}l - \frac{1}{4}l.$$

$$\text{If } AB = 3 \text{ miles, } m = \frac{5}{2}l.$$

$$\text{If } AB = 6 \text{ miles, } m = \frac{7}{2} \text{ of } \frac{3}{2}l.$$

Let us suppose that we have found $A = 10^\circ$

Now, as CA is west by the compass, BA is N. 80° $40' 11''$ W. Run this line and establish the quarter section at a point equidistant from the two section corners, which will be, with sufficient accuracy, one-half the length of the random line from 2. Pull up the temporary quarter section stake on the random line

Proceed from 4 to 5, then on a random line to 6, and back on a true line to 7, and so on to 16.

From 16 run due north on a random line to the north line of the township, setting up a temporary quarter section stake at 40 chains.

If the random line intersect the north line of the township at the pre-established section corner, the random line will be the true line, and is made permanent by blazing back, and making the quarter section corner permanent.

If the random line does not close exactly on the pre-established section corner, measure and note the distance of the intersection from said corner, calculate a course that will run a true line southward from the corner to 16, run this line, and establish the quarter section corner on it just 40 chains from 16, throwing the excess or deficiency, if any, on the last half mile.

If the north township line is a base line or standard parallel, no random line is run, but a true line due north, on which a quarter section post is established 40 chains from 16; and at the intersection with said base line or standard parallel, establish a closing corner, measuring and noting its distance from the corresponding standard corner.

Pass from 17 to 18, and survey the second tier of sections in the same manner as the first, closing on the interior section corners before established as upon those on the east line of the township.

In running the line between the fifth and sixth tiers of sections, not only is a random line run east as before, but one is run west to the range line, and a true line run back, and the permanent quarter section corner established on it just 40 chains from the in-

terior corner, throwing the excess or deficiency on the west half mile.

The Surveyor-General furnishes the outline of the diagram, and the deputy fills it out, and makes the appropriate topographical sketches.

260. Meandering.

Navigable rivers, lakes, and bayous, being public highways, are meandered and separated from the adjoining land.

Standing with the face down stream, the bank on the right hand is called the *right bank*; the bank on the left, the *left bank*.

If a river is navigable, both banks are meandered, care being taken not to mistake, in high water, the border of bottom-land for the true bank.

Commence at a meander corner of the township line, take the bearing along the bank of the river, and measure the distance of the longest possible straight course to the nearest chain, if the distance exceeds 10 chains; otherwise, to the nearest ten links; and so on to the next meander corner on another boundary line of the township.

Enter in the field book, after the township notes, keeping the notes separate through each fractional section, the date, the point of beginning, the bearings and distances in order, the intersections with all intermediate meander corners, the height of falls, the length of rapids, the location and width at the mouth of streams running into the water you are meandering, the location of springs on the banks, the nature of their waters, the location of islands, the elevation of banks, etc.

If the river is not navigable, meander the right bank, unless it presents formidable obstacles not found on the left bank, but the crossing of the stream, in making a bridge, must be made from a pre-established meander corner on one bank to the corner on the other bank, and the width of the river between the corners computed trigonometrically.

Wide flats, whose area is more than 40 acres, permanently covered with water, along rivers not navigable, are meandered on both banks.

The position of islands in rivers is determined by measuring, on or near the bank, a base line, connected with the surveyed lines, and taking the proper bearings to a flag or other object on the island, and computing the distance from the meander corners of the river to points on the bank of the island. The island can be meandered from such points.

In meandering lakes, ponds, or bayous, commence at a meander corner of the township line, and proceed as in case of a river. If, however, the body of water is entirely within a township, begin at a meander corner established in subdividing.

In meandering a pond lying entirely within the boundaries of a section, run to the pond two lines from the nearest section or quarter section corners, on opposite sides of the pond, giving their bearings and distances, and at the intersection of these lines with the bank of the pond establish witness points by planting posts, witnessed by bearing trees or mounds and pits, then commence to meander at one of these points, and proceed around to the other, and thence to the point of beginning.

No blazes or marks are made on meander lines between established corners.

261. Swamp Lands.

By the act of Congress approved Sept. 28th, 1850, swamp and overflowed lands, unfit for cultivation, are granted to the state in which they are situated.

If the larger part of the smallest legal subdivision is swamp, it goes to the state; if not, it is retained by the Government.

In order to determine what lands fall to the state under the swamp act, it is required that the field notes, beside other things required to be noted, should indicate the points where the public lines enter and leave all such land.

The aforesaid grant does not embrace lands subject to casual inundation, but those only where the overflow would prevent the raising of crops without artificial aid, such as levees, etc. The surveyor should therefore state whether such lands are continually and permanently wet, or subject to overflow so frequently as to render them totally unfit for cultivation.

The depth of inundation is to be stated, as determined from indications on the trees, and the frequency of inundation should be given as accurately as possible, from the nature of the case or reliable testimony.

The character of the timber, shrubs, plants, etc., growing on such lands, and on the land near rivers, lakes, or other bodies of water, should be stated.

The words "unfit for cultivation" should be employed, in connection with the usual phraseology, in the notes, on entering or leaving such lands.

If the margin of bottoms, swamps, or marshes in which such uncultivable land exists, is not identical with the body of land unfit for cultivation, a separate entry must be made opposite the marginal distance.

In case the land is overflowed by artificial means, such as dams for milling, logging, etc., such overflow will not be officially regarded, but the lines of the public surveys will be continued across the same without setting meander posts, stating particularly in the notes the depth of the water, and how the overflow was caused.

262. Field Books.

The field books are the original and official records of the location and boundaries of the public lands, and afford the elements from which the plots are constructed.

They should, therefore, contain an accurate record of every thing officially done by the surveyor, pursuant to instructions in running, measuring, and marking lines, and establishing corners, and should present a full topographical description of the tract surveyed.

There are four distinct field books:

1. A field book for the *meridian and base lines*, exhibiting the establishment of the township, section, and quarter section corners on these lines, the crossing of streams, ravines, lakes, and mountains, the character of the soil, timber, minerals, etc.
2. A field book for *standard parallels or section lines*, showing the township, section, and quarter section corners on the lines, and the topography of the country through which the lines pass.
3. A field book for *city or township lines*, showing the establishment of corners on the lines, and the topography.
4. A field book for *subdivision or section lines*, giving the corners and topography as aforesaid.

The variations of the needle must be stated in a separate line, preceding the notes of measurement, which must be recorded in the order in which the work is done, and the date must immediately follow the notes of each day's work.

The exhibition of every mile surveyed must be complete in itself, and be separated from the preceding and following notes by a line drawn across the paper.

The topographical description must follow the notes for each mile, and not be mixed up with them.

No abbreviations are allowed, except for words constantly occurring, as *sec.* for section, *ch.* for chains, *ft.* for feet, $\frac{1}{4}$ *sec. cor.* for quarter section corner.

Proper names are never to be abbreviated.

The field books must be so kept as to show the amount of work done in each fiscal year.

The notes should be expressed in clear and precise language, and the writing legible.

No record is to be obliterated, or leaf mutilated or taken out.

The title-page of each book should designate the kind of lines run, giving prominently the name of the state or territory and surveyor, the dates of contract, and of commencing and completing the work.

The second page should contain the names and duties of assistants; and whenever a new assistant is employed, or the duties of any of them changed, such facts, with the reason, should be stated in an appropriate entry, immediately preceding the notes taken under such changed arrangements.

An index, in the form of a diagram or plot of the survey, with number on each line, referring to the page of the field notes on which is found the description of the line, must accompany the notes.

263. Records in the Field Book.

1 **General heading of the pages.** The number of the township and range, and the name of the principal meridian of reference, stand at the head of each page.

2 **Heading for each mile.**—The bearing, location, and kind of line run, whether random or true, must be stated in a line; and the variation of the needle, in a separate line on the page at the head of the notes, for each mile run.

3 **Courses and distances.**—The course and length of each line run, noting all necessary offsets therefrom, with the reason and mode thereof.

4 **The method of perpetuating corners.** If a tree, note the kind and diameter; if a stone, its dimensions, as factors in the order of length, breadth, and thickness; if a post, its dimensions, the kind of timber, the kind of memorial, if any, buried by its side, and if surrounded by a mound, the material of which the mound is constructed, whether of stones or earth. The course and distance of the pits from the center of the mound where a necessity exists for deviation from the general rule of witness trees.

5 **Bearing trees.**—The kind and diameter of all bearing trees, with the course and distance of the same from their respective corners, and the precise relative position of the witness corners with respect to the true corners.

6 **Line trees.**—The kind, diameter, and distance on the line, from the corner, of all trees which the line intersects.

7 **Intersection of land objects.**—The distance at which the line first intersects and then leaves every settler's claim and improvement, prairie, bottom land, swamp,

marsh, grove, or windfall, with the course of the same at both points of intersection; the distance at which a line begins to ascend, arrives at the top, or reaches the foot of all remarkable hills and ridges, with their courses and estimated height above the surrounding country.

8 **Intersection of water objects.** The distance at which the line intersects rivers, creeks, or other bodies of water, the width of navigable streams, and small lakes or ponds between the meander corners, the height of banks, the depth and nature of the water.

9 **Surface.**—Level, rolling, broken, or hilly.

10 **Soil.**—First, second, or third-rate; clay, sand, loam, or gravel.

11 **Timber.**—Kind, in order of abundance, and undergrowth.

12 **Bottom-lands.**—Wet or dry; whether subject to inundation, and to what depth.

13 **Springs.**—Fresh, saline, or mineral; and course of their streams.

14 **Improvements.**—Towns and villages, Indian villages and wigwams, houses and cabins, fields, fences, sugar groves, mill-seats, forges or factories.

15 **Coal beds.**—Note the quality of coal beds, and their extent to the nearest legal subdivision.

16 **Roads and trails.**—Whence, whither, and direction.

17 **Rapids, cascades.**—Length of rapids, height of falls in feet.

18 **Precipices.**—Describe precipices, caves, ravines, sink-holes.

19 **Quarries.**—Whether marble, granite, limestone or sand-stone.

20. **Natural curiosities.**—Interesting fossils, ancient works, ruins, roads, fortifications, embankments, etc.

21. **Change of variation.**—Any material change in the variation of the needle must be noted, and the exact points where such variation occurs.

22. **Dates.**—State the date of each day's work in a separate line, immediately after the notes for that day.

23. **General description.**—At the conclusion of the notes for the subdivisational work, taken on the line, the deputy must subjoin a general description of the township in the aggregate, in reference to the face of the country, its soil, timber, geological features, etc.

24. **Verification of Deputy Surveyor.**—The deputy must append to each separate book of field notes his affidavit that all the lines therein described have been run, and all the corners established and perpetuated according to the instructions and laws, and that the foregoing notes are the true and original field notes of such survey.

25. **Verification of Assistants.**—The compassman, flagman, chainmen, and axmen must be sworn under oath, that they assisted said deputy in executing said surveys, and that, to the best of their knowledge and belief, the work has been strictly performed according to the instructions furnished by the Surveyor-General.

26. **Approval and certificate of the Surveyor-General.**—The Surveyor-General will attach his official approval to each of the original field books, and affix his official certificate to the copies of the field notes transmitted to the general land office, that they are true copies of the originals on file in his office.

The following specimen pages of field notes, taken from the *United States Manual of Surveying Instructions*, will illustrate the subject.

FIELD NOTES

OF THE

Exterior and Subdivision Lines

OF TOWNSHIP 25 NORTH, RANGE 2 WEST,

WILLAMETTE MERIDIAN,

OREGON.

Surveyed by Robert Acres, Deputy Surveyor,

Under his contract, dated —, 18—.

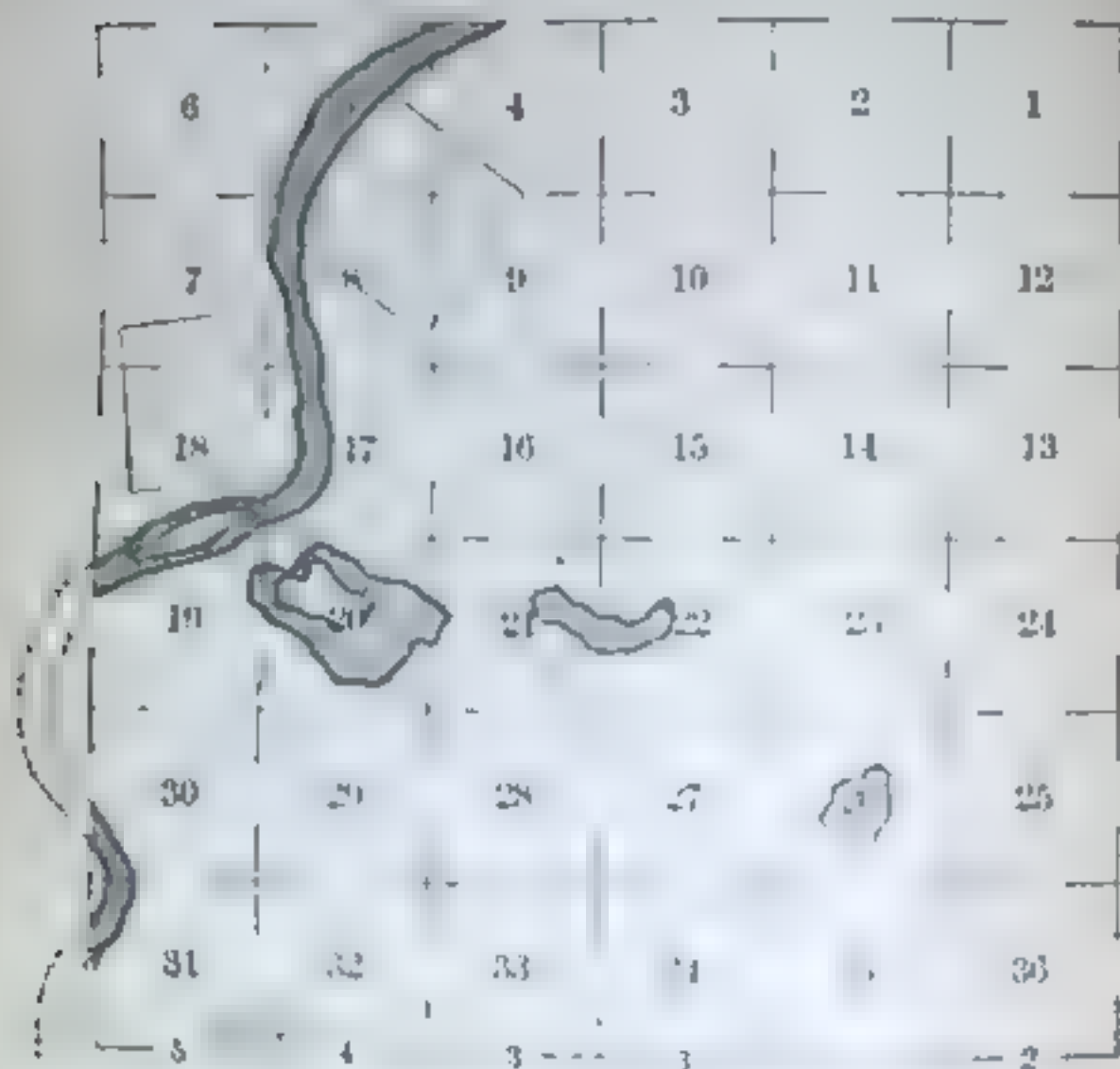
Survey commenced —.

Survey completed —.

264. Index.

Recovering the lines to the pages of the field notes.

T. 25 N., R. 2 W., Willamette Meridian.



The lines numbered are described in the notes on the pages indicated by the numbers.

NAMES OF SURVEYOR AND ASSISTANTS.

Robert Acres, Surveyor	George Sheer	Assessor.
Peter Long, Chairman	Adam D. J.	Assessor.
John Short, Chairman	Henry Elm	Comptroller.

265. Field Notes.

South Boundary, T. 25 N, R. 2 W, Willamette Meridian.

Chains.

Begin at the post, the established corner to Townships 24 and 25 North, in Ranges 2 and 3 West. The witness trees all standing, and agree with the description furnished me by the office, viz:

A Black Oak, 20 in. dia., N. 37° E. 27 links.

A Burr-oak, 24 in. dia., N. 43° W. 35 links.

A Maple, 18 in. dia., S. 27° W. 39 buks.

A White Oak, 15 in dia., S. 17° E 41 buks.

East on a random line on the South Boundaries of sections 31, 32, 33, 34, 35, and 36

Variation by Burt's improved solar compass, $18^{\circ} 41'$ E.

I set temporary half-mile and mile posts at every 40 and 80 chains, and at 5 miles, 74 chains 53 links, to a point 2 chains and 20 links north of the corner to Townships 24 and 25 North, Ranges 1 and 2 W.

(Therefore, the correction will be 5 chains,
17 links West, and 37 links South per mile.)

I find the corner post standing and the witness trees to agree with the description furnished me by the Surveyor-General's office, viz:

A Burr-oak, 17 in. dia., bears N. 41° E 31 links.

A White Oak, 16 in. dia., bears N. 26° W.
21 links.

A Linden, 20 in. dia., bears S 12° W 15 kts.,

A Black Oak, 24 in. dia., bears S. 27° E 14 links

(2)

North Boundary, T. 25 N., R. 2 W., Willamette Meridian.

Chains.	
	From the corner to Townships 24 and 25 N., Ranges 1 and 2 W., I run (at a variation of $18^{\circ} 41'$ East. [See Arts. 258, 289.]
10.00	N. $89^{\circ} 44'$ W., on a true line along the South Boundary of section 36, set a post for quarter section corner, from which
	A Beech, 24 in. dia., bears N. 11° E. 38 links dist.
	A Beech, 9 in. dia., bears S. 9° E. 17 links dist.
62.50	A Brook, 6 links wide, runs North.
80.00	Set a post for corner to sections 35 and 36, 1 and 2, from which
	A Beech, 9 in. dia., bears N. 22° E. 16 links dist.
	A Beech, 8 in. dia., bears N. 19° W. 14 links dist.
	A White Oak, 10 in. dia., bears S. 52° W. 7 links dist.
	A Black Oak, 11 in. dia., bears S. 46° E. 8 links dist.
	Land—level, good soil, fit for cultivation.
	Timber—Beech, various kinds of Oak, Ash, Hickory
40.00	N. $89^{\circ} 44'$ W. on a true line along the South Boundary of section 35, Variation $18^{\circ} 41'$ E.
	Set a post for quarter section corner, from which
	A Beech, 8 in. dia., bears N. 20° E. 8 links dist.
	No other tree convenient; made a trench around post

(3)

South Boundary, T. 25 N., R. 2 W., Willamette Meridian

Chains.	
65.00	Begin to ascend a moderate hill; bears N and S.
80.00	Set a post with trench, for corner of sections 34 and 35, 2 and 3, from which
	A Beech, 10 in. dia., bears N. 56° W. 9 links dist.
	A Beech, 10 in. dia., bears S. 51° E. 13 links dist.
	No other tree convenient to mark.
	Land—level, or gently rolling, and good for farming.
	Timber—Beech, Oak, Ash, and Hickory; some Walnut and Poplar.
40.00	N. $89^{\circ} 44'$ W. on a true line along the South Boundary of section 34, Variation $18^{\circ} 41'$ E.
	Set a quarter section post with trench, from which
	A Black Oak, 10 in. dia., bears N. 2° E. 635 links dist.
	No other tree convenient to mark.
80.00	To point for corner sections 33, 34, 3 and 4
	Drive charred stakes, raised mounds with trenches, as per instructions, from which
	A Burr-oak, 16 in. dia., bears N. 31° E. 344 links.
	A Hickory, 12 in. dia., bears S. 43° W. 231 links.
	No other tree convenient to mark.
	Land—level, rich, and good for farming.
	Timber—some scattering Oak and Walnut.

(4)

South Boundary, T. 25 N., R. 2 W., Willamette Township.

Chains.	N. 89° 44' W. on a true line along the South Boundary of section 33, Variation 18° 41' E.
37.51	A Black Oak, 24 in. dia.
40.00	Set a post for quarter section corner, from which
	A Black Oak, 18 in. dia., bears N. 25° E. 32 links dist.
	A White Oak, 15 in. dia., bears N. 43° W. 22 links dist.
62.00	To foot of steep hill, bears N. E. and S. W.
80.00	Set a post for corner to sections 32, 33, 4 and 5, from which
	A White Oak, 15 in. dia., bears N. 23° E. 27 links dist.
	A Black Oak, 20 in. dia., bears N. 82° W. 75 links dist.
	A Burr-oak, 20 in. dia., bears S. 37° W. 92 links dist.
	A White Oak, 24 in. dia., bears S. 26° E. 42 links dist.
	Land—gently rolling, rich farming land. Timber—Oak, Hickory, and Ash.

	N. 89° 44' W. on a true line along the South Boundary of section 32, Variation 18° 41' E.
37.50	A Creek, 20 links wide, runs North.
40.00	Set a granite stone, 14 in. long, 10 in. wide, and 4 in. thick, for quarter section corner, from which
	A Maple, 20 in. dia., bears N. 41° E. 25 links dist.
	A Birch, 21 in. dia., bears N. 35° W. 22 links dist.

(5)

South Boundary, T. 25 N., R. 2 W., Willamette Meridian.

Chains.	To S. E. edge of swamp.
76.00	As it is impossible to establish permanently the corner to sections 31, 32, 5 and 6, in the swamp, I therefore, at this point, 4.00 chains east of the true point for said section corner, raise a witness mound with trench, as per instructions, from which
	A Black Oak, 20 in. dia., bears N. 51° E. 115 links.
80.00	A point in deep swamp for corner to sections 31, 32, 5 and 6.
	Land—rich bottom; west of creek, part wet; east of creek, good for farming
	Timber—good; Oak, Hickory, and Walnut.
	N. 89° 44' W. on a true line along the South Boundary of section 31, Variation 18° 41' E.
11.00	Leave swamp and rise bluff 30 feet high, bears N. and S.
40.00	Set post for quarter section corner, from which
	A Sugar tree, 27 in. dia., bears S. 81° W. 12 links dist.
	A Beech, 24 in. dia., bears S. 71° E. 21 links dist.
54.00	Foot of rocky bluff 30 feet high, bears N. E. and S. W.
57.50	A spring branch comes out at the foot of the bluff, 5 links wide; runs N. W. into swamp.
61.00	Enter swamp; bears N. and S.
70.00	Leave swamp; bears N. and S.

(6)

North Boundary, T. 25 N., R. 2 W., Willamette Meridian.

Chains The swamp contains about 15 acres, the greater part in section 31.

74.73 The corner to Townships 24 and 25 N., Ranges 2 and 3 W.

Land—except the swamp, rolling, good, rich soil.

Timber—Sugar-tree, Beech, Swamp Maple.
Jan. 25th, 1854.

Between Ranges 2 and 3 West, from corner to Townships 24 and 25 N., I run

North, on the range line between sections 31 and 36, Variation $18^{\circ} 56'$ East.

8.56 Set a post on the left bank of Chickeeles river, for corner to fractional sections 31 and 36, from which

A Hackberry, 11 in. dia., bears N. 50° E. 11 links dist.

A Sycamore, 60 in. dia., bears S. 15° W. 24 links dist.

I now cause a flag to be set on the right bank of the river, and in the line between sections 31 and 36. I now cross the river, and from a point on the right bank thereof, west of the corner just established on the left bank, I run North on an offset line, 25 chains and 94 links, to a point 8 chains and 56 links west of the flag. I now set a post in the place of the flag, for corner to fractional sections 31 and 36, from which

A Beech, 10 in. dia., bears N. 2° E. 12 links dist.

(7)

Between Ranges 2 and 3 W., T. 25 N., Willamette Meridian.

Chains. A Black Oak, 12 in. dia., bears N. 80° W. 16 links dist.

34.50 The corner above described.

40.00 Set a post for $\frac{1}{4}$ section corner, from which
A Burr-oak, 20 in. dia., bears N. 37° E. 26 links dist.

A Black Oak, 24 in. dia., bears N. 80° W. 16 links dist.

43.41 A Black Walnut, 30 in. dia.

80.00 Set a post for corner to sections 30, 31, 25, and 36, from which

A Beech, 14 in. dia., bears N. 20° E. 14 links dist.

A Hickory, 9 in. dia., bears N. 25° W. 12 links dist.

A Beech, 16 in. dia., bears S. 40° W. 16 links dist.

A White Oak, 10 in. dia., bears S. 44° E. 20 links dist.

Land—level; rich bottom; not inundated.

Timber—Oak, Hickory, Beech, and Ash.

In like manner all the other Township lines are run.

General Description.

This township contains a large amount of first-rate land for farming. It is well timbered with Oak, Hickory, Sugar-tree, Walnut, Beech, and Ash.

Chickeeles river is navigable for small boats in low water, and does not often overflow its banks, which are from ten to fifteen feet high.

The township will admit of a large settlement, and should therefore be subdivided.

(8)

*Field Notes of the Subdivision Lines and Meanders
of Clackamas River, in Township 25 N.,
R. 2 W., Willamette Meridian.*

Chains.	To determine the proper adjustment of my compass for subdividing this township, I commence at the corner to Townships 21 and 25 N., R. 1 and 2 W., and run
	North, on a blank line along the East Boundary of section 36, Variation $17^{\circ} 51'$ East,
40.05	To a point 5 links west of the quarter section corner.
80.09	To a point 12 links west of the corner to sections 25 and 36.
	To retrace this line, or run parallel thereto, my compass must be adjusted to a variation of $17^{\circ} 46'$ East.
	Subdivision commenced Feb. 1, 1854.
	From the corner to sections 1, 2, 35, and 36, on the South Boundary of the Township, I run
	North, between sections 35 and 36, Variation $17^{\circ} 46'$ East,
9.19	A Beech, 30 in. dia.
29.97	A Beech, 30 in. dia.
40.00	Set a post for quarter section corner, from which
	A Beech, 8 in. dia., bears N. 23° W. 45 links dist.
	A Beech, 15 in. dia., bears S. 48° E. 12 links dist.
51.00	A Beech, 18 in. dia.
76.00	A Sugar-tree, 30 in. dia.

(9)

Township 25 N., Range 2 W., Willamette Meridian.

Chains.	
80.00	Set a post for corner to sections 25, 26, 35, and 36, from which
	A Beech, 28 in. dia., bears N. 60° E. 45 links dist.
	A Beech, 24 in. dia., bears N. 62° W. 17 links dist.
	A Poplar, 20 in. dia., bears S. 70° W. 50 links dist.
	A Poplar, 36 in. dia., bears S. 66° E. 31 links dist.
	Land—level, second-rate.
	Timber—Poplar, Beech, Sugar-tree, and some Oak; undergrowth—same, and Hazel.
	East, on a random line between sections 25 and 36, Variation $17^{\circ} 46'$ East.
9.00	A Brook, 20 links wide, runs north.
15.00	To foot of hills, bears N. and S.
40.00	Set a post for temporary quarter section corner.
55.00	To opposite foot of hill, bears N. and S.
72.00	A brook, 15 links wide, runs N.
80.00	Intersected East Boundary at post corner to sections 25 and 36, from which corner I run
	West, on a true line between sections 25 and 36, Variation $17^{\circ} 46'$ East.
40.00	Set a post on top of hill, bears N. and S., from which
	A Hickory, 14 in. dia., bears N. 60° E. 27 links dist.
	A Beech, 15 in. dia., bears S. 74° W. 9 links dist.

(10)

Township 25 N., Range 2 W., Willamette Meridian.

Chains
N. 00

The corner to sections 25, 26, 35, and 36.
Land — east and west parts, level, first-rate;
middle part, broken, third-rate.

Timber — Beech, Oak, Ash, etc.; under-
growth — same, and Spice in the bottoms.

North, between sections 25 and 26, Vari-
ation $17^{\circ} 46'$ East.

7.00

A Poplar, 40 in. dia.

17.20

A Brook, 25 links wide, runs N. W.

18.05

A Walnut, 30 in. dia.

23.44

A Brook, 25 links wide, runs N. E.

40.00

Set a post for $\frac{1}{4}$ sec. corner, from which

A Burr-oak, 36 in. dia., bears N. 42° E. 18
links dist.

A Beech, 30 in. dia., bears S. 72° W. 9
links dist.

60.15

A Beech, 30 in. dia.

80.00

Set a post for corner to sections 23, 24, 25,
26, from which

A White Oak, 14 in. dia., bears N. 50° E.
40 links.

A Sugar-tree, 12 in. dia., bears N. 14° W.
31 links.

A White Oak, 13 in. dia., bears S. 38° W.
32 links.

A Sugar-tree, 12 in. dia., bears S. 42° E.
14 links.

Land — level on the line; high ridge of
hills through the middle of section 25, run-
ning N. and S.

Timber — Beech, Walnut, Ash, Maple, etc.

(11)

Township 25 N., Range 2 W., Willamette Meridian.

Chains In like manner other subdivision lines
are run.

*Notes of the Meanders of a Small Lake in
Section 26.*

Begin at the $\frac{1}{4}$ sec. cor. on the line between
sections 23 and 26, run thence South

24.00

To the margin of the lake, where set a
post for meander corner, from which

A Beech, 14 in. dia., bears N. 45° E. 10
links dist.

A Beech, 9 in. dia., bears N. 15° W. 14
links dist.

Thence meander around the lake as follows:
S. 53° E. 17.75. At 75 links, cross outlet
to lake 10 links wide, runs N. E.

S. 3° E. 13.00.

S. 30° W. 8.00.

S. 65° W. 12.00 to a point previously deter-
mined 20.30 chains North of the quarter sec-
tion corner on the line between sections 26
and 35.

Set post meander corner, Maple, 16 in. dia.,
bears S. 15° W. 20 links dist.

Ash, 12 in. dia., bears S. 21° E. 15 links
dist.

N. 63° W. 10.00

N. 13° W. 21.00

In this vicinity we
discovered remarkable
fossil remains of ani-
mals well worth the at-
tention of naturalists.

(12)

Township 25 N., Range 2 W., Willamette Meridian.

Courses N. 32° E. 17.30 to the place of beginning
This is a beautiful lake, with well-defined
banks from 6 to 10 feet high.
Land — first-rate.

Meanders of the left bank of Chickeeles River.

Begin at the corner to fractional sections 4 and 33, in the North Boundary of the Township, and on the left and S. E. bank of the river, and run thence down the stream with the meanders of the left bank of said river, in fractional section 4, as follows:

Courses.	Dist.	Remarks.
S. 76° W.	18.50	
S. 61° W.	10.00	
S. 59° W.	8.30	To the corner to fractional sections 4 and 5; thence in section 5,
S. 54° W.	10.70	
S. 40° W.	5.60	
S. 50° W.	8.50	
S. 37° W.	17.00	
S. 44° W.	22.00	
S. 38° W.	26.72	To the corner to fractional sections 5 and 8; thence in section 8,
S. 21° W.	16.00	
S. 10° W.	13.00	
South	8.50	To the head of rapids.
S. 9° E.	5.00	
S. 17° E.	20.00	
S. 10° E.	12.00	To the foot of rapids.
S. 22½° E.	8.46	To the corner to fractional sections 8 and 17
		Land, along fractional section 8,

(13)

Township 25 N., Range 2 W., Willamette Meridian.

Courses.	Dist.	Remarks.
		high, rich bottom; not inundated. The rapids are 37.00 chains long; rocky bottom; estimated fall, 10 feet.
		<i>Meanders in Section 17.</i>
S. 17° E.	15.00	At 5 chains, discovered a vein of coal, which appears to be 5 feet thick, and may be readily worked.
S. 8° E.	12.00	
S. 4° W.	22.00	At 3 chains, the ferry across the river to Williamsburgh, on the opposite side of the river.
S. 25° W.	17.00	
S. 78° W.	12.00	
S. 71° W.	9.55	To the corner to fractional sections 17 and 18; thence in section 18,
S. 65° W.	15.00	
S. 73½° W.	15.93	To the corner to fractional sections 18 and 19.
S. 65° W.	14.00	In section 19.
S. 60° W.	23.00	
S. 42° W.	10.00	
S. 20° W.	10.00	
S. 16½° W.	13.83	At 2 chains, cross outlet to pond and lake, 50 links wide, to the corner to fractional sections 19 and 24, on the range line, 32.50 chains North of the corner to sections 19, 30, 24, and 25.

The above selections will serve as specimens of the manner of taking the field notes.

266. General Description.

The quality of the land in this township is considerably above the average. There is a fair proportion of rich bottom-land, chiefly situated on both sides of Clackeeles river, which is navigable, through the township, for steamboats of light draft, except over the rapids in Section 8.

The uplands are generally rolling, good first and second rate land, etc.

267. Certificates.

I, Robert Acres, Deputy Surveyor, do solemnly swear that, in pursuance of a contract with _____, Surveyor of the public lands of the United States, in the State [or Territory] of _____, bearing date the _____ day of _____, 18____, and in strict conformity to the laws of the United States and the instructions furnished by the said Surveyor-General, I have faithfully surveyed the exterior boundaries [or subdivision and meanders, as the case may be] of Township number twenty-five North of the base line of Range number two West of the Willamette Meridian, in the _____ aforesaid; and do further solemnly swear that the _____ are the true and original field notes of such survey.

ROBERT ACRES,

Deputy Surveyor.

Subscribed by said Robert Acres, Deputy Surveyor, and sworn to before me, a Justice of the Peace for the _____ County, in the State [or Territory] of _____ this _____ day of _____, 18____.

HENRY DOOLITTLE,

Justice of the Peace.

We hereby certify that we assisted Robert Acres, Deputy Surveyor, in surveying the exterior boundaries, and subdividing Township number twenty-five North of the base line of Range number two West of the Willamette Meridian, and that said Township has been, in all respects, to the best of our knowledge and belief, well and faithfully surveyed, and the boundary monuments planted according to the instructions furnished by the Surveyor-General.

PETER LONG, *Chainman.*

JOHN SHORT, *Chainman.*

GEORGE SHARP, *Arman.*

ADAM DELL, *Arman.*

HENRY FLAGG, *Compassman.*

Subscribed and sworn to by the above named persons, before me, a Justice of the Peace for the county of _____, in the State [or Territory] of _____, this _____ day of _____, 18____.

HENRY DOOLITTLE,

Justice of the Peace

SURVEYOR'S OFFICE AT _____, 18____.

The foregoing field notes of the Survey of [here describe the survey], executed by Robert Acres, under his contract of the _____ day of _____, 18____, in the month of _____, 18____, having been critically examined, the necessary corrections and explanations made, the said field notes, and the surveys they describe, are hereby approved

A. B.,

Surveyor-General

To the notes of each Township, in the copies of the field notes transmitted to the seat of government, the Surveyor-General will append the following certificate

I certify that the foregoing transcript of the field notes of the Survey of the [here describe the character of the surveys, whether meridian, base line, standard parallel, exterior township lines, or subdivision lines and meanders of a particular township], in the State [or Territory] of _____, has been correctly copied from the original notes on file in this office. A. B.,

Surveyor-General.

268. Corners and Boundaries Unchangeable.

According to an act of Congress, entitled "An act concerning the mode of Surveying the Public Lands of the United States," approved February 11th, 1805, and still in force,

1st. "All the corners marked in the surveys returned by the Surveyor-General, shall be established as the proper corners of sections or subdivisions of sections which they were intended to designate; and the corners of half and quarter sections, not marked on said surveys, shall be placed, as nearly as possible, equidistant from those two corners which stand on the same line."

2d. "The boundary lines actually run and marked in the surveys returned by the Surveyor-General, shall be established as the proper boundary lines of the sections or subdivisions for which they were intended; and the length of such lines, as returned by the Surveyor-General aforesaid, shall be held and considered as the true length thereof."

If it is afterward found that a post is out of line, or that the line has been unequally subdivided, the general government only has the power of correction, and that only while it holds the title to the lands affected.

Such boundaries only as are established by the Surveyor-General, or the deputy, in the performance of his official duties, and in accordance with law, come under the above rules.

269. Restoring Lost Boundaries.

Lost boundaries must be restored in conformity with the laws under which they were originally established.

At an early day, three sets of section corners were established on the range lines; later, two sets on all the township boundaries; at present, the section lines close on previously established corners on township corners, making one set of corners, except on the base lines and standard parallels, where double corners—standard corners and closing corners—are established.

In order to restore lost boundaries correctly, the surveyor must know the manner in which townships were originally subdivided.

In case of three sets of corners on the range lines, one set was planted when the exteriors were run.

Corners on the east and west lines between two townships, belong to the sections of the township north.

From these corners, section lines were run due north, which would not, in general, close on the corners of the township line on the north, thus making two sets of corners on the north and south boundaries of the township.

The east and west lines were run due east and west from the last interior section corner, and new corners established at the intersections with the range lines.

In case of two sets of corners, the subdivisions were made as above, except that the east and west lines

were closed on the corners previously established on the east boundary, but were run due west from the last interior section corner to the range line, and new section corners established at the intersection with the range line.

The method of making but one set of corners, except on the base line and standard parallels, is the one now in vogue, and has been sufficiently considered.

270. Restoring Lost Corners.

Lost corners must be restored, if possible, to their exact original position.

The surveyor should seek to accomplish this, first, by the aid of bearing trees, mounds, etc., described in the original field notes.

If the corner can not be located in this way, good testimony may be taken.

It often happens that in retracing lines, the measurements do not agree with the field notes. When such cases occur, from whatever cause, the surveyor must establish his corners at intervals proportional to those given in the original field notes.

1. *To restore a lost corner common to four sections.*

Find the distances between the nearest noted line trees or well-defined corners, north and south, and east and west of the lost corner. Establish the corner between them at a point intercepting distances proportional to those given in the original notes.

2. *To restore one of a double corner when the other is standing.*

First ascertain to which sections the existing corner belongs. Then re-establish the lost corner in the

direction and at the distance stated in the original notes. Verify the work by chaining to noted line trees or corners, having previously compared your chaining with that of the United States deputy by re-chaining between corners noted in the original survey, and making all distances proportional.

3. *To restore that one of a double corner established in running the township line when both are missing.*

Run a straight line between the nearest noted line trees or corners on the line, and, at the distance given in the notes, establish the corner which will be common to two sections north or west of the line.

Let the accuracy of the result be verified by measuring to the next section corner west or north.

4. *To restore that one of a double corner established in subdividing the township when both are missing.*

Retrace the section line which closed on the corner, and establish the section post at the intersection with the township line. Verify the result by measuring on the township line to noted objects.

The restored corner will be common to two sections south or east of the line.

5. *To restore one of a triple corner, on a range line when one at least remains standing.*

The one of the triple corner, established when the range line was run, is not a section corner.

First identify the existing corners, then establish the lost corner, according to the field notes, north or south of the existing corner, on the line, and verify the result.

If the field notes do not give the distances between the triple corners, retrace the section line closing on said corner.

6. To restore a triple corner when all are lost.

Rechain the range line, and retrace the section lines closing on the range line.

7. To restore lost quarter section corners.

1st. Except on those section lines which close on the north or west boundaries of a township, quarter section corners are equidistant between the two section corners. Hence, rechain the section line, then chain back one-half the distance.

2d. On township lines, where there may be double section corners, only one set of quarter section corners are actually marked in the field — those established when the exteriors are run half-way between the section corners established at the same time. These are restored as above.

The same will apply when there are triple corners.

3d. If the section line closes on the north or west boundary of a township, the quarter section corner must be established 40 chains of the original measurement from the last interior section corner.

8. To restore lost township corners.

1st. If the corner is common to four townships, retrace the township and range lines, and establish the corner at their intersection.

2d. If the corner is common only to two townships, as may be the case on the base line or standard parallels, retrace the base line or standard parallel from the

last standing corner, if the lost corner is common to two townships north; but if the lost corner is common to two townships south, retrace also the range line.

9. To restore lost meander corners.

Retrace the lines which close upon the banks in the direction they were originally run.

Fractional section lines closing on Indian boundaries, private grants, etc., should be retraced, and the corners established in the same manner.

Remark.—If, in restoring a lost corner, the original corner is found by some unmistakable trace, it must stand, and the resurvey be made to correspond.

271. Subdividing Sections.

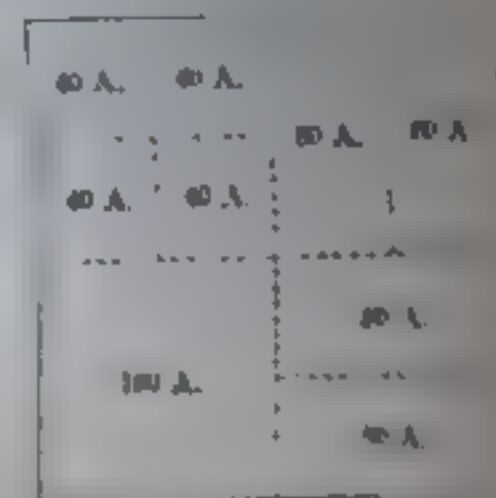
The United States deputy runs only the exterior or section lines, and makes the section and quarter section corners.

Lines joining the opposite quarter section corners divide the section into quarter sections of 160 acres each.

These quarter sections are divisible into half-quarters of 80 acres, and these into quarter-quarters of 40 acres.

These are the legal subdivisions of a section, and are exhibited in the annexed diagram.

If private parties wish the subdivision lines traced on the ground, they employ the county surveyor, or a private surveyor, who must be governed by the section and quarter section corners previously established.



The following rules will enable the surveyor to subdivide a section in accordance with the laws of the United States.

1. The original section and quarter section corners must stand where they were established by the government surveyor.

2. The quarter-quarter corners must be established equidistant, and on the line between the section and quarter section corners of the exterior lines of the section, and equidistant and on the line between quarter section corners of internal lines of the section.

3. All subdivision lines must run straight from the proper corner in one exterior line of the section to the corresponding corner in the opposite exterior line.

4. In fractional sections, where no opposite corresponding corner has been established, the subdivision line must be run from the given corner due north and south, or east and west, to the exterior boundary of said fractional section.

5. Anomalous sections or sections larger than a mile, sometimes close on a previously established line, in finishing up a public survey.

Quarter section and section corners are established 40 chains and 80 chains, respectively, from the previously established corners, and posts are planted every 20 chains of the remaining distance.

Anomalous sections are subdivided by running straight lines from the corners on the south line to the corresponding corners on the north, and east, and west lines, the same as in regular sections.

VARIATION OF THE NEEDLE.

272. Definitions and Illustrations.

The variation of the needle is the angle which the magnetic meridian makes with the true meridian.

The variation is *east* or *west*, according as the north end of the needle is east or west of the true meridian.

The variation is different at different places, and it does not remain the same at the same place.

The line of no variation is that line traced through those points on the surface of the earth where the needle points due north.

At all places east of this line, the variation is west; and at all places west of this line, the variation is east.

West variation is designated by the sign *plus*, and east variation by the sign *minus*.

In the year 1840, at a point whose latitude is $40^{\circ} 53'$, and longitude $80^{\circ} 13'$, being a little S. E. of Cleveland, O., the variation was nothing. The line of no variation passed through this point $N\ 24^{\circ} 35' W$, and $S\ 24^{\circ} 35' E$.

273. Changes of Variation.

1. **Irregular changes.**—The needle is subject to sudden changes coincident, in time, with a thunder storm, an aurora borealis, solar changes, etc.

2. **Diurnal changes.**—In the northern hemisphere, the north end of the needle moves from $10'$ to $15'$ west from about 8 A. M. to 2 P. M., and then gradually returns to its former position.

3 **Annual changes.** The diurnal changes vary with the season, being about twice as great in the summer as in the winter.

4 **Secular changes.**—In addition to the above changes, there is a change of variation, in the same direction, running with considerable regularity through a period of about 234 years, as is indicated by observations at Paris.

In the United States, the north end of the needle was moving east from the earliest recorded observations till about the year 1810, since which time the movement has been west, at the rate, on an average, of about 5' per annum.

We give the following tables of places, their latitude and longitude, and variation as it was in 1840, and the annual change of variation, from the tables prepared by Professor Loomis for the 39th and 42d volumes of Silliman's Journal:

Places near the Line of no Variation.

Places.	Lat.	Lon.	Var.	An. Mo.
A Point.	40° 53'	80° 13'	0° 00'	+ 4'.4
Cleveland, O.	41° 31'	81° 45'	— 0° 19'	4'.4
Mackinaw.	45° 51'	84° 41'	— 2° 08'	3'.9
Charlottesville, Va.	39° 02'	78° 30'	+ 0° 19'	3'.7

Assuming the annual motion uniform, and correctly found for 1840, the variation for any subsequent time can be found by multiplying the annual motion by the number of years since 1840, and taking the algebraic sum of the product and the variation at that date.

Places where the Variation was West.

Places.	Lat.	Lon.	Var.	An. Mo.
Point in Maine.	48° 00'	67° 37'	+ 19° 30'	+ 8'.8
Waterville, Me.	44° 27'	69° 32'	12° 36'	5'.7
Montreal.	45° 31'	73° 35'	10° 18'	5'.7
Burlington, Vt.	44° 27'	73° 10'	9° 27'	5'.3
Hanover, N. H.	43° 42'	72° 14'	9° 20'	5'.2
Cambridge, Mass.	42° 22'	71° 08'	9° 12'	5'.
Hartford, Conn.	41° 46'	72° 41'	6° 58'	5'.
Newport, R. I.	41° 28'	71° 21'	7° 45'	5'.
Geneva, N. Y.	42° 52'	77° 03'	4° 18'	4'.1
West Point	41° 25'	74° 00'	6° 52'	4'.
New York City.	40° 43'	71° 01'	5° 34'	3'.6
Philadelphia.	39° 57'	75° 11'	4° 08'	3'.2
Buffalo, N. Y.	42° 52'	79° 06'	1° 37'	1'.1

Places where the Variation was East.

Places.	Lat.	Lon.	Var.	An. Mo.
Jacksonville, Ill.	34° 43'	90° 20'	8° 28'	+ 2'.5
St. Louis, Mo.	38° 57'	90° 17'	8° 37'	2'.3
Nashville, Tenn.	36° 10'	86° 52'	6° 42'	2'.
Leavenworth, Mo.	29° 40'	94° 00'	8° 41'	1'.4
Mobile, Ala.	30° 42'	88° 16'	7° 05'	1'.4
Tuscan, Ala.	33° 12'	87° 43'	7° 26'	1'.6
Columbus, Ga.	32° 28'	85° 11'	5° 28'	2'.
Milledgeville, Ga.	33° 07'	83° 24'	5° 07'	2'.4
Savannah, Ga.	32° 05'	81° 12'	4° 13'	2'.7
Tallahassee, Fla.	30° 26'	84° 27'	5° 03'	1'.8
Pensacola, Fla.	30° 24'	87° 23'	5° 53'	1'.4
Logansport, Ind.	40° 45'	86° 22'	5° 24'	2'.7
Cincinnati, O.	39° 06'	84° 27'	4° 46'	3'.1

274. Methods of Ascertaining the Variation.

First establish a true meridian, which may be done

1. *By use of Burt's Solar Compass,*

2. *By observation of the North star, when on the meridian.*

The north star is about $1^{\circ} 22'$ from the true pole, around which it revolves in a sidereal day, or 23 h., 56 m., 4 s.

Twice in this period the star will be on the meridian.

The exact moment of its passage can be determined very nearly, from the fact that it reaches the meridian almost at the same instant as Alioth in the tail of the Great Bear, or the first star in the handle of the Dipper.

Suspend a plumb line a few feet in front of the telescope, and place a faint light near the object glass of the telescope, so that the spider lines may be seen.



Just 17 minutes after the plumb line, the North star, and Alioth all fall on the vertical spider line, the North star is on the meridian.

The horizontal limb of the instrument is then firmly clamped, and the telescope is turned to be horizontal.

A light, shining through a small aperture in a board, at some distance, say ten rods, is moved by an assistant, according to signals, till it ranges with the intersection of the spider lines.

A stake driven into the ground directly under the light, and another directly under the telescope, will mark, on the ground, the true meridian.

The season of the year may be such that Alioth may be above instead of below the North star, when both are on the meridian at night. With the telescope, the stars can be seen in the day-time.

3. *By the azimuth of the North star.*

When the North star is farthest from the meridian, east or west, it is said to be at its greatest eastern or western elongation.

The azimuth of a star is the angle which a vertical plane, through the star, makes with the meridian plane.

Let us now find the azimuth of the North star at its greatest elongation.

Let Z be the zenith, P the pole, S the North star at its greatest elongation, ZP , ZS , and PS arcs of great circles. Then ZPS will be a spherical triangle, right-angled at S , and the angle Z will be the azimuth, PS the greatest elongation, and ZP the complement of latitude, since the elevation of the pole above the horizon is equal to the latitude.



Now from Napier's principles, we have

$$\sin e = \cos l \cos (90^{\circ} - Z).$$

$$\therefore \sin Z = \frac{\sin e}{\cos l}.$$

Introducing R and applying logarithms, we have

$$\log \sin Z = 10 + \log \sin e - \log \cos l.$$

Hence, the azimuth is readily computed if we know the greatest elongation of the star and the latitude of the place.

Greatest Elongation of Polaris.

<i>Date.</i>	<i>Elongation.</i>	<i>Date.</i>	<i>Elongation.</i>	<i>Date.</i>	<i>Elongation.</i>
1870	1° 23' 01".	1880	1° 19' 50".4	1890	1° 16' 40".7
1871	1° 22' 41".9	1881	1° 19' 31".4	1891	1° 16' 21".8
1872	1° 22' 22".9	1882	1° 19' 12".5	1892	1° 16' 03".
1873	1° 22' 03".8	1883	1° 18' 53".5	1893	1° 15' 44".1
1874	1° 21' 44".8	1884	1° 18' 34".5	1894	1° 15' 25".3
1875	1° 21' 25".7	1885	1° 18' 15".5	1895	1° 15' 06".4
1876	1° 21' 06".6	1886	1° 17' 56".6	1896	1° 14' 47".6
1877	1° 20' 47".6	1887	1° 17' 37".6	1897	1° 14' 28".7
1878	1° 20' 28".5	1888	1° 17' 18".6	1898	1° 14' 09".9
1879	1° 20' 09".5	1889	1° 16' 59".7	1899	1° 13' 51".

The elongation in the table is given for the 1st of January of each year; but the elongation for any month of the year can be readily found.

Thus, let us find the elongation for May 1st, 1873.

Jan. 1st, 1873, Elongation	1° 22' 03".8
Jan. 1st, 1874, Elongation	1° 21' 44".8
Change for 12 months	19"
Change for 4 months	6.3"

Then, for May 1st, 1873, we shall have,

$$\text{Elongation} = 1^{\circ} 22' 03".8 - 6 - 1^{\circ} 21' 57".5.$$

1. Find the azimuth of the North star at its greatest elongation, May 1st, 1873 — latitude 40°. *Ans.* 1° 47'.

2. Find the azimuth of the North star at its greatest elongation, July 1st, 1877 — latitude 42°. *Ans.* 1° 49½'.

3. Find the azimuth of the North star at its greatest elongation, Sept. 21st, 1880 — latitude 45°. *Ans.* 1° 51½'.

It will be necessary to know the times of the greatest elongation. These times are given in the following tables, for the 1st, 11th, and 21st of each month of the year 1880, which will answer the purpose for the rest of the century, since the change of time is very slow, being only about 16 minutes in 50 years.

Eastern Elongation.

<i>Month.</i>	<i>1st day.</i>	<i>11th day.</i>	<i>21st day.</i>
April.	6h. 40m. A.M.	6h. 01m. A.M.	5h. 22m. A.M.
May.	4h. 42m. A.M.	4h. 03m. A.M.	3h. 24m. A.M.
June.	2h. 41m. A.M.	2h. 01m. A.M.	1h. 22m. A.M.
July.	0h. 43m. A.M.	0h. 00m. A.M.	11h. 21m. P.M.
August.	10h. 38m. P.M.	9h. 59m. P.M.	9h. 19m. P.M.
Sept.	8h. 36m. P.M.	7h. 57m. P.M.	7h. 17m. P.M.

Western Elongation.

<i>Month.</i>	<i>1st day.</i>	<i>11th day.</i>	<i>21st day.</i>
Oct.	6h. 31m. A.M.	5h. 52m. A.M.	5h. 13m. A.M.
Nov.	4h. 30m. A.M.	3h. 50m. A.M.	3h. 11m. A.M.
Dec.	2h. 31m. A.M.	1h. 52m. A.M.	1h. 13m. A.M.
Jan.	0h. 28m. A.M.	11h. 44m. P.M.	11h. 04m. P.M.
Feb.	10h. 22m. P.M.	9h. 42m. P.M.	9h. 03m. P.M.
March.	8h. 31m. P.M.	7h. 52m. P.M.	7h. 13m. P.M.

About half an hour before the greatest eastern or western elongation, place the transit in a convenient position, and level it carefully.

Paste white paper on a board about one foot square, and perforate the board through the center with a two-inch auger, and, on the lower edge, fix some contrivance for holding a candle.

Let this board be fixed to a vertical staff, so as to slide freely up and down, and let it be placed about one foot in front of the telescope, so that the light reflected from the paper will render the spider lines visible.

Slide the board up or down the staff till the North star is visible through the telescope and orifice in the board, and bring the vertical spider line in range with the star.

As the star approaches its greatest elongation, move the telescope by a tangent screw, so as to keep the vertical line in range with the star. When the star reaches its greatest elongation, it will appear, for some time, to coincide with the spider line, and then leave it in the opposite direction.

Clamp the horizontal limb, and turn the telescope down till it is horizontal.

Let now a staff, with a light on its upper end, be carried ten or fifteen rods distant, toward the star, and placed so as to range, when vertical, with the vertical spider line of the telescope.

Drive a stake at the foot of the staff, and another directly under the instrument, then will the line determined by the stakes make an angle with the true meridian, equal to the azimuth of the North star. The true meridian will lie west or east of the line of stakes, north of the telescope, according as the elongation was east or west, and may readily be located by the instrument.

The location of the meridian can be verified thus:

Let AB be the line of the stakes produced to a considerable distance, say from 20 to 40



chains, A the azimuth angle, AC the true meridian, and BC perpendicular to AB .

BC can be found from the formula,

$$BC = AB \tan A.$$

Then laying off BC on the ground, and driving a stake at C , the stakes A and C will trace the true meridian.

Having found the true meridian, the variation of the needle can be readily determined by turning the telescope or the sights of the compass in the direction AC .

Without finding the true meridian, the bearing of AB being equal to the known azimuth of the North star at its greatest elongation, the variation of the needle can be found by directing the telescope or the sights of the compass in the direction AB .

The following method may be resorted to by the surveyor who does not possess an instrument with a telescope.

Fix a plank, firmly level, east and west, about three feet above the ground; then take a board about six inches square, and having detached one of the compasses, fix it to the board, at right angles with its upper edge. Drive a nail obliquely a little way into the board, so that it can be tacked to the plank.

About fifteen feet north of the plank suspend a plumb line, from the top of an inclined stake of such height that the North star, when seen through the sight while the board rests on the plank, will appear about one foot below the upper end of the plumb line.

Suspend the plumb in a vessel of water to prevent the line from vibrating, and let an assistant hold a light near it, so that it can be seen through the sight.

About half an hour before the time of the greatest elongation of the North star, place the board on the plank, and slide so that the star and plumb line shall range when seen through the sight. As the star approaches its greatest elongation, move the board along the plank in the opposite direction, so as to keep the range.

When the star reaches its greatest elongation, it will appear to keep the range for several minutes, then it will move slowly in the opposite direction.

Tack the board to the plank, taking care not to change its position. Then let a staff with a light on its top be placed about ten rods farther to the north, so as to range, when vertical, through the sight, with the plumb line.

Drive a stake at the foot of the staff, and one directly under the plumb line, then will the line of the stakes make, with the meridian, an angle equal to the azimuth of the North star at its greatest elongation.

The true meridian, and the variation of the compass, can then be found as above.

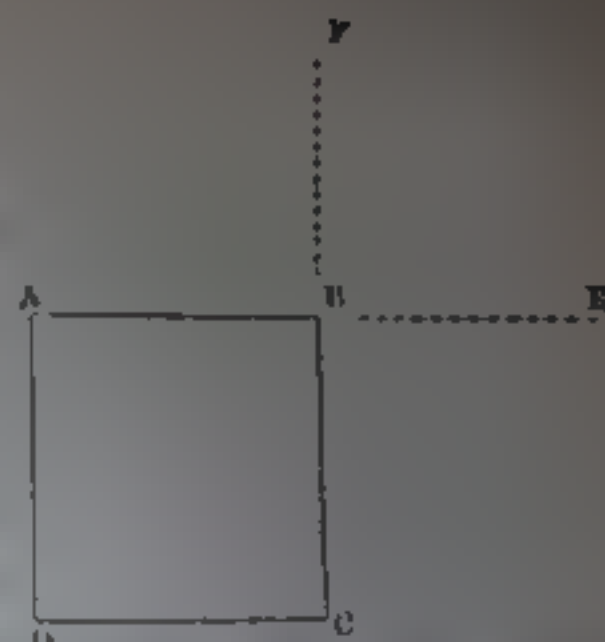
FIELD OPERATIONS

275. Finding Corners.

In searching for a corner, first see if the monument, whether tree, post, stake, or stone, is given and witnessed in the original field notes, and, if found, must be considered correctly as establishing the corner.

If no monument can be found, the corner can often be found by indirect methods, of which the following are the most available:

Thus, if a monument can be found at each of the corners A , C , D , but not at B , find the corners E and F , at each of which set up a flag-staff or high pole, and send the flag-man as near to B as possible, and let him stand facing D , so that he can see signals made both at A and C .



The observer at A can, by waving his hand, bring the flag-man in the line AE , and the observer at C can bring him in the line CF , and being in both lines, AE and CF , at the same time, he will be at their intersection B , the corner required.

If the corner E can be found, but not F , measure AB the required distance in the line AE . If the distance AB is not known, but it is simply known that AB is equal to DC , first measure DC . If neither E nor F can be found, run AB parallel to DC , and CB parallel to DA , and the intersection of these lines will determine B , if the field is a parallelogram.

If the field is not a parallelogram, retrace one of the lines terminated by known corners, and compare the bearing with the bearing in the original notes, which will give the variation of the needle. Then run the lines AB and CB from the notes, allowing for the variation, and the intersection will determine B .

In like manner two or more lost corners may be found.

If the bearings and distances are given in the original notes, and but one corner can be found, retrace some established line in the neighborhood to find the variation, and, beginning at the known corner, run the lines from the notes, allowing for the variation.

The importance of allowing for the variation may be illustrated thus.

Let the full lines bound the lot.

If the surveyor should run this lot from the original notes, one corner being known, the dotted lines would mark the boundaries as run, and their intersections the corners, thus encroaching on one side, and leaving gaps on the other, which of course would never do.



276. Finding Bearings and Distances.

After finding the corners, set a stake at each, and, beginning at any corner, place the compass or transit directly over the stake, and send the flag-man to the next corner, who must place the flag-staff on the stake.

Take the bearing, and measure the distance as heretofore directed; and, in like manner, find the bearings and distances of the remaining sides.

If obstacles should prevent the taking of the bearing of any line, measure the same distance from each corner, at right angles to the line, on the same side, so as to secure a line free from obstacles, and take the bearing of this line, which will be the bearing of the required line, since they are parallel.

Lines are measured a little to one side when fences, ponds, or other obstacles, are in the line.

Thus, if the perpendiculars AC and BD are equal,

$$CD = AB$$

AB can be found by Trigonometry, if AE and EB and two angles be measured



277. Offsets.

Offsets are perpendiculars measured from a line to the angles of a neighboring broken line, or to the banks or centers of creeks, rivers, or other bodies of water. Thus, a , b , c .



278. Taking Field Notes.

First Method.

Sta.	Bearings.	Dist.
1	N. 20° E.	15.50
2	E.	18.00
3	S. 20° E.	30.00
4	W.	25.00
	N. 32½° W.	16.09

Second Method



The first method is in the proper form for calculation, and may be conveniently employed when it is not important to make a map of the lot surveyed.

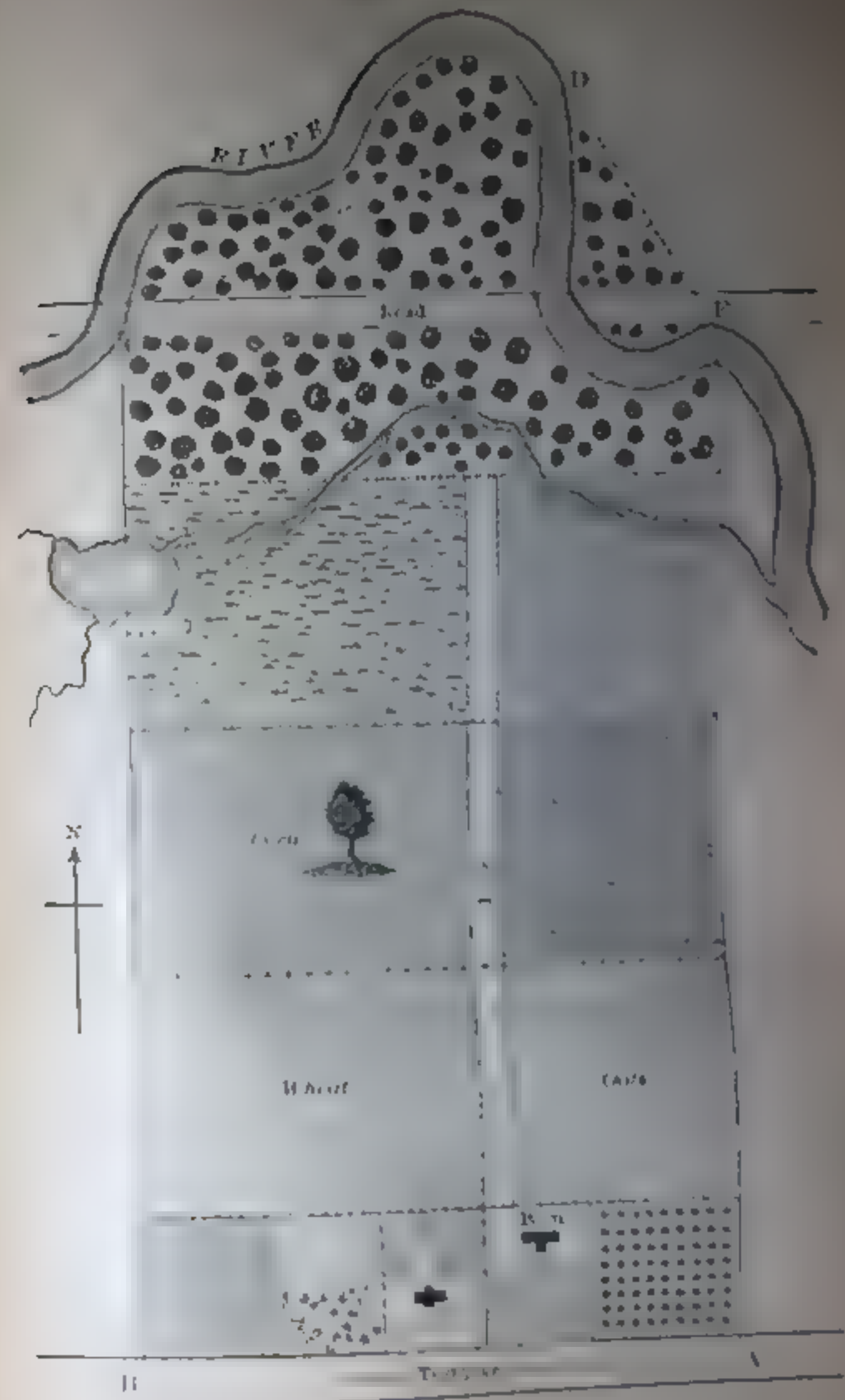
The second method, being a random outline with bearings and distances indicated, may be employed when it is desirable for the surveyor to keep before him, while at work, an outline of the lot.

Field Method.

	18.00	Station A
	37.00	Orchard fence
	42.00	Outfield fence
	28.00	Meadow fence
	14.00	S. Bank of Creek
	13.20	N. Bank of Creek
	10.80	Pasture fence
	4.80	S. Bank of River
Station E	△	S. Left Bank of River
	18.40	N. Bank of River
	17.40	Offset
	10.40	Offset
	10.50	
Station D	△	S. 32° E. Left Bank of River
	31.00	Left Bank of River
	30.00	Right Bank of River
	23.00	Offset
	16.40	Offset
	7.30	Offset
	4.80	N. Line of Road
Station C	△	N. 63° E. Right Bank of River
	68.00	Road East
	54.00	Woods
	65.20	Pond
	48.40	
	42.00	Pasture fence
	26.00	Cornfield fence
	10.52	Wheatfield fence
Station B	△	N. Middle of Turnpike
	40.00	Lot Line
	31.20	Meadow fence
	24.00	Grove fence
	17.20	Dooryard fence
	10.08	Orchard fence
Station A	△	W. Middle of Turnpike

MAP OF FARM

Scale 16 p. to 1 inch.



from the origin to the lines of farms, creeks, etc., which it intersects.

Set temporary stakes at the angles, and at convenient distances along the middle line, to guide in making the road, and plant monuments at a given distance and bearing from the angular points, so that they will not be disturbed in making or working the road. Take notes, and make a correct plot of the road.

281. Surveying Towns.

Commence at the intersection of principal streets, take their bearings, measure their lengths, noting the distances to the streets and alleys crossed, taking offsets to corners of streets and prominent objects, as public buildings, etc., till a prominent cross-street is reached, which survey in the same manner, changing the courses at such stations as will lead back to the original station.

Survey all the streets and alleys enclosed. Then survey an adjoining district, and so on, till the entire town or city has been surveyed.

Take notes, and make an accurate map of the town, on which locate not only the streets and alleys, but public buildings, parks, fountains, monuments, etc.

282. Reverse Bearing.

Let AB be a line run from A to B , AN and BS meridians, then will NAB be the bearing of AB , and SBA will be the reverse bearing.

Since the meridians AN and BS may be regarded as parallel, the bearing and reverse



bearing are equal. Thus, if the bearing of AB is $N. 30^\circ E.$, the reverse bearing is $S. 30^\circ W.$

The bearing and reverse bearing agree in the value of the angle, and differ in both the letters which indicate the general direction of the line. In fact, the reverse bearing of a line is the bearing of the line if run in the opposite direction. Thus, SBA , the reverse bearing of the line AB , run from A to B , is the bearing of the line BA , run from B to A .

Of the letters used in bearings, we shall call N and S latitude letters, and E and W departure letters.

To guard against inaccurate observations, and the disturbance of the needle occasioned by local attraction, the reverse bearing should be taken at every station. If the bearing and reverse bearing agree in value, the bearing may be considered as correctly taken; if they differ materially, both should be taken again. If they still differ, the difference may be regarded as occasioned by local attraction.

To ascertain at which station the local attraction exists, place the instrument at a third station, at a considerable distance from each of the doubtful stations, and sight to each, then from these back to the third station. The local attraction may be considered to exist at the station where the bearing of the third station disagrees with its bearing taken at the third station.

If the error occurred in the foresight, correct it before entering the bearing in the field notes, and note the amount of disturbance; if the error occurred in the backsight, the next foresight will be affected, and should be corrected before entered.

PRELIMINARY CALCULATIONS.

283. Angles between Courses.

1. If the latitude letters are alike, also the departure letters, the included angle is equal to the difference of the bearings.

If AB bears N. 40° E., and AC N. 20° E., $BAC = BAN - CAN = 40^\circ - 20^\circ = 20^\circ$.

If AD bears S. 40° W., and AE S. 20° W., $DAE = DAS - EAS = 40^\circ - 20^\circ = 20^\circ$.



2. If the latitude letters are alike, and the departure letters unlike, the included angle is equal to the sum of the bearings.

If AB bears N. 38° E., and AC N. 18° W., $BAC = BAN + NAC = 38^\circ + 18^\circ = 56^\circ$.

If AD bears S. 38° W., and AE S. 18° E., $DAE = DAS + SAE = 38^\circ + 18^\circ = 56^\circ$.

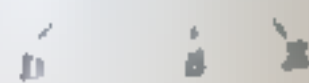


3. If the latitude letters are unlike, and the departure letters alike, the included angle is equal to 180° minus the sum of the bearings.

If AB bears N. 45° E., and AC S. 30° E., $BAC = 180^\circ - (NAB + SAC) = 180^\circ - 75^\circ = 105^\circ$.



If AD bears S. 45° W., and AE N. 30° W., $DAE = 180^\circ - (DAS + EAN) = 180^\circ - 75^\circ = 105^\circ$.



4. If the latitude letters are unlike, also the departure letters, the included angle is equal to 180° minus the difference of the bearings.

If AB bears N. 45° E., and AC S. 15° W., $BAC = 180^\circ - (NAB - SAC) = 180^\circ - 30^\circ = 150^\circ$.

If AD bears S. 45° W., and AE N. 15° E., $DAE = 180^\circ - (SAD - NAE) = 180^\circ - 30^\circ = 150^\circ$.



Remark. These principles apply when both courses run from or toward the vertex; if one runs from the vertex, and the other toward it, reverse the bearing of one side before applying the principles.

284. Examples.

1. Find the angle A , if AB bears N. 78° E., and AC N. 24° E. Ans. 54° .

2. Find the angle A , if BA bears S. 31° E., and AC S. 48° W. Ans. 109° .

3. Find the angle A , if BA bears S. 70° W., and CA N. 25° E. Ans. 155° .

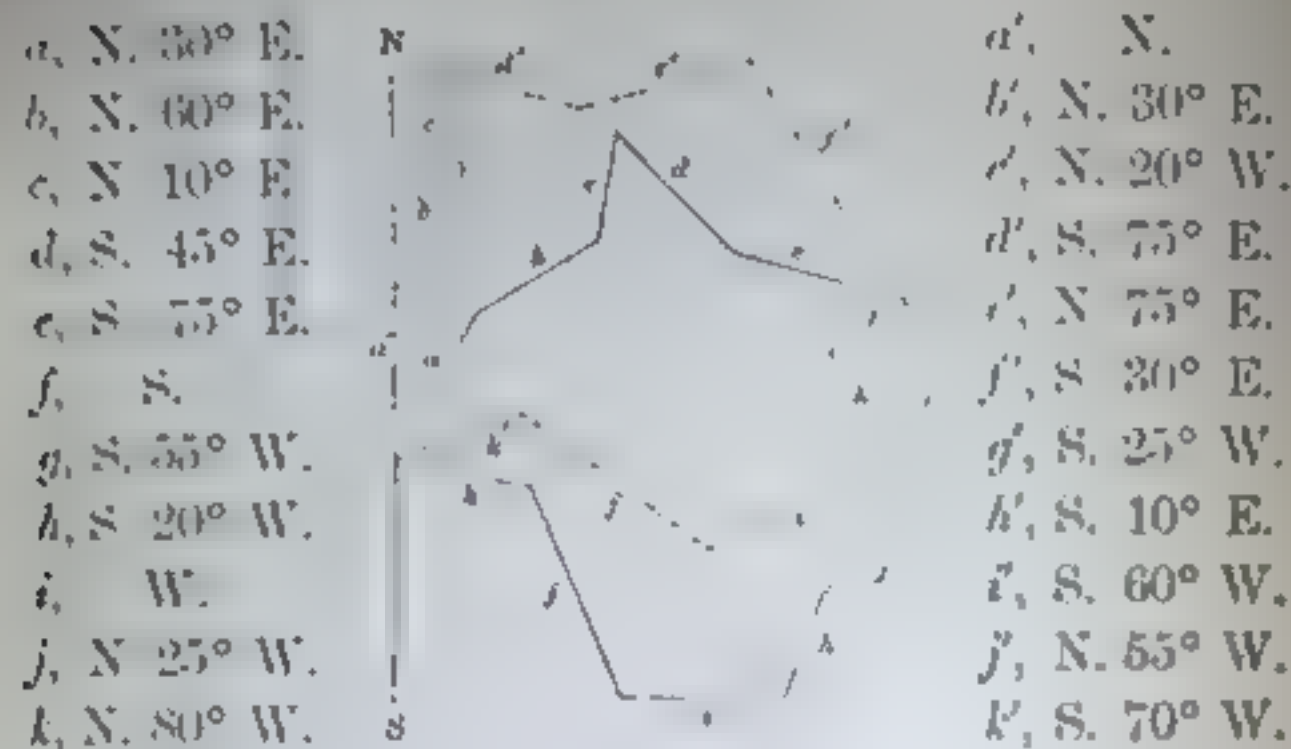
4. Find the angles of the polygon $ABCDE$, if AB bear N. 20° E.; BC , N. 60° E.; CD , S. 50° E.; DE , S. 40° W.; EA , N. 78° W.

Ans. $A = 72^\circ$, $B = 150^\circ$, $C = 110^\circ$, $D = 90^\circ$, $E = 118^\circ$.

285. Problem.

To find the bearings of the sides of a field, if the field be surveyed by a compass, and the sides to become a meridian.

In the following diagram let the full lines denote the original position of the sides of the field, a the side that is to become the meridian, and the dotted lines the revolved position of the sides.



From the above illustration we derive the following principles:

1. If the letters which indicate the general direction of the side which is to be made a meridian are both alike or both unlike those of another side, then,

1st. If the bearing of the former is less than that of the latter, the difference of the bearings will be the bearing of the latter, the letters remaining the same as before.

2d. If the bearing of the former is greater than that of the latter, the difference of the bearings will be the bearing of the latter, the departure letter being changed.

2. If one of the letters which indicate the general direction of the side which is to be made a meridian is like and the other unlike the corresponding letter of another side, then

1st. The sum of the bearings, if less than 90° , will be the bearing of that side, the letters remaining the same as before.

2d. If the sum of the bearings is greater than 90° , its supplement will be the bearing of that side, the latitude letter being changed.

286. Examples.

1. The bearings of the sides of a field are as follows: 1st, N. 30° E.; 2d, N. 60° E.; 3d, S. 40° E.; 4th, S. 30° W.; 5th, W.; 6th, N. $18\frac{1}{4}^\circ$ W. Find the bearings of the sides if the second side becomes a meridian.

Ans. 1st, N. 30° W.; 2d, N.; 3d, N. 80° E.; 4th, S. 30° E.; 5th, S. 30° W.; 6th, N. $78\frac{1}{4}^\circ$ W.

2. The bearings of the sides of a field are as follows: 1st, N. 45° W.; 2d, N. 18° E.; 3d, E.; 4th, N. 32° E.; 5th, S. $42\frac{1}{2}^\circ$ E.; 6th, S.; 7th, S. $65\frac{1}{4}^\circ$ W. Find the bearings if the first side be made a meridian.

Ans. 1st, N.; 2d, N. 63° E.; 3d, S. 45° E.; 4th, N. 77° E.; 5th, S. $2\frac{1}{2}^\circ$ W.; 6th, S. 45° W.; 7th, N. $67\frac{1}{4}^\circ$ W.

3. The bearings of the sides of a field are as follows: 1st, N. 20° E.; 2d, N. 70° E.; 3d, E.; 4th, S. 45° E.; 5th, S.; 6th, S. 45° W.; 7th, W.; 8th, N. $3\frac{1}{4}^\circ$ W. Find the bearings if the sixth side be made a meridian.

Ans. 1st, N. 25° W.; 2d, N. 25° E.; 3d, N. 45° E.; 4th, E.; 5th, S. 45° E.; 6th, S.; 7th, S. 45° W.; 8th, N. $48\frac{1}{4}^\circ$ W.

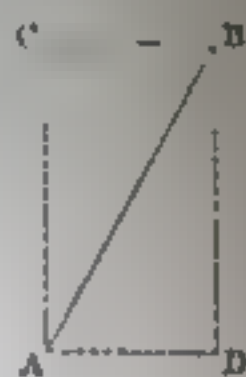
287. Latitude and Departure.

The latitude of a course is the distance between the two parallels of latitude passing through the extremities of the course.

The **departure** of a course is the distance between the two meridians passing through the extremities of the course.

Let AB be a course, AD and BC parallels of latitude, and AC and BD meridians. Then will AC or DB be the latitude of the course, and CB or AD its departure.

$$\text{But } AC = AB \times \cos CAB, \\ \text{and } CB = AB \times \sin CAB.$$



Hence, *latitude* = *course* \times *cosine of bearing*,
and *departure* = *course* \times *sine of bearing*.

If the line runs due east or west, its latitude is 0.

If the line runs due north or south its departure is 0.

Latitude *north* is considered *plus*; latitude *south*, *minus*.

Departure *east* is considered *plus*; departure *west*, *minus*.

For brevity let us designate the bearing by b , the course by c , the latitude by l , and departure by d , then we shall have the cases given in the following article:

288. Table of Cases.

	Given	Req		
1	$b, c,$	$l, d.$	$l = c \cos b,$	$d = c \sin b.$
2	$b, l,$	$c, d.$	$c = \frac{l}{\cos b},$	$d = l \tan b.$
3	$b, d,$	$c, l.$	$c = \frac{d}{\sin b},$	$l = d \cot b.$
4	$c, l,$	$b, d.$	$\cos b = \frac{l}{c},$	$d = \sqrt{c^2 - l^2}.$
5	$c, d,$	$b, l.$	$\sin b = \frac{d}{c},$	$l = \sqrt{c^2 - d^2}.$
6	$l, d,$	$b, c.$	$\tan b = \frac{d}{l},$	$c = \sqrt{l^2 + d^2}.$

289. Examples.

1. Given $b = N. 53^\circ 20' E.$, and $c = 26.50$ ch.; required l and d .
Ans. $l = 15.82$ ch. N., $d = 21.26$ ch. E.

2. Given $b = S. 75^\circ 47' W.$, and $l = 22.04$ ch. S.; required c and d .
Ans. $c = 89.75$ ch., $d = 87$ ch. W.

3. Given $b = N. 35^\circ W.$, and $d = 1.55$ ch. W.; required c and l .
Ans. $c = 2.70$ ch., $l = 2.21$ ch. N.

4. Given $c = 35.35$ ch., and $l = 31$ ch. N.; required b and d .
Ans. $b = N. 28^\circ 44' E.$ or $W.$, $d = 16.99$ ch. E. or W.

5. Given $c = 81.80$ ch., and $d = 22.89$ ch. W.; required b and l .
Ans. $b = N.$ or $S. 47^\circ W.$, and $l = 21.35$ ch. N. or S.

6. Given $l = 7.02$ ch. S., and $d = 7.14$ ch. W.; required b and c .
Ans. $b = S. 45^\circ 29' W.$, $c = 10.01$ ch.

290. Traverse Table.

The **traverse table** affords a ready method of finding the latitude and departure of a course whose distance and bearing are given.

Let us find the l and d of a line whose b is $N. 35^\circ 15' E.$, and $c = 47.85$ ch.

Turning to the traverse table, under $35^\circ 15'$ we find

$c = 10$ gives $l = 8.267$, $d = 5.509$

$c = 7$ gives $l = 5.72$, $d = 4.04$

$c = .8$ gives $l = .65$, $d = .46$

$c = .05$ gives $l = .04$, $d = .03$

$c = 17.85$ gives $l = 30.08$, $d = 27.02$

S. N.

The l and d for 40 are found from the l and d of 4, as given in the table, by multiplying by 10, or removing the decimal point one place to the right.

The l and d for the distance 7 are given in the table, but the right hand figure is dropped, and 1 is carried if the figure dropped exceeds 5.

The l and d for the distance .8 are found from the l and d for the distance 8 by removing the decimal point one place to the left, rejecting the figures at the right of the second decimal place, carrying as above.

For the distance .05, remove the decimal point two places to the left, reject and carry as before.

If the bearing exceeds 45° , the l and d will be found in columns marked at the bottom of the page.

291. Examples.

1. Given $b = N. 28^\circ 45' E.$, and $c = 5.35$ ch.; required l and d .
Ans. $l = 30.98$ ch. N., $d = 17$ ch. E.

2. Given $b = S. 36\frac{1}{2}^\circ E.$ and $c = 12.76$ ch.; required l and d .
Ans. $l = 15.51$ ch. S., $d = 11.59$ ch. E.

3. Given $b = N. 53^\circ 15' E.$, $c = 11.60$ ch.; required l and d .
Ans. $l = 6.94$ ch. N. $d = 9.29$ ch. E.

4. Given $b = S. 74\frac{1}{2}^\circ E.$, $c = 20.95$ ch.; required l and d .
Ans. $l = 8.27$ ch. S. $d = 20.83$ ch. E.

5. Given $b = N. 33\frac{1}{2}^\circ W.$, $c = 37$ ch.; required l and d .
Ans. $l = 30.91$ ch. N., $d = 20.29$ ch. W.

6. Find the l and d of the sides of a lot of which the following are the field notes: Commencing at the most westerly station, and running thence $N. 52^\circ E.$, 21.28 ch.; thence $S. 20\frac{1}{2}^\circ E.$, 8.18 ch.; thence $S. 31\frac{1}{2}^\circ W.$, 15.36 ch.; thence $N. 61^\circ W.$, 11.18 ch., to the point of beginning.

The work is written thus:

<i>Sta.</i>	<i>Bearings.</i>	<i>Dist.</i>	<i>N. Lat.</i>	<i>S. Lat.</i>	<i>E. Dep.</i>	<i>W. Dep.</i>
1	N. 52° E.	21.28	13.10		16.77	
2	S. $20\frac{1}{2}^\circ$ E.	8.18		7.11	4.06	
3	S. $31\frac{1}{2}^\circ$ W.	15.36		13.06		8.48
4	N. 61° W.	11.18	7.92			12.67

292. Balancing the Work.

It is evident that in passing around a field to the point of beginning, we have gone just as far north as south, and just as far east as west. Hence the sum of the northings should be equal to the sum of the southings, and the sum of the eastings to the sum of the westings.

In practice, however, this is seldom the case, owing to the fact that the bearings are taken only to quarter degrees, and that the chaining is not perfectly correct.

It is not a settled point among surveyors how great an error in latitude or departure can be allowed without resurveying the lot. Some would admit an error of 1 link for every 10 chains in the sum of the courses; others, 1 link for every 3 chains. Each surveyor must settle this point for himself by ascertaining, by experience, how nearly he can make his work balance.

When an error is as likely to occur in one course as in another, the errors of latitude and departure are distributed among the courses in proportion to their length.

It will not, in general, be necessary to make all the proportions, for after making one for latitude and one for departure, the remaining corrections can be made by a comparison of distances.

Let us take example 6 of the last article.

No.	Bearing	Lat.	N Lat.	S Lat.	E Dep.	W Dep.	N L.	S L.	E D.	W D.
1	N 82° E	21.28	13.10		16.77		13.12		16.74	
2	S 29° E	8.18		7.11	4.06			7.10	4.05	
3	S 31° W	15.36		13.06		8.08		13.05		8.10
4	N 61° W	14.48	7.02		12.67	7.03			12.66	

59 30 20 12 20 17 20 83 20 75 20 15 20 15 20 79 20 79

Error in Lat. 20.17 — 20.12 .05.

Error in Dep. = 20.83 — 20.75 .08.

Corrections for Latitude.

Corrections for Departure.

59 30 : 21.28 :: .05 : .02

59 30 : 21.28 :: .08 : .03

59 30 : 8.18 :: .05 : .01

59 30 : 8.18 :: .08 : .01

59 30 : 15.36 :: .05 : .01

59 30 : 15.36 :: .08 : .02

59 30 : 14.48 :: .05 : .01

59 30 : 14.48 :: .08 : .02

The corrections are made to the nearest link or hundredth.

Since the north latitude is too small, and the south latitude too great, add to each north latitude the corresponding correction, and subtract from the south latitude. In a similar manner correct the departure.

If one side is much more difficult to measure than the remaining sides, it is to be presumed that the error occurred chiefly in measuring that side, and the corrections should be made accordingly.

If, in taking one bearing, the object could not be distinctly seen, the error probably occurred in that bearing; then correct mainly in the latitude and departure of that course.

In practice it will not be necessary to make additional columns for the corrected latitude and departure, since they may be written in the same columns, over the others, with different colored ink.

293. Examples.

1. Find the l and d , and balance the work from the following notes:

1st, N. $34\frac{1}{2}^\circ$ E., 8.19 ch.; 2d, N. 85° E., 3.84 ch.; 3d, S. $56\frac{1}{2}^\circ$ E., 6.60 ch.; 4th, S. $34\frac{1}{2}^\circ$ W., 10.59 ch.; 5th, N. 56° W., 9.60 ch.

2. Find the l and d , and balance the work from the following notes:

1st, N. 5° E., 22.50 ch.; 2d, S. 83° E., 12.96 ch.; 3d, N. 50° E., 19.20 ch.; 4th, S. 32° E., 32.76 ch.; 5th, S. 41° W., 12.60 ch.; 6th, W., 16.86 ch.; 7th, N. 79° W., 21.84 ch.

3. Find the balanced l and d of the following:

1st, N. 30° E., 10 ch.; 2d, N. 60° E., 18.18 ch.; 3d, S. 10° E., 20.10 ch.; 4th, S. 30° W., 24.50 ch.; 5th, W., 15 ch.; 6th, N. $18\frac{1}{2}^\circ$ W., 19.92 ch.

294. Double Meridian Distance.

The double meridian distance of a course is double the distance of its middle point from a given meridian.

Let AB be a given course, NS the given meridian, P the middle point of AB , PQ perpendicular to NS .

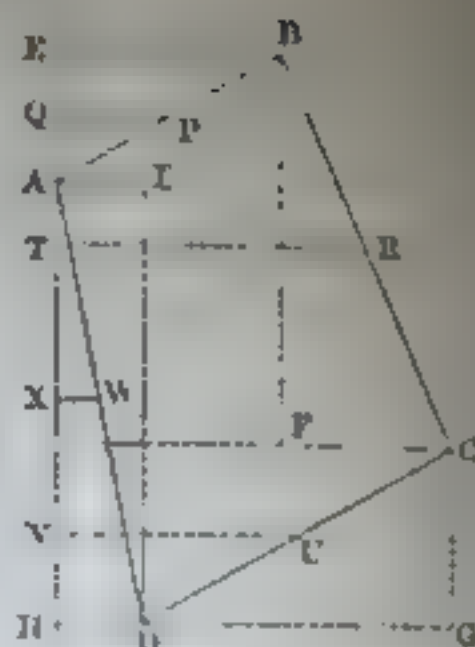
Then will $2QP$ be the double meridian distance of AB .

In the following illustration we shall assume that the meridian of reference passes through the most westerly station, which we shall call the principal station, that departures east are plus, and west, minus, that the lines were run in the direction

ABCD, so as to keep the field on the right.

The following relations can be verified from the diagram:

1. $2QP = EB$.
2. $2TR = 2QP + EB + FC$.
3. $2VU = 2TR + FC + (-GD)$.
4. $2XW = 2VU + (-GD) + (-IA) = AI$.



1. The double meridian distance of the first course is equal to its departure.

2. The double meridian distance of the second course is equal to the double meridian distance of the first course, plus the departure of the first course, plus the departure of the second course.

3. The double meridian distance of any course is equal to the double meridian distance of the preceding course, plus the departure of that course, plus the departure of the given course.

4. The double meridian distance of the last course is equal to its departure with its sign changed.

Take the example of a preceding article, as balanced.

Sta	Bearings	Dist.	N.Lat.	S.Lat.	E.Dep.	W.Dep.	DMD.
1	N. 52° E.	21.28	13.12		16.74		16.74
2	S. 29½° E.	8.18		7.10	4.05		37.53
3	S. 31½° W.	15.36		13.05		8.10	33.48
4	N. 61° W.	11.18	7.03			12.69	12.69

Dep. of 1st course = 16.74 = D.M.D. of 1st course.
 + dep. of 1st course = 16.74
 + dep. of 2d course = 4.05
 37.53 = D.M.D. of 2d course.

+ dep. of 2d course = 4.05
 41.58
 + dep. of 3d course = 8.10
 33.48 = D.M.D. of 3d course.
 + dep. of 3d course = 8.10
 25.38
 + dep. of 4th course = 12.69
 12.69 = D.M.D. of 4th course.

The principal or most westerly station is not always the first station in the field notes.

It will be observed that the word *plus*, in the above principles and illustrations, is used in the algebraic sense, that east departure is considered *plus* and west departure *minus*; that plus, an east departure, is a plus quantity, and plus a west departure a minus quantity; and that the double meridian distance of the last course is equal to its departure with its sign changed, which will serve as a verification of the work.

The first station of the notes, in the preceding example, is the most westerly, and was therefore taken for the principal station.

The most westerly station can readily be determined by inspecting the bearings of the courses as given in the field notes, and should be taken as the principal station, and the corresponding course as the first course in the double meridian distances.

295. Examples

1. Given the following field notes:

1st, N. 30° E., 10 ch.; 2d, N. 60° E., 18.18 ch.; 3d, S. 40° E., 20.10 ch.; 4th, S. 30° W., 24.50 ch.; 5th, W., 15 ch.; 6th, N. 18° 45' W., 19.92 ch. Required the

latitude and departure; balance the work, and find the double meridian distances.

2. Given the following field notes:

1st, N. 45° W., 20 ch.; 2d, N. 18° E, 12.25 ch.; 3d, E., 12.80 ch.; 4th, N. 32° E, 6.50 ch.; 5th, S. $42\frac{1}{2}^{\circ}$ E., 13.20 ch.; 6th, S., 14.75 ch.; 7th, S. $65\frac{1}{4}^{\circ}$ W., 16.30 ch. Required the corrected latitude and departure, and the double meridian distances.

AREA OF LAND.

296. Table of Linear Measure.

Mi.	Ch.	Rds.	Yds.	Ft.	Lk.	In.
1 =	80 =	320 =	1760 =	5280 =	8000 =	63360.
	1 =	4 =	22 =	66 =	100 =	792.
		1 =	$5\frac{1}{2}$ =	$16\frac{1}{2}$ =	25 =	198.
			1 =	3 =	$4\frac{1}{4}$ =	36.
				1 =	$1\frac{1}{4}$ =	12.
					1 =	$7\frac{1}{8}$.

297. Table of Superficial Measure.

Mile.	Acres.	Roods.	Chains.	Perches.	Links.
1 =	640 =	2560 =	6400 =	102400 =	64000000.
	1 =	4 =	10 =	160 =	100000.
		1 =	$2\frac{1}{2}$ =	40 =	25000.
			1 =	16 =	10000.
				1 =	625.

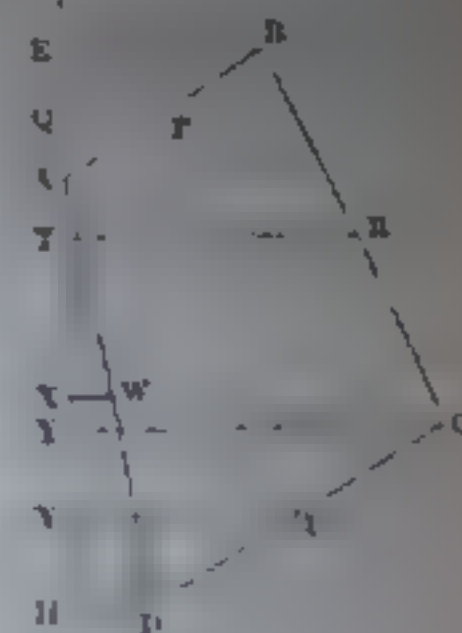
Note 1.—It should be remembered that in finding the area of a tract of land the inequalities of its surface are not considered, but the tract is treated as a horizontal plane.

Note 2.—The area of a portion of land can, in a great variety of cases, be calculated by the rules already given for *Mensuration of Plane Surfaces*.

298. Problem.

To find the area of a tract of land when the length and direction of the bounding lines are given.

It is evident from the diagram that the area of $ABCD$ is equal to the sum of the trapezoids $EBCY$ and $YCDH$, minus the sum of the triangles AEB and ADH ; and that twice the sum of the trapezoids, minus twice the sum of the triangles, is equal to twice $ABCD$.



The following table will exhibit the general form of operation:

No.	Course	N. Lat.	S. Lat.	DMD	Triangle	Trapezoid
1	AB	AF		2QP	$2QP \cdot AF$	
2	BC		EY	2TR		$2TR \cdot EY$
3	CD		YH	2VU		$2VU \cdot YH$
4	DA	HA		2XB	$2XB \cdot HA$	

It will be observed that we have taken the most westerly station for the principal station, and have multiplied the double meridian distance of each course by its latitude, and that the product is double the area of a triangle when the latitude is north, and double the area of a trapezoid when the latitude is south.

If we had taken the most easterly station for the principal station, the reverse would be true.

In the above we have supposed that the lines were run in such direction as to keep the lot at the right.

If the lines were run in the opposite direction, so as to keep the lot at the left, the reverse would be true.

In any case, the sum of the double areas of the trapezoids, minus the sum of the double areas of the triangles, is equal to double the area required.

299. Rule.

Multiply the double meridian distance of each course by its latitude, placing the product in one column when the latitude is north, and in another column when the latitude is south, and divide the difference of the sums of the two columns by 2, and the quotient will be the area required.

Take the example of a preceding article whose D. M. D.'s have been found

Sta.	Bearings.	Dist.	N. Lat.	S. Lat.	E. Dep.	W. Dep.	D. M. D.	Triang.	Trap.
1	N. 52° E.	21.28	13.12		16.74			4 219.6288	
2	S. 29° E.	8.18		7.10	4.05				266.4630
3	S. 31° W.	15.36		13.05		8			136.9140
4	N. 61° W.	14.48	7.03			12.69	12.69	89.2107	

Area = 19 A. 2 R. 36 P.

Triangles	Trapezoids
16.74 × 13.12 = 219.6288	7.10 × 7.10 = 266.4630
12.69 × 7.03 = 89.2107	13.05 × 13.05 = 418.9140

Divide double the area by 2, the result by 10 to reduce the chains to acres, multiply the decimal by 4 to reduce to rods, and the next decimal by 10 to reduce to perches.

300. Plotting.

Plotting is the process of representing, to a given scale, the length, direction, and relative position of the bounding lines of a tract of land.

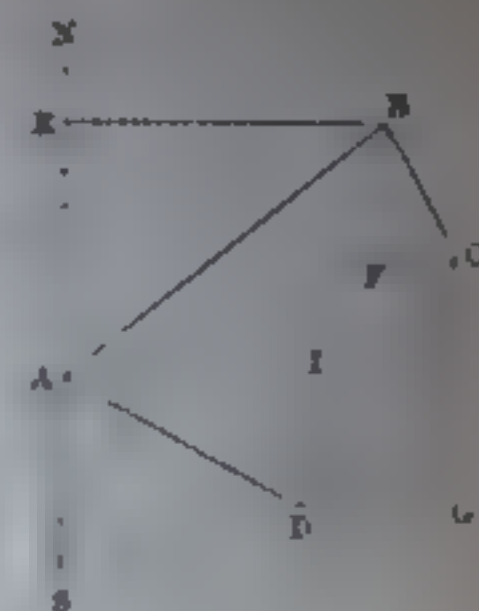
1st Method.—By means of latitudes and departures.

Take the example of the last article.

Let NS represent the meridian passing through the principal station A.

Select a scale whose unit shall represent 1 ch., and take AE = 13.12 ch., the lat. of first course.

Through E draw a line perpendicular to NS; take EB = 16.74 ch., the dep. of first course, and draw AB.



Through B draw a meridian, and take BF = 7.10, the lat. of second course.

Through F draw a line perpendicular to BF, take FC = 4.05 ch., the dep. of second course, and draw BC.

Through C draw a meridian, and take CG = 13.05, the lat. of third course.

Through G draw a line perpendicular to CG, and take GD = 8 ch., the dep. of third course, and draw CD.

Through D draw a meridian, and take DI = 7.03 ch., the lat. of fourth course.

Through I draw a line perpendicular to DI, take ID = 12.69 ch., the dep. of fourth course, and draw DA.

Remark 1.—If the departure of fourth course terminates at A, the work will be verified.

2. It will be observed that N. lat. is laid off upward, S. lat. downward, E. dep. to the right, and W. dep. to the left.

3. The auxiliary lines can be drawn with a pencil and afterward erased.

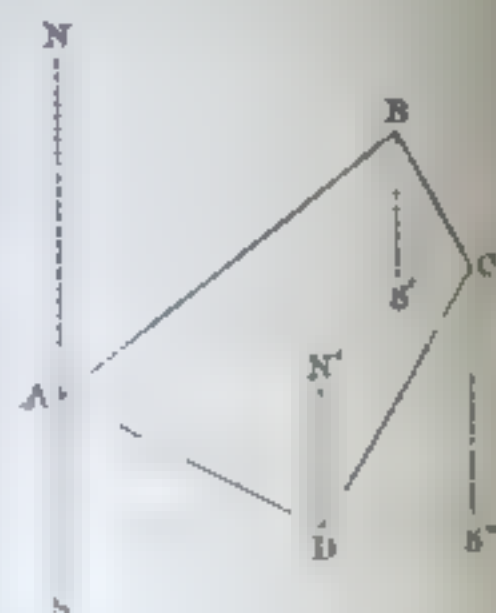
4. If every scale in possession of the surveyor should make the diagram too large or too small, all the latitudes and departures can be divided or multiplied by the same number, and the results taken instead of the given latitudes and departures.

2d Method.—By means of bearings and distances.

Take the same example.

Let NS represent the meridian passing through the principal station A .

With a protractor lay off the angle $NAB = 52^\circ$, the bearing of first course, and take $AB = 21.28$ ch., the first course.



Through B draw a meridian and lay off $S'BC = 29\frac{1}{2}^\circ$, the bearing of second course, and take $BC = 8.18$ ch., the second course.

Through C draw a meridian, and lay off $S''CD = 31\frac{1}{2}^\circ$, the bearing of third course, and take $CD = 15.36$ ch., the third course.

Through D draw a meridian, and lay off $N'''DA = 61^\circ$, the bearing of fourth course, and take $DA = 14.18$ ch., the fourth course, which will terminate at A if the work is correct.

Remark 1.—The latitude and departure letters indicate the general direction of the lines, and the degrees the exact direction.

2. Let the examples of the following article be carefully plotted, and the area be found.

3. By a careful inspection of the bearings, the most westerly station can be found, which take for the principal station.

4. The distances are all given in chains.

301. Examples.

1.

No.	Bearings.	Dist.
1	N. 30° E.	10
2	N. 60° E.	18.18
3	S. 40° E.	20.10
4	S. 30° W.	21.50
5	W.	15
6	N. $48\frac{1}{2}^\circ$ W.	19.92
Ans. 80 A. 1 R. 25 P.		

2.

No.	Bearings.	Dist.
1	N. 47° E.	15.65
2	S. 57° E.	16.55
3	S. $28\frac{1}{2}^\circ$ W.	17.67
4	S. $29\frac{1}{2}^\circ$ W.	1.11
5	S. 54° W.	1.04
6	N. $40\frac{1}{2}^\circ$ W.	15.80
Ans. 25 A. 0 R. 38 P.		

3.

No.	Bearings.	Dist.
1	N. 45° W.	20
2	N. 18° E.	12.25
3	E.	12.80
4	N. 32° E.	6.50
5	S. $42\frac{1}{2}^\circ$ E.	13.20
6	S.	14.75
7	S. $65\frac{1}{2}^\circ$ W.	16.30
Ans. 58 A. 3 R. 30 P.		

4.

No.	Bearings.	Dist.
1	N. 58° E.	12.97
2	S. $27\frac{1}{2}^\circ$ E.	3.20
3	S. $83\frac{1}{2}^\circ$ E.	11.65
4	S. 19° E.	15.56
5	S. $64\frac{1}{2}^\circ$ W.	14.03
6	N. 64° W.	14.86
7	N. $15\frac{1}{2}^\circ$ W.	11.23
Ans. 45 A. 2 R. 5 P.		

5.

Sta.	Bearings.	Dist.
1	N. 20° E.	12.20
2	N. 70° E.	15.50
3	E.	18.25
4	S. 45° E.	20.00
5	S.	20.00
6	S. 45° W.	20.00
7	W.	18.25
8	N. 30½° W.	36.66

Ans. 188 A. 3 R. 20 P.

6.

Sta.	Bearings.	Dist.
1	S. 34° E.	4.56
2	S. 66½° W.	13.84
3	N. 12½° E.	12.15
4	N. 48½° W.	12.30
5	N. 58½° E.	9.92
6	N. 39½° E.	5.22
7	S. 45½° E.	18.63
8	S. 52½° W.	10.76

Ans. 32 A. 2 R. 26 P.

7.

Sta.	Bearings.	Dist.
1	N. 30° E.	15.
2	N. 60° E.	15.
3	E.	15.
4	S. 60° E.	15.
5	S. 30° E.	15.
6	S.	15.
7	S. 30° W.	15.
8	S. 60° W.	15.
9	W.	15.
10	N. 60° W.	15.
11	N. 30° W.	15.
12	N.	15.

Ans. 251.9 A.

8.

Sta.	Bearings.	Dist.
1	S. 76½° E.	6.69
2	S. 11½° W.	5.96
3	S. 38° E.	9.82
4	N. 30½° E.	8.63
5	S. 70½° E.	9.43
6	S. 1° W.	15.70
7	N. 12½° W.	13.06
8	N. 61° W.	11.93
9	S. 70° W.	10.45
10	N. 22° W.	11.60
11	N. 37° E.	14.37
12	N. 22° E.	10.79

Ans. 76.11 A.

302. Problem.

To find the area when offsets are taken.

Find the area of the tract of land bounded by the full lines and middle of the river, as shown in the annexed diagram



Having run the stationary line *CD*, we have the following notes.

For *ABCDE*.

Sta.	Bearings.	Dist.
1	N. 20° E.	15.50
2	E.	18.00
3	S. 20° E.	30.00
4	W.	25.00
5	N. 32½° W.	16.00

Area 70 A 1 R 33 P + 14 A 3 R 8 P = 84 A 1 R 41 P

We find, as in the last article, *ABCDE* = 70 A 1 R. 33 P.

To find the area included between the stationary line *CD* and the line passing along the middle of the river, we find *Ch* = 7, *ab* = *Cb* - *Ch* = 12.20 - 7 = 5.20, etc., which gives the altitudes of the trapezoids. The parallel sides are given under the head of offsets.

The altitude of a trapezoid multiplied by the sum of the parallel sides will give twice its area.

The calculation is made as in the annexed table, the letters, *S*, *N*, *P*, *O*, *I*, *D*, *S*, *O*, *P*, *T*, *A*, *R*, *P*.

For *Offsets*.

Sta.	Dist.	Offset
1	0.00	2.50
2	7.00	6.00
3	12.20	4.00
4	22.25	7.00
5	38.00	2.50

columns of the table, denoting stations, station distances or distances from C, offsets, intercepted distances, sum of offsets, and double trapezoids.

S.	S. D.	O.	I. D.	S. O.	D. T.
1	0.00	2.50			
2	7.00	6.00	7.00	8.50	59.5000
3	12.20	4.00	5.20	10.00	52.0000
4	22.25	7.00	10.05	11.00	110.5500
5	30.00	2.55	7.75	9.55	74.0125

Area, 14 A. 8 R. 8 P.

2) 296.0625

10) 148.03125

14.803125

4

3.212500

40

8.500000

If the offsets fall within the stationary line, the sum of the trapezoids must be subtracted.

In general, if the lines are run so as to keep the field on the right, the sum of the trapezoids must be added in case of left-hand offsets, and subtracted in case of right-hand offsets.

In case of navigable rivers, the bank is in general, the boundary—the first and last offsets become 0, and the first and last trapezoids become triangles, but the form of the computation is the same.

303. Examples.

1. Find the area of the lot of which the following are the field notes, and make a plot of the survey.

Rectilinear Area.			L.H. Offsets.*		R.H. Offsets.**	
Sta.	Bearings.	Dist.	S. Dist.	Offsets	S. Dist.	Offsets
1	N. 45° E.	10.00	0.00	1.00	0.00	1.10
2	N.	10.00	6.50	4.25	5.62	4.00
3	N. 45° E.	10.00	12.50	2.43	12.62	5.27
4	E.	10.00	17.50	5.17	17.07	1.13
5*	S.	31.21	26.21	5.83		
6**	W.	17.07	31.21	1.25		
7	N. 45° W.	10.00				

55.774715 A. + 12.17075 A. = 67.945465 A. = 61 A. 3 R. 15 P.

The left-hand offsets were made from the fifth course, as indicated by the single star, and the right-hand offsets from the sixth course, as indicated by the double star.

2. Find the area of the lot of which the following are the field notes, and make a plot of the survey.

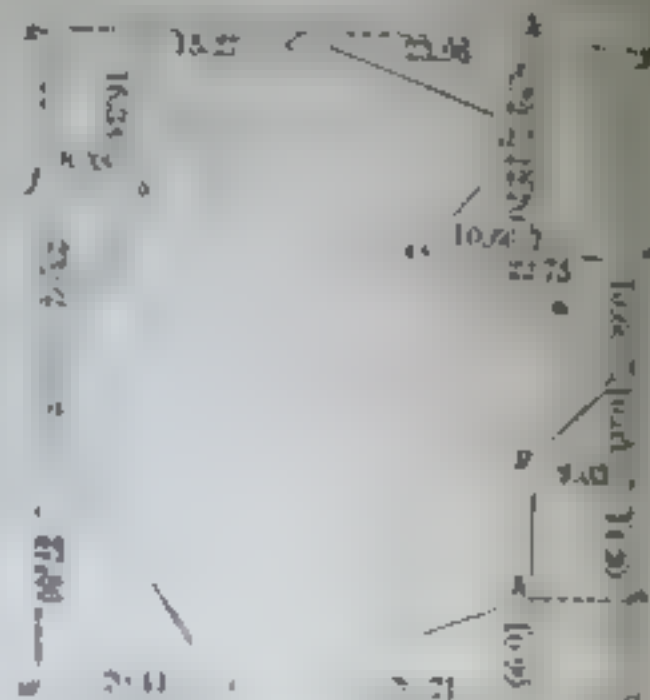
Rectilinear Area.			L.H. Offsets.*		R.H. Offsets.**	
No.	Bearings.	Dist.	S. Dist.	Offsets	S. Dist.	Offsets
1	N. 30° E.	20	0.00	0.00	0.00	0.00
2	E.	20	6.00	3.00	6.00	4.00
3*	S. 30° E.	20	10.00	2.00	14.00	4.00
4**	S. 30° W.	20	15.00	3.50	20.00	0.00
5	W.	20	20.00	0.00		
6	N. 30° W.	20				

Ans. 102 A. 1 R. 36 P.

304. Pogue's Method of Finding the Area.

This method is illustrated by the following example:

1	N. 20° E.,	24.50 ch.
2	N. 43° E.,	22.40 ch.
3	S. 70° E.,	25.50 ch.
4	S. 40° W.,	16.58 ch.
5	S. 65° E.,	25.10 ch.
6	S. 42° W.,	13.50 ch.
7	S.,	14.20 ch.
8	S. 70° W.,	32.15 ch.
9	N. 36½° W.,	34.55 ch.



Make a plot from the field notes, draw meridians through the most easterly and westerly stations, and parallels of latitude through the most northerly and southerly, thus enclosing the whole figure in a rectangle.

Find, from the traverse table, the latitudes and departures as in diagram.

To find xy , pass from the most westerly station, round the north, to the most easterly, taking the sum of the eastings minus the sum of the westings; and to find zr , pass from the most easterly station, round the south, to the most westerly, taking the sum of the westings minus the sum of the eastings, thus:

$$\begin{aligned} xy &= 8.38 + 15.27 + 23.96 - 10.66 + 22.75 = 59.70 \\ zr &= 9.03 + 30.21 + 20.11 = 59.35 \\ \frac{1}{2}(xy + zr) &= \text{the average width} = 59.53 \end{aligned}$$

To find ux , pass from the most southerly station, round the west, to the most northerly, taking the sum of the northings minus the sum of the southings; and to find

yz , pass from the most northerly station, round the east, to the most southerly, taking the sum of the southings minus the sum of the northings, thus:

$$\begin{aligned} ux &= 27.86 + 23.02 + 16.38 = 67.26 \\ yz &= 8.72 + 12.70 + 10.60 + 10.03 + 14.20 + 10.99 = 67.24 \\ \frac{1}{2}(ux + yz) &= \text{the average altitude} = 67.25 \end{aligned}$$

$$\text{Area of rectangle} = 59.69 \times 67.25 = 4014.1525.$$

From the area of the rectangle we must deduct the area included between $uxyz$ and $abedefgha$, thus found:

$$\begin{aligned} abj &= \frac{23.02 \times 8.38}{2} = 96.4538 \\ bjxc &= \frac{8.38 + 8.38 + 15.27}{2} \times 16.38 = 222.3257 \\ ckd &= \frac{23.96 \times 8.72}{2} = 104.4656 \\ del &= \frac{12.70 \times 10.66}{2} = 67.0210 \\ kymf &= \frac{(8.72 + 12.70)(22.75 - 10.66)}{2} = 258.9678 \\ fuhq &= \frac{10.03 + 14.20 + 14.20}{2} \times 9.03 = 173.5114 \\ hoi &= \frac{9.03 + 9.03 + 30.21}{2} \times 10.99 = 265.2436 \\ iaa &= \frac{20.44 \times 27.86}{2} = 284.7292 \\ \text{Total} &= 1633.9631 \end{aligned}$$

$$\begin{aligned} abedefgha &= 4014.1525 \text{ sq. ch.} - 1633.9631 \text{ sq. ch.} \\ &= 2380.1894 \text{ sq. ch.} = 238.02 \text{ A.} \end{aligned}$$

For additional exercises, work the examples of articles 301 and 303, and compare the answers obtained by the two methods.

SUPPLYING OMISSIONS.

305. Case I.

When the bearing and length of one side are wanting.

The wanting side must be such that its latitude and departure will make the work balance. Hence, its latitude must be the difference between the sum of the northings and the sum of the southings of the given sides, and of the same name as the less; and its departure must be the difference between the sum of the eastings and the sum of the westings of the given sides, and of the same name as the less.

Having found the latitude and departure of the wanting side, construct a right-angle triangle by drawing on the paper, to represent the latitude, a line, up or down, according as the latitude is north or south; and at the terminus of the line, draw, to represent the departure, a horizontal line, to the right or left, according as the departure is east or west, and join the origin of the line representing the latitude with the terminus of the line representing the departure, and this last line will be the hypotenuse which will represent the course or length of the line sought, and the angle which it makes with the vertical line will be the bearing.

Denote the latitude by l , the departure by d , the course by c , and the bearing by b , then we have,

$$(1) \quad c = \sqrt{l^2 + d^2}. \quad (2) \quad \tan b = \frac{d}{l}.$$

Having found the bearing and distance, enter them in the notes and find the area.



306. Examples.

Supply the omissions in the following field notes, calculate the areas, and plot the surveys.

1.			2.		
No.	Bearings.	Dist.	No.	Bearings.	Dist.
1	N. 18° E.	9.25	1	N. 24° W.	15.50
2	N. 71° E.	8.33	2	N. 31° E.	17.07
3	S. $43\frac{1}{2}^\circ$ E.	12.37	3	E.	20.
4	S. $36\frac{1}{2}^\circ$ W.	16.00	4	Want'g.	Want'g.
5	Want'g.	Want'g.	5	S. 56° W.	30.50
(N. 43° W., 14.18 ch.)			(S. $12\frac{1}{2}^\circ$ E., 12.15 ch.)		
Area (23 A. 3 R. 32 P.)			Area (56 A. 3 R. 0 P.)		

307. Case II.

When the lengths of two sides are wanting.

Revolve the field so that one of the sides whose bearing only is given shall become a meridian, and find, by article 285, the bearings of all the sides in their new position.

The departure of the side made a meridian will then be 0, and the difference of the sums of the columns of the departures will be the departure, in the new position, of the other side whose distance is wanting.

Knowing the bearing and departure of this side, we can find its distance and latitude. Then the difference between the sums of the columns of latitudes will be the length of the side made a meridian.

Revolve the field to its original position, calculate its area, and make a plot of it, or if the area only

is required after supplying omissions, it may be computed more readily without revolving the field to its original position.

308. Examples.

1.			2.		
Sta.	Bearings.	Dist.	Sta.	Bearings.	Dist.
1	N. 30° E.	10.00	1	N. 47° E.	15.65
2	N. 60° E.	18.18	2	S. 57° E.	10.55
3	S. 40° E.	Want'g	3	S. 28½° W.	Want'g
4	S. 30° W.	Want'g	4	S. 29½° W.	1.11
5	W.	15.00	5	S. 51° W.	1.04
6	N. 18½° W.	19.92	6	N. 40½° W.	Want'g
Ans. { 3d. 20.08 ch. 4th. 24.52 ch. 80 A. 1 R. 25 P.			Ans. { 3d. 17.69 ch. 6th. 16.01 ch. 23 A. 1 R. 14 P.		

309. Case III.

When the bearings of two sides are wanting.

If the sides whose bearings are wanting are separated from each other by one or more bearing sides, suppose one of these sides and a side adjacent to the other to change places, so as to bring the sides under consideration together without changing their bearings or lengths of the sides transposed.

Then, throwing these sides out of consideration, find, by Case I, the bearing and length of the line joining the extremities of the sides whose bearings are wanting.

This line with the sides form a triangle, whose sides are known, from which the angles can be computed.

Knowing the angles and the bearing of one side, the bearings of the other sides can be found.

Restore to their original position the sides which have changed places, if such is the fact, calculate the area, and make a plot of the field.

310. Examples.

1.			2.		
Sta.	Bearings.	Dist.	Sta.	Bearings.	Dist.
1	N. 45° W.	20.00	1	N. 58° E.	12.97
2	N. 18° E.	12.25	2	S. 27½° E.	3.50
3	E.	12.80	3	S. 83½° E.	11.65
4	N. 32° E.	6.50	4	S. 19° E.	15.56
5	S. 42½° E.	13.20	5	Wanting	14.63
6	Wanting	14.75	6	N. 64° W.	14.86
7	Wanting	16.30	7	Wanting	11.23
Ans. { 6th. S 7th. S. 65½° W. 59 A. 3 R. 30 P.			Ans. { 5th. S. 62½° W. 7th. N. 15½° W. 45 A. 2 R. 5 P.		

311. Case IV.

When the bearing of one side and the length of another are wanting.

Revolve the field so that the side whose bearing only is given shall become a meridian.

The departure of this side will then be 0, and the difference of the sums of the columns of departures will be the departure, in its new position, of the side whose bearing is wanting.

Knowing the length and departure of this side, its bearing and latitude can be found.

Then, the difference of the sums of the columns of latitudes will be the latitude of the side made a meridian.

Revolve the field to its original position, compute the area and plot the work.

Remark 1. In finding the bearing of the side whose distance only is given, though the angle can be readily found, the bearing, and consequently the latitude, may be either north or south, since either will comply with the condition. The length of the side whose bearing only is given will therefore be ambiguous, and there will be two solutions to the problem. If but one solution is admissible, the omission should be supplied by a remeasurement; and if the lost bearing or distance can not be taken directly, auxiliary lines may be run, and the omissions supplied by Trigonometry.

2. From the fact that two omissions can be supplied, the surveyor should not deem it unimportant to find all the measurements on the ground, since thus he can ascertain the correctness of his notes by balancing his work—a test not applicable when omissions are supplied.

312. Examples.

1.			2.		
Sta.	Bearings.	Dist.	Sta.	Bearings.	Dist.
1	N. 20° E.	12 20	1	S. 34° E.	4 56
2	N. 70° E.	15 50	2	S. 66½° W.	13 84
3	E.	18 25	3	N. 14° E.	12 45
4	S. 45° E.	20 00	4	Wanting	12 30
5	S.	20 00	5	N. 8½° E.	9 92
6	Wanting.	20 00	6	N. 50° E.	5 22
7	W.	Wanting	7	S. 14½° E.	Wanting.
8	N. 30½° W.	16 00	8	S. 52° W.	10 76

Ans. { 6th. S. 45° W.
7th. 18.25.
188 A. 3 R. 20 P.

Ans. { 4th. N. 18½° W.
7th. 18.64.
32 A. 2 R. 26 P.

LAYING OUT LAND.

313. Laying out Squares.

To lay out a given quantity of land in the form of a square.

Let a be the area of the square, and x one side.

$$\text{Then, } x^2 = a, \therefore x = \sqrt{a}$$

Reduce the given area to square chains, extract the square root, and the result will be the length of one side.

With the chain and transit lay out the square on the ground.

EXAMPLES.

1. Lay out 12 A. 3 R. 20 P. in the form of a square
2. Find the side of a square containing 1 A., and lay out the square on the ground.

314. Laying out Rectangles.

1. *To lay out a given quantity of land in the form of a rectangle, one side of which is given.*

Let a be the area of the rectangle, b the given side, and x an adjacent side

$$\text{Then, } bx = a, \therefore x = \frac{a}{b}$$

2. *To lay out a given quantity of land in the form of a rectangle whose length is to its breadth in a given ratio*

Let a denote the area of the rectangle, x its length, y its breadth, and $m : n$ the ratio of x to y

$$\text{Then, } \begin{cases} xy = a \\ x = y \cdot m : n \end{cases} \therefore \begin{cases} y = \sqrt{\frac{a \cdot n}{m}} \\ x = \sqrt{\frac{a \cdot m}{n}} \end{cases}$$

3. To lay out a given quantity of land in the form of a rectangle when the sum of its length and breadth is given.

Let a be the area of the rectangle, x the length, y the breadth, and s the sum of x and y .

$$\text{Then, } \begin{cases} x + y = s \\ xy = a \end{cases} \therefore \begin{cases} x = \frac{1}{2}s + \frac{1}{2}\sqrt{s^2 - 4a} \\ y = \frac{1}{2}s - \frac{1}{2}\sqrt{s^2 - 4a} \end{cases}$$

4. To lay out a given quantity of land in the form of a rectangle when the difference of the length and breadth is given.

Let a denote the area of the rectangle, x its length, y its breadth, and d the difference of x and y .

$$\text{Then, } \begin{cases} x - y = d \\ xy = a \end{cases} \therefore \begin{cases} x = \frac{1}{2}(\sqrt{d^2 + 4a} + d) \\ y = \frac{1}{2}(\sqrt{d^2 + 4a} - d) \end{cases}$$

315. Examples.

1. The area of a rectangle is 3 A., one side is 4 ch. Find an adjacent side and lay out the rectangle.

2. The area of a rectangle is 8 A.; the length is to the breadth as 3 is to 2. Find the sides and lay out the rectangle. *Ans.* 10.95 ch. and 7.30 ch.

3. The area of a rectangle is 48 A.; the sum of the length and breadth is 14 ch. Find the sides and lay out the rectangle. *Ans.* 8 ch. and 6 ch.

4. The area of a rectangle is 18 A.; the difference of the length and breadth is 3 ch. Find the sides and lay out the rectangle. *Ans.* 15 ch. and 12 ch.

316. Laying out Parallelograms.

1. To lay out a given quantity of land in the form of a parallelogram when the base is given.

Let a be the area, b the base, and x the altitude.

$$\text{Then } bx = a, \therefore x = \frac{a}{b}.$$

Measure the base, from any point of which erect a perpendicular equal to the calculated altitude.

Through the extremity of the perpendicular run a line parallel to the base, any point of which may be taken for one extremity of the upper base, which may then be measured off on this line.

2. When one side and an adjacent angle are given.

Let a be the area, b the given side, A the given angle, and x the other side adjacent to this angle.

$$\text{Then } bx \sin A = a, \therefore x = \frac{a}{b \sin A}.$$

3. When two adjacent sides are given.

Let a be the area, b and c the given sides, and x their included angle.

$$\text{Then } bc \sin x = a, \therefore \sin x = \frac{a}{bc}.$$

Remark.—If $bc = a$, then $\sin x = 1$, $x = 90^\circ$, and the parallelogram becomes a rectangle.

If $bc < a$, the solution is impossible.

317. Examples.

1. The area of a parallelogram is 6 A., the base is 6 ch. Find the altitude and lay out the land.

2. The area of a parallelogram is 12 A., one side is 12 ch., and an adjacent angle is 60° . Find the other side adjacent to the given angle and lay out the land.

3. The area of a parallelogram is 8 A, two adjacent sides are 8 ch. and 12 ch. Find their included angle and lay out the land.

318. Laying out Triangles.

1. To lay out a given quantity of land in the form of a triangle when the base is given.

Let a denote the area, b the base, and x the altitude.

$$\text{Then, } \frac{1}{2}bx = a, \therefore x = \frac{2a}{b}.$$

Measure the base, at any point of which erect a perpendicular equal to the calculated altitude.

Through the extremity of this perpendicular draw a line parallel to the base. This parallel will be the locus of the vertex, any point of which may be taken for the vertex.

2. When the base is to the altitude in a given ratio.

Let a denote the area, x the base, y the altitude, and $m:n$ the ratio of the base to the altitude.

$$\text{Then, } \left\{ \begin{array}{l} \frac{1}{2}xy = a. \\ x:y::m:n. \end{array} \right\} \therefore \left\{ \begin{array}{l} \sqrt{\frac{2am}{n}}. \\ \sqrt{\frac{2an}{m}}. \end{array} \right.$$

3. When the triangle is equilateral

Let a denote the area and x one side

$$\text{Then, } .4330127 x^2 = a, \therefore x = \sqrt{\frac{a}{.4330127}}.$$

4. When one side and the adjacent angle are given.

Let a denote the area, b the given side, x the adjacent side, and A the included angle

$$\text{Then, } \frac{1}{2}bx \sin A = a, \therefore x = \frac{2a}{b \sin A}.$$

5. When two sides are given.

Let a denote the area, b and c the given sides, and x their included angle.

$$\text{Then, } \frac{1}{2}bc \sin x = a, \therefore \sin x = \frac{2a}{bc}.$$

319. Examples.

1. The area of a triangle is 3 A, the base is 5 ch. Find the altitude and lay out the triangle on the ground.

2. The area of a triangle is 12 A, the base is to the altitude as 3 is to 2. Find the base and altitude and lay out the triangle on the ground.

3. The area of an equilateral triangle is 1 A. Find a side and lay out the triangle.

4. The area of a triangle is 1.2 A, one side is 2 ch., an adjacent angle is 45° . Find the other side adjacent to the given angle and lay out the land.

5. The area of a triangle is 2 A, two sides are 6 ch. and 10 ch. Find the included angle and lay out the triangle.

320. Laying out Circles or Regular Polygons.

1. Let a be the area of the circle, and x the radius.

$$\text{Then, } 3.1416 x^2 = a, \therefore x = \sqrt{\frac{a}{3.1416}}.$$

2. Let a be the area of a regular polygon, x one side, α one angle, n the number of sides, and a' the area of a similar polygon whose side is 1. Article 167

$$\text{Then, } a'x^2 = a, \therefore x = \sqrt{\frac{a}{a'}}. \quad y = \frac{180^\circ(n-2)}{n}.$$

321. Examples.

1. Find the radius of a circle whose area is 1 A. and lay out the circle.
2. Find the sides and angles of a regular hexagon containing 1 A. and lay out the hexagon.
3. Find the sides and angles of a regular octagon containing 1 A. and lay out the octagon.

DIVIDING LAND.

322. Division of Rectangles or Parallelograms.

1. To cut off a given area by a line parallel to a given side.

Let a be the area, b the given side, x the distance to be cut off on the sides adjacent to b , and A the acute angle of the parallelogram

For the rectangle, $bx = a$, $\therefore x = \frac{a}{b}$.

For the parallelogram, $bx \sin A = a$, $\therefore x = \frac{a}{b \sin A}$.

2. When the lot is to be divided into parts having a given ratio, by lines parallel to two of the sides, divide the other sides into parts having the same ratio

323. Examples.

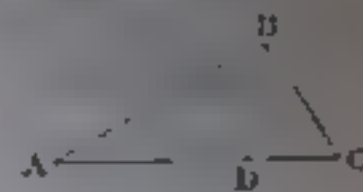
1. The sides of a rectangle are 15 ch. and 10 ch.; cut off 8 A. by a line parallel to the shorter sides.
2. The adjacent sides of a parallelogram are 12 ch. and 20 ch., and their included angle is 65° ; cut off 10 A. by a line parallel to the shorter sides.
3. A man willed that his farm, which was 1 mile long and $\frac{1}{2}$ mile wide, be divided among his three

sons, A , B , and C , aged 21 yrs., 18 yrs., 15 yrs., respectively, in proportion to their ages, by lines parallel to the shorter sides. Make the divisions.

324. Division of Triangles.

1. To find a point on a given side of a triangle from which a line drawn to the vertex of the opposite angle will divide the triangle into parts having a given ratio.

Let $b = AC$, the given side;
 D , the required point; $x = AD$,
 and $ABD : DBC :: m : n$.



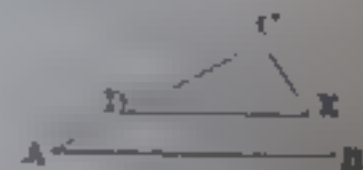
By composition we have,

$$ABC : ABD :: m + n : m; \text{ but } ABC : ABD :: b : x$$

$$\text{Hence, } m + n : m :: b : x, \therefore x = \frac{bm}{m + n}.$$

2. Two sides of a triangle being given, to divide the triangle into parts having a given ratio by a line parallel to the third side.

Let $a = BC$, $b = AC$, the given sides;
 $x = CE$, $y = CD$,
 and $DEC : ABED :: m : n$.



By composition we have,

$$ABC : DEC :: m + n : m;$$

$$\text{but } ABC : DEC :: a^2 : x^2 = b^2 : y^2.$$

$$\text{Hence, } \left\{ \begin{array}{l} m + n : m :: a^2 : x^2, \\ m + n : m :: b^2 : y^2, \end{array} \right\} \Rightarrow \left\{ \begin{array}{l} x = a \sqrt{\frac{m}{m + n}}, \\ y = b \sqrt{\frac{m}{m + n}}. \end{array} \right.$$

If for example, the triangle is to be divided into three equal parts by lines parallel to the third side, then,

The distances cut off on a are $a \sqrt{\frac{1}{3}}$, $a \sqrt{\frac{2}{3}}$.

The distances cut off on b are $b \sqrt{\frac{1}{3}}$, $b \sqrt{\frac{2}{3}}$.

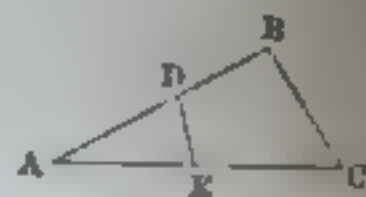
3. Two sides of a triangle being given, to cut off, by a line intersecting the given sides, an isosceles triangle having a given ratio to the given triangle.

Let $b = AC$, $c = AB$, the two given sides; $x = AE = AD$, and

$$ADE : ABC :: m : n.$$

$$\text{But, } ADE : ABC :: x^2 : bc.$$

$$\text{Hence, } m : n :: x^2 : bc, \therefore x = \sqrt{\frac{bcm}{n}}.$$

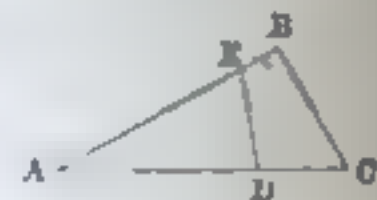


4. Two sides of a triangle being given, to cut off a triangle having a given ratio to the given triangle by a line running from a given point in one of the given sides to the other given side.

Let $b = AC$, $c = AB$, the given sides; D , the given point; $d = AD$, $x = AE$, and $AED : ABC :: m : n$.

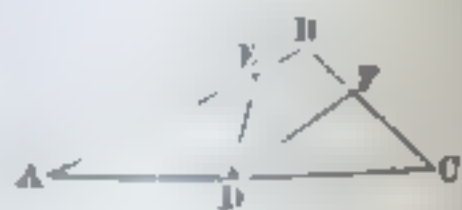
$$\text{But, } AED : ABC :: dx : bc.$$

$$\text{Hence, } m : n :: dx : bc, \therefore x = \frac{bcm}{dn}.$$



5. The three sides being given, to divide the triangle into three equal parts by lines running from a given point in one of the sides.

Let a, b, c be the sides of the triangle, respectively, opposite the angles A, B, C ; $p = AD$, $q = CD$, $x = AE$, and $y = CF$.

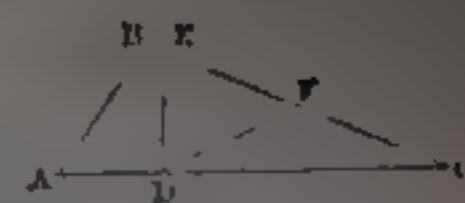


$$\text{Then, } \left\{ \begin{array}{l} 3 : 1 :: bc : px, \\ 3 : 1 :: ab : qy, \end{array} \right\} \therefore \left\{ \begin{array}{l} x = \frac{bc}{3p}, \\ y = \frac{ab}{3q}. \end{array} \right.$$

If x , thus found, is greater than c , both lines will intersect a . Then find y as above.

Let $x = CE$.

$$\text{Then, } 3 : 2 :: ab : qx, \therefore x = \frac{2ab}{3q}.$$



If y , found above, is greater than a , both lines will intersect c . Then find x as in first case.

Let $AF = y$.

$$\text{Then, } 3 : 2 :: bc : py, \therefore y = \frac{2bc}{3p}.$$



6. To divide a triangle into four equal triangles, join the middle-points of the sides.

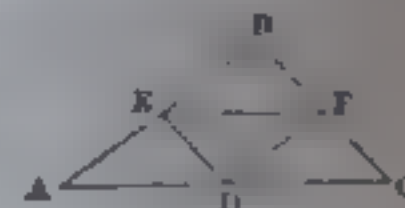
The lines ED , EF , and DF are, respectively, parallel to BC , AC , and AB .

$EDF = EDF$, since each is $\frac{1}{2}$ the parallelogram BD .

$ADE = EDF$, since each is $\frac{1}{2}$ the parallelogram AE .

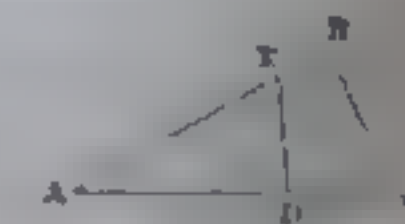
$CDF = EDF$, since each is $\frac{1}{2}$ the parallelogram CE .

Hence, the triangles are all equal, and each is $\frac{1}{4}$ ABC .



7. The bearing of two sides being given, to cut off a triangle having a given area by a line of a given bearing intersecting the sides whose bearings are given.

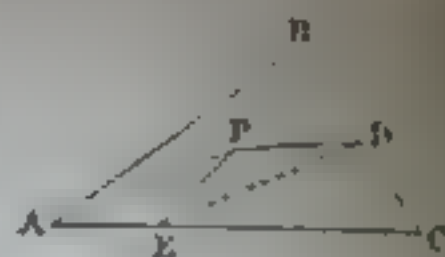
Let ADE be the triangle cut off, a the area of ADE ; $x = AD$ and $y = AE$. The angles A, D, E can be determined from the bearings.



$$\text{Then, } \left\{ \begin{array}{l} \frac{1}{2} xy \sin A = a, \\ \sin E : \sin D :: x : y \end{array} \right\} \therefore \left\{ \begin{array}{l} x = \frac{2a \sin E}{\sin A \sin D}, \\ y = \frac{2a \sin D}{\sin A \sin E}. \end{array} \right.$$

8. To divide a triangle into two equal parts by lines drawn from a point within.

Let ABC be the given triangle, and P the given point.



Run a line from P to the vertex A , and another from P to D , the middle point of the opposite side BC . Run DE parallel to PA , and run PE . PD and PE will be the dividing lines, and $CDPE$ will be $\frac{1}{2} ABC$.

For, draw the line AD , then we have,

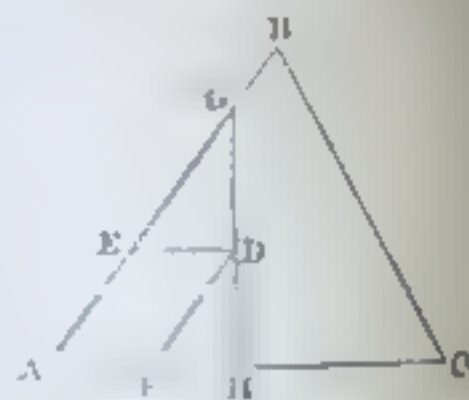
$$CDPE = CDE + PED, \text{ and } ACD = CDE + AED.$$

$$\text{But } PED = AED, \therefore CDPE = ACD.$$

$$\text{But } ACD = \frac{1}{2} ACB, \therefore CDPE = \frac{1}{2} ACB.$$

9. Through a given point, within a given triangle, to draw a line which shall cut off a triangle having a given ratio to the given triangle.

Let ABC be the given triangle; a, b, c , the sides opposite the angles A, B, C , respectively; D the point given by knowing $p = AF = ED$, parallel to AC ; $q = AE = FD$, parallel to AB ; $x = AH$, $y = AG$, and $AGH : ABC :: m : n$. Then,

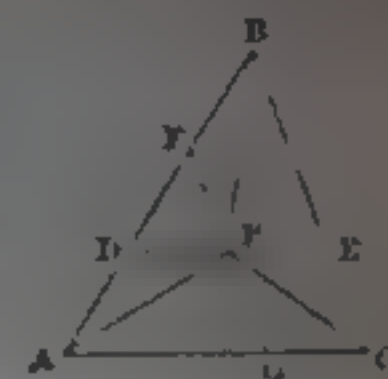


$$\left. \begin{array}{l} x : y :: x - p : q. \\ xy : bc :: m : n. \end{array} \right\} \therefore \left\{ \begin{array}{l} x = \frac{bcm \pm 1}{2nq} \sqrt{b^2c^2m^2 - 4bcmnpq} \\ y = \frac{bcm \pm 1}{2bp} \sqrt{b^2c^2m^2 - 4bcmnpq} \end{array} \right.$$

Remark — If either $x > b$ or $y > c$, the line cuts off the triangle from another angle; and the distances cut off from the vertex of this angle can be found in a manner similar to the above.

10. To find a point within a triangle from which the lines drawn to the vertices will divide the triangles into three equal triangles.

Let ABC be the triangle. Take $AD = \frac{1}{3} AB$, $CE = \frac{1}{3} CB$, and draw DE . Take $BF = \frac{1}{3} BA$, $CG = \frac{1}{3} CA$, and draw FG .



P , the intersection of these lines, will be the point required.

$$\text{For } AD : AB :: \text{altitude of } APC : \text{altitude } ABC.$$

$$\text{But } AD = \frac{1}{3} AB, \therefore \text{altitude } APC = \frac{1}{3} \text{ altitude } ABC.$$

$$\therefore APC = \frac{1}{3} ABC.$$

$$\text{In like manner, } BPC = \frac{1}{3} ABC.$$

$$\therefore APB = \frac{1}{3} ABC.$$

Remark. — If APC , BPC , and APB are to be to each other as p, q, r , take $AD = \frac{p}{p+q+r}$ of AB , $CE = \frac{q}{p+q+r}$ of CB , $BF = \frac{q}{p+q+r}$ of BA , $CG = \frac{r}{p+q+r}$ of CA , and draw DE and FG , their intersection will be the point required.

325. Examples.

1. One side of a triangle is 15 ch.; from what point in this side must a line be drawn to the vertex of the opposite angle so as to divide the triangle into two triangles which are to each other as 2 to 3?

Ans. 6 ch. from one extremity

2. Two sides of a triangle are 10 ch and 15 ch., respectively; find the distance from the vertex of the

angle included by these sides, cut off on each of these sides by a line parallel to the third side, dividing the triangle into a triangle and a trapezoid, so that the triangle cut off shall be to the trapezoid as 9 to 16.

Ans. 6 ch. and 9 ch.

3. Two sides of a triangle are 4 ch. and 9 ch., respectively; find the distance from the vertex cut off on each of these sides by a line cutting off an isosceles triangle which shall be to the given triangle as 16 to 25.

Ans. 4.80 ch.

4. Two sides of a triangle are 7 ch. and 9 ch., respectively. From a point in one side, 5 ch. from the vertex of the angle included by these sides, a line is run to the other given side, cutting off a triangle which is to the given triangle as 5 to 9. How far from the same vertex does this line intersect that side?

Ans. 7 ch.

5. The sides of a triangle, ABC , are $a = 6$ ch., $b = 12$ ch., and $c = 9$ ch. From the middle point of b two lines are run, dividing the triangle into three equal parts. To what points of what sides must the lines be run?

Ans. To c , 6 ch. from A , and to a , 4 ch. from C .

6. The sides of a triangle, ABC , are $a = 10$ ch., $b = 12$ ch., and $c = 4$ ch. From a point in b , 3 ch. from A , two lines are run, dividing the triangle into three equal parts. To what points of what side must these lines be run?

Ans. To a , 8.89 ch. from C , and to a , 4.44 ch. from C .

7. The sides of a triangle, ABC , are $a = 5$ ch., $b = 18$ ch., and $c = 15$ ch. From a point in b , 12 ch. from A , two lines are run, dividing the triangle into three equal parts. To what points must these lines be run?

Ans. To c , 7.50 ch. from A , and to B .

8. In the triangle ABC , the side AB runs N. 50° E., AC runs E. DE , running N. 10° W., intersects these lines in D and E , and cuts off $ADE = 10$ A. Required AD and AE . *Ans.* $AD = 16.54$, $AE = 18.81$.

9. In the 9th general problem of the last article, $b = 10$ ch., $c = 12$ ch., $m = 1$, $n = 4$, $p = 2$ ch., $q = 3$ ch. Find x and y . *Ans.* $x = 7.24$ ch., $y = 4.14$ ch.

326. Division of Trapezoids.

1. Given the bases and a third side of a trapezoid, to divide it into parts having a given ratio by a line parallel to the bases.

Let $ABCD$ be the trapezoid, $b = AB$, $b' = CD$, $s = AD$, $x = AE$, $y = EF$, the dividing line, parallel to the bases, and $ABFE : EFCD :: m : n$.



Produce AD and BC to G .

$$\text{Then, } \begin{cases} ABG : DCG :: b^2 : b'^2, \\ EFG : DCG :: y^2 : b'^2. \end{cases}$$

These proportions taken by division give,

$$ABCD : DCG :: b^2 - b'^2 : b'^2,$$

$$EFCD : DCG :: y^2 - b'^2 : b'^2.$$

Since the consequents are the same, we have,

$$ABCD : EFCD :: b^2 - b'^2 : y^2 - b'^2.$$

This proportion taken by division gives,

$$ABFE : EFCD :: b^2 - y^2 : y^2 - b'^2,$$

$$\text{But } ABFE : EFCD :: m : n.$$

$$\therefore b^2 - y^2 : y^2 - b'^2 :: m : n, \therefore y = \sqrt{\frac{b^2 n + b'^2 m}{m + n}}.$$

Drawing DH parallel to BC , we have,

$$AH : EI :: AD : ED,$$

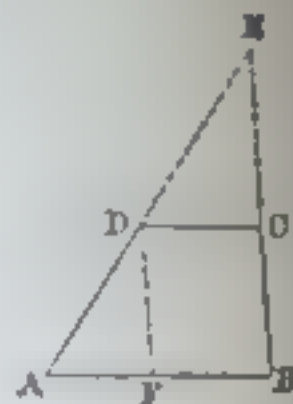
$$\text{or } b - b' : y - b' :: s : s - x, \therefore x = \frac{s}{b - b'}(b - y),$$

$$\therefore x = \frac{s}{b} \left(b - \sqrt{\frac{b^2 n + b'^2 m}{m + n}} \right)$$

2. Given a side and two adjacent angles of a tract of land, to cut off a trapezoid of a given area by a line parallel to the given side.

1st. When the sum of the two angles $< 180^\circ$.

Let $a \doteq ABCD$ = the area cut off, $b = AB$ the given side, $x = AD$, $y = BC$, $z = DC$, $E = 180^\circ - (A + B)$.



$$(1) \text{ Area } ABE = \frac{1}{2} EB \times EA \sin E.$$

$$\sin E : \sin A :: b : EB, \therefore EB = \frac{b \sin A}{\sin E}.$$

$$\sin E : \sin B :: b : EA, \therefore EA = \frac{b \sin B}{\sin E}.$$

Substituting the values of EB and EA in (1), we have,

$$(2) \text{ ABE} = \frac{b^2 \sin A \sin B}{2 \sin E}$$

$$\therefore (3) \text{ DCE} = \frac{b^2 \sin A \sin B}{2 \sin E} - a.$$

$$\text{But } ABE : DCE :: b^2 : z^2,$$

$$\therefore \frac{b^2 \sin A \sin B}{2 \sin E} : \frac{b^2 \sin A \sin B}{2 \sin E} - a :: b^2 : z^2.$$

$$\therefore z = \sqrt{b^2 - \frac{2 a \sin E}{\sin A \sin B}}.$$

Draw DF parallel to EB , then $ADF = E$ and $DFA = B$.

$$\sin E : \sin B :: b : z, \therefore z = \frac{b \sin B}{\sin E}.$$

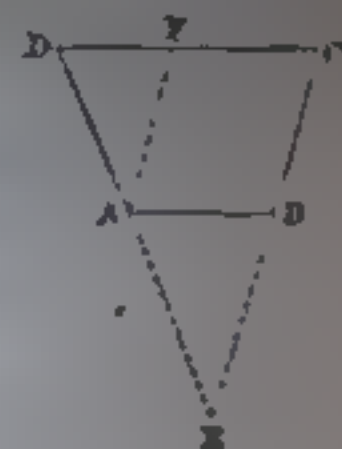
$$\text{In like manner we shall find } y = \frac{(b - z \sin A)}{\sin E}.$$

Since z is known, x and y are known.

2d. When the sum of the two angles $> 180^\circ$.

E and DC lie on opposite sides of AB .

Let $a \doteq ABCD$ = the area to be cut off, $b = AB$ the given side, $x = AD$, $y = BC$, $z = DC$, $E = A + B - 180^\circ$.



By a process similar to that employed in first case, we find,

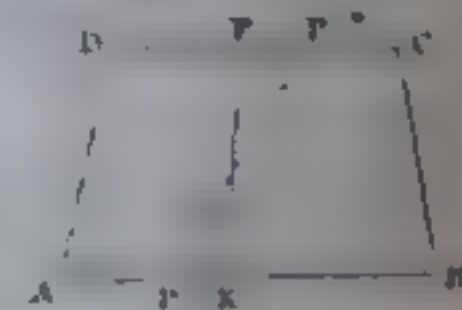
$$z = \sqrt{b^2 + \frac{2 a \sin E}{\sin A \sin B}}.$$

$$x = \frac{(z - b) \sin B}{\sin E}.$$

$$y = \frac{(z - b) \sin A}{\sin E}.$$

3. To divide a trapezoid into proportional parts by a line joining the bases.

Let $ABCD$ be the trapezoid, b and b' the bases, a the altitude, m and n the ratio of the parts.



$$\text{Take } AE = \frac{mb}{m+n}, \text{ then } EB = \frac{nb}{m+n}.$$

$$\text{also } DF = \frac{mb'}{m+n}, \text{ then } FC = \frac{nb'}{m+n}.$$

Then, $AEFD = \frac{am(b+b')}{2(m+n)}$, and $EBCF = \frac{an(b+b')}{2(m+n)}$.

$$\text{But } \frac{am(b+b')}{2(m+n)} : \frac{an(b+b')}{2(m+n)} :: m : n.$$

$$\therefore AEFD : EBCF :: m : n.$$

Remark.—If the line is to be drawn from a given point P , in one base, first divide as above; then, if P is on one side of E , take P' as far on the other side of F , and draw PP' .

This change in the dividing line does not affect the altitude of the parts, nor the sum of their bases, since one is increased as much as the other is diminished, nor, consequently, their area.

A similar process can be employed whatever be the number of parts.

327. Examples.

1. A trapezoid whose bases are $b = 15$ ch. and $b' = 12$ ch., and third side $s = 10$ ch., is divided by a line parallel to the bases into two parts, such that the part adjacent to b is to the part adjacent to b' as 3 to 2. Required the length of the dividing line, and the distance from b cut off on s . *Ans.* 13.28 ch., and 5.73 ch.

2. Given a side 14.30 ch., and the two adjacent angles, 60° and 70° , respectively, of a tract of land from which 10 A. are to be cut off by a line parallel to the given side. Required the length of the dividing line, and the respective distances from the given side cut off on the adjacent sides.

Ans. 4.03 ch., 12.60 ch., and 11.61 ch.

3. Given a side 10 ch. and the two adjacent angles, 120° and 115° , respectively, of a tract of land, from which 15 A. are to be cut off by a line parallel to the

given side. Required the length of the dividing line, and the respective distances from the given side cut off on the adjacent sides.

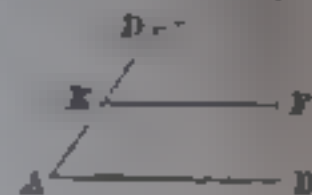
Ans. 20.32 ch., 11.42 ch., 10.91 ch.

4. A trapezoid whose parallel sides are $AB = 14$ ch., and $DC = 7$ ch., is divided by the line PP' into two parts which are to each other as 3 to 4; $AP = 4$ ch., find DP' . *Ans.* 5 ch.

328. Division of Trapeziums.

1. Given a side, two adjacent angles, and the area of a trapezium, to divide it, by a line parallel to the given side, into parts having a given ratio.

Let $ABCD$ be the trapezium; $b = AB$, the given side; A and B , the given angles; $G = 180^\circ - (A + B)$, $a =$ the area of $ABCD$, $x = AE$, $y = BF$, and $ABFE : EFCD :: m : n$.



$$\therefore ABFE = \frac{ma}{m+n}, EFCD = \frac{na}{m+n}.$$

$$ABG = \frac{1}{2} BG \times AG \times \sin G.$$

$$BG = \frac{b \sin A}{\sin G} \text{ and } AG = \frac{b \sin B}{\sin G}.$$

$$\therefore ABG = \frac{b^2 \sin A \sin B}{2 \sin G}.$$

$$\therefore EFG = \frac{b^2 \sin A \sin B}{2 \sin G} - \frac{ma}{m+n}.$$

$$ABG : EFG :: AG^2 : EG^2, ABG : EFG :: BG^2 : FG^2.$$

Substituting, in the proportions, the values of ABG , EFG , AG and BG , find EG and FG , and substituting the values of AG , EG , BG and FG in the equations,

$$x = AG - EG \text{ and } y = BG - FG, \text{ we have,}$$

S. N. 28.

$$x = \frac{b \sin B}{\sin G} - \sqrt{\frac{b^2 \sin^2 B}{\sin^2 G} - \frac{2ma \sin B}{(m+n) \sin A \sin G}}$$

$$y = \frac{b \sin A}{\sin G} - \sqrt{\frac{b^2 \sin^2 A}{\sin^2 G} - \frac{2ma \sin A}{(m+n) \sin B \sin G}}$$

2. Given the bearings of three adjacent sides of a tract of land, and the length of the middle side, to cut off, by a line running a given course, a trapezium of a given area.

Let $a = ABCD$, the area cut off; $b = AB$, the given side; $x = AD$, $y = BC$, $z = CD$.

From the given bearings, find the angles A, B, C, D, E .



$$BE = \frac{b \sin A}{\sin E} \text{ and } AE = \frac{b \sin B}{\sin E}$$

$$ABE = \frac{1}{2} BE \times AE \times \sin E = \frac{b^2 \sin A \sin B}{2 \sin E}$$

$$\therefore DCE = \frac{b^2 \sin A \sin B}{2 \sin E} - a$$

$$DE = \frac{z \sin C}{\sin E} \text{ and } CE = \frac{z \sin D}{\sin E}$$

$$DCE = \frac{1}{2} DE \times CE \times \sin E = \frac{z^2 \sin C \sin D}{2 \sin E}$$

$$\therefore \frac{z^2 \sin C \sin D}{2 \sin E} = \frac{b^2 \sin A \sin B}{2 \sin E} - a$$

$$\therefore z = \sqrt{\frac{b^2 \sin A \sin B}{\sin C \sin D} - \frac{2a \sin E}{\sin C \sin D}}$$

Substituting the value of z in the values of DE and CE , then the values of AE, DE, BE and CE in the equations,

$x = AE - DE$, and $y = BE - CE$, we find,

$$x = \frac{b \sin B}{\sin E} - \sqrt{\frac{b^2 \sin A \sin B \sin C}{\sin^2 E \sin D} - \frac{2a \sin C}{\sin D \sin E}}$$

$$y = \frac{b \sin A}{\sin E} - \sqrt{\frac{b^2 \sin A \sin B \sin D}{\sin^2 E \sin C} - \frac{2a \sin D}{\sin C \sin E}}$$

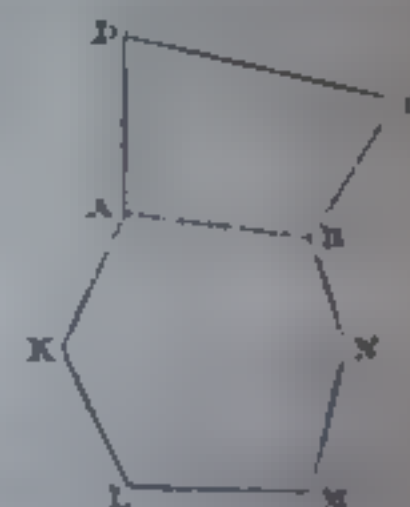
Remark.—If $A + B > 180^\circ$, the values of x and y are

$$x = \sqrt{\frac{b^2 \sin A \sin B \sin C}{\sin^2 E \sin D} + \frac{2a \sin C}{\sin D \sin E}} - \frac{b \sin B}{\sin E}$$

$$y = \sqrt{\frac{b^2 \sin A \sin B \sin D}{\sin^2 E \sin C} + \frac{2a \sin D}{\sin C \sin E}} - \frac{b \sin A}{\sin E}$$

3. The bearings of several adjacent sides of a tract of land being given, and the length of each, except the first and last, to cut off a given area by a line of given bearing intersecting the first and last sides.

Let the bearings and distances of AK, KL, LM, MN, NB be given, and the bearings of AD and BC ; and let a be the area cut off by CD .



Draw AB ; then, in the polygon, $ABNMLK$, the bearings and distances of all the sides are known, except AB , which can be computed, and the area of $ABNMLK$ found. Subtract the area thus found from the area to be cut off by CD , and the remainder will be the area of $ABCD$.

Then, by the last case, find AD and BC .

4. The bearings of the sides of any quadrilateral tract of land and the distances of two opposite sides being given, to divide it into parts having a given ratio by a line of a given course intersecting the other sides.

Let $b = AB$, $c = CD$,
 $x = AE$, $y = BF$, $z = EF$,
 and $ABFE : EFCD :: m : n$.

Find the angles A, B, C, D, E, F, G .

$$BG = \frac{b \sin A}{\sin G}, \quad AG = \frac{b \sin B}{\sin G}, \quad DG = \frac{c \sin C}{\sin G},$$

$$CG = \frac{c \sin D}{\sin G}, \quad FG = \frac{z \sin E}{\sin G}, \quad EG = \frac{z \sin F}{\sin G}.$$

$$ABFE = \frac{m(b^2 \sin A \sin B + c^2 \sin C \sin D)}{2(m+n) \sin G}.$$

$$ABFE = \frac{b^2 \sin A \sin B + z^2 \sin E \sin F}{2 \sin G}.$$

Equating these values of $ABFE$, we find,

$$z = \sqrt{\frac{mb^2 \sin A \sin B + mc^2 \sin C \sin D}{(m+n) \sin E \sin F}}.$$

Substituting this value of z in the values of FG and EG , then the values of AG , EG , BG and FG in

$x = AG - EG$, and $y = BG - FG$, we have,

$$x = \frac{b \sin B}{\sin G} - \frac{\sin F}{\sin G} \sqrt{\frac{mb^2 \sin A \sin B + mc^2 \sin C \sin D}{(m+n) \sin E \sin F}},$$

$$y = \frac{b \sin A}{\sin G} - \frac{\sin E}{\sin G} \sqrt{\frac{mb^2 \sin A \sin B + mc^2 \sin C \sin D}{(m+n) \sin E \sin F}}.$$

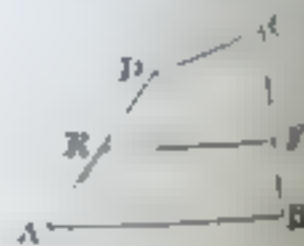
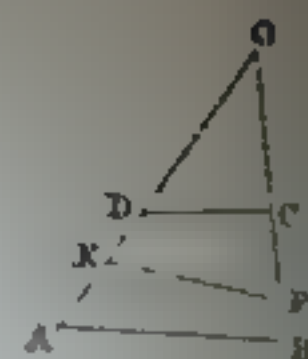
5. The bearings and distances of the sides of any quadrilateral tract of land being given, to divide it into parts having a given ratio by a line dividing the opposite sides proportionally.

$$b = AB, \quad c = CD, \quad d = AD,$$

$$e = BC, \quad x = AE, \quad y = BF,$$

$$ABFE : EFCD :: m : n,$$

$$x : d - x :: y : e - y, \quad \therefore y = \frac{ex}{d}.$$



From the bearings find the angles A, B, C, D, G .

$$BG = \frac{b \sin A}{\sin G}, \quad \text{and} \quad AG = \frac{b \sin B}{\sin G},$$

$$ABFE = \frac{m(b^2 \sin A \sin B + c^2 \sin C \sin D)}{2(m+n) \sin G}.$$

$$EFG = \frac{b^2 \sin A \sin B}{2 \sin G} - \frac{m(b^2 \sin A \sin B + c^2 \sin C \sin D)}{2(m+n) \sin G}.$$

$$\therefore EFG = \frac{nb^2 \sin A \sin B + mc^2 \sin C \sin D}{2(m+n) \sin G}.$$

$$\text{But } EFG = \frac{1}{2}(q-x)(p-\frac{ex}{d}) \sin G.$$

$$\therefore \frac{1}{2}(q-x)(p-\frac{ex}{d}) \sin G = \frac{nb^2 \sin A \sin B + mc^2 \sin C \sin D}{2(m+n) \sin G}.$$

$$\therefore x = \frac{dp + eq \pm \sqrt{(dp - eq)^2 + \frac{8deab}{\sin G}}}{2e}.$$

$$\therefore y = \frac{dp + eq \pm \sqrt{(dp - eq)^2 + \frac{8deab}{\sin G}}}{2d}.$$

6. The bearings and distances of the sides of a quadrilateral being given, to cut off a given area by a line running through a point whose bearing and distance from the vertex of one of the angles are given.

Let a be the area of $ABFE$, cut off by EF through P .

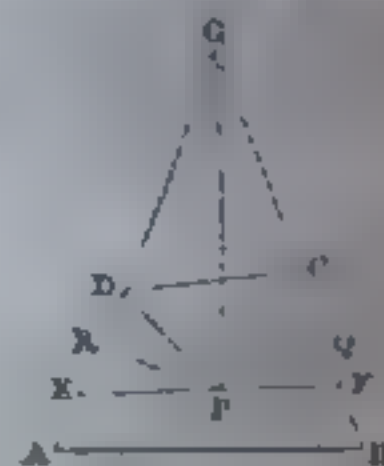
$$b = AB, \quad c = CD, \quad u = EG,$$

$$e = BC, \quad x = AE, \quad y = BF.$$

The bearings give the angles A, B, C, D, PCQ, PCD .

$$BG = \frac{b \sin A}{\sin G}, \quad AG = \frac{b \sin B}{\sin G}, \quad ABG = \frac{b^2 \sin A \sin B}{2 \sin G}.$$

$$EFG = \frac{b^2 \sin A \sin B}{2 \sin G} - a = a'.$$



In the triangle DCP we have given CD , CP , and PCP , hence DP and DP can be found; then PDR $CPR = CDP$

$$PR = DP \sin PDR = p, \text{ and } PQ = CP \sin PCQ = q$$

$$EPG = \frac{1}{2} pu, \text{ and } FPG = \frac{1}{2} qv.$$

$$\therefore \left. \begin{array}{l} \frac{1}{2} pu + \frac{1}{2} qv = a' \\ \text{But } \frac{1}{2} uv \sin G = a' \end{array} \right\} \therefore \begin{cases} u = \frac{a'}{p} \pm \sqrt{\left(\frac{a'}{p}\right)^2 - \frac{2aq}{p \sin G}} \\ v = \frac{a'}{q} \pm \sqrt{\left(\frac{a'}{q}\right)^2 - \frac{2ap}{q \sin G}} \end{cases}$$

$$\therefore \begin{cases} x = \frac{b \sin B}{\sin G} - \frac{a'}{p} \pm \sqrt{\left(\frac{a'}{p}\right)^2 - \frac{2aq}{p \sin G}} \\ y = \frac{b \sin A}{\sin G} - \frac{a'}{q} \pm \sqrt{\left(\frac{a'}{q}\right)^2 - \frac{2ap}{q \sin G}} \end{cases}$$

7. The bearings and distances of the sides of a quadrilateral being given, to divide it into four equal parts by two lines intersecting the pairs of opposite sides, respectively, one line being parallel to one side

Let EF , parallel to AB , and MN , parallel to BC , each divide $ABCD$ into two equal parts; and PQ , parallel to FC , divide $EFCD$ into two equal parts.

Find AE , BF , BM , CN , CP , and FQ , by problem 1 of this article.

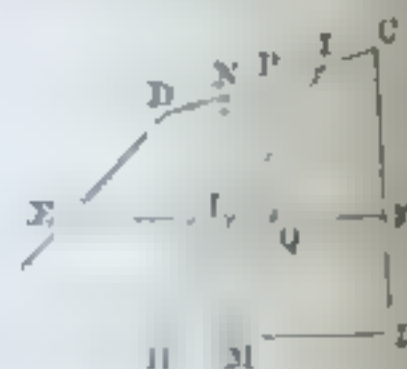
$$EF = AB - AE \cos A - BF \cos B.$$

Likewise find MN and PQ . $NP = CN - CP$.

Produce MQ to I , draw NH parallel to IM , and draw HI ; then will EF and HI be the lines required.

The line EF is evidently one of the required lines.

We are now to prove that HI is the other.



The two triangles, HNI and HNM , are equal, since they have a common base, HN , and a common altitude, their vertices being in IM , parallel to the base.

To each of these equal triangles add $AHND$, and we have $AHID = AMND = \frac{1}{2} ABCD$.

We are now to prove that HI divides $EFCD$, and also $ABFE$ into two equal parts.

$$IMH : IQL :: \overline{IM}^2 : IQ^2.$$

$$IMN : IQP :: \overline{IM}^2 : IQ^2.$$

$$\therefore IMH : IQL :: IMN : IQP.$$

$$\text{But } IMH = IMN. \therefore IQL = IQP.$$

To each add $QFCI$, and we shall have,

$$LFCI = QFCP = \frac{1}{2} EFCD.$$

Again, $HBCI = AHID$ and $LFCI = ELID$.

Subtracting the second from the first, member from member, we have,

$$HBFL = AHLE.$$

Hence, HI is the other division line required.

Let us now find the situation of the points H and I , on the lines AB and CD , respectively.

$$NM : PQ :: NP + PI : PI$$

$$\therefore NM \times PI = PQ \times NP + PQ \times PI$$

$$(NM - PQ) PI = PQ \times NP.$$

$$\therefore PI = \frac{PQ \times NP}{NM - PQ}. \text{ Then, } CI = CP - PI.$$

The bearing and length of IM , and the area of $ICBM$, can be found by Art. 305. $IMH = ICBH - ICBM$

If p be the perpendicular from I to AB ,

$$p = IM \sin IMB. \quad MH = \frac{2 IMH}{p}. \quad BH = BM + MH$$

329. Examples.

1. A trapezium, one side of which is 20 ch., the adjacent angles 60° and 80° , respectively, and the area 10 A., is divided into two equal parts by a line parallel to the given side. Required the distance from the given side cut off on the adjacent sides.

Ans. 8.04 ch., and 2.68 ch.

2. From a tract of land, the bearings of three of whose adjacent sides are S. 20° W., E., and N. 10° W., and the distance of the middle side is 10 ch., 5 A. are cut off by a line running S. 70° W., and intersecting the first and third of the above mentioned sides. Required the distances cut off on these sides from the middle side.

Ans. 4.91 ch., and 7.29 ch.

3. From a tract of land, the bearings of whose sides are S. 38° E., S. $29\frac{1}{2}^\circ$ E., S. $31\frac{1}{2}^\circ$ W., N. 61° W., and N. 40° W., respectively, and the distances of the second, third, and fourth sides are 8.18 ch., 15.26 ch., and 14.48 ch., respectively, 39 A. 2 R. 36 P. are cut off by a line running N. 80° E., and intersecting the first and last sides. Required the distances cut off on these sides respectively.

Ans. 7.01 ch., 16.19 ch.

4. A tract of land, the bearing and distances of whose sides are AB, E. 22.21 ch.; BC, N. $56\frac{1}{2}^\circ$ W., 12 ch.; DA, S. 24° W., is cut by EF running S. $76\frac{1}{2}^\circ$ E., intersecting AD and BC and dividing the field so that ABFE : EFCD = 5 : 3. Required AE and BF.

Ans. AE = 16.50 ch., BF = 11.31 ch.

5. A trapezium whose sides are AB = 20.15 ch., BC = 21.73 ch., CD = 15.38 ch., DA = 13.32 ch., and whose angles are A = $97\frac{1}{2}^\circ$, B = 64° , C = $89\frac{1}{4}^\circ$, D = 100° , is divided into two equal parts by the line EF,

dividing AD and BC proportionally. Required AE and BF.

Ans. AE = 6.22 ch., BF = 10.15 ch.

6. Within a tract of land whose sides are 1st. E. 15.58 ch.; 2d. N. $13\frac{1}{2}^\circ$ W., 40.86 ch.; 3d. S. 82° W., 30.40 ch.; 4th. S. $9\frac{1}{2}^\circ$ W., 36 ch.—there is a spring whose bearing and distance from the 3d corner is S. 21° W., 15.80 ch. It is required to cut off 40 A. from the north side of this tract by a line running through the spring and intersecting the 2d and 4th sides. Required the distance from the 1st corner to the point of intersection on the 4th side.

Ans. 26.73 ch.

7. A tract of land whose boundaries are—1st. E. 23.24 ch.; 2d. N. $11\frac{1}{2}^\circ$ W., 15.25 ch.; 3d. N. $51\frac{1}{2}^\circ$ W., 11.50 ch.; 4th. S. 27° W., 24.82 ch.—is to be divided into four equal parts by two lines, one parallel to the first side, the other intersecting the first and third sides. Required the distances cut off by the parallel from the first and second corners, measured on the fourth and second sides, respectively; also the distances cut off by the other line from the first and fourth corners, measured on the first and third sides, respectively.

Ans. 8.57 ch., 7.79 ch., 10.66 ch., 3.15 ch.

330. Division of Polygons.

1. From a given point in the boundary of a tract of land, the bearings and distances of whose sides are given, to run a line which shall cut off a given area.

Let A be the point, and suppose it probable that the dividing line will terminate on DE. Suppose the closing line AD to be run, the bearing and distance of which can be found on the

S. N. 20.



ground by observation and measurement, or, as in surveying commissions, from the bearings and distances of AB , BC , and CD . Compute the area of $ABCD$, which, if less than the area to be cut off, subtract from that area, which gives the addition, a , to $ABCD$. The bearings of AD and DE give the angle ADE .

The perpendicular, $AG = AD \sin ADG$.

Then, if AP is the dividing line, $DP = \frac{a}{\frac{1}{2}AG}$.

If $DP > DE$, run another closing line AE , and proceed as before.

If $ABCD$ is greater than the area to be cut off, subtract the area to be cut off from $ABCD$ and divide the difference by one-half the perpendicular from A to CD , and the quotient, if less than DC , will be the distance from D to the point on DC to which the division line is to be drawn.

If the quotient is greater than DC , run another closing line, AC , and proceed as before.

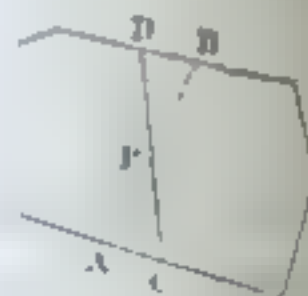
2. Through a given point within a tract of land, the bearings and distances of whose sides are given, to run a line which shall cut off a given area.

Let P be the given point. Run a trial line, AB , and calculate the area which it cuts off.

Let d be the difference between this area, which we will suppose too small, and the area to be cut off.

Let CD be the division line required

$$d = APC - BPD.$$



Let $m = AP$, and $n = PB$, which measure; find the angle PAC , also PBD . We are to find the angle P .

$$C = 180^\circ - (A + P), \text{ and } D = 180^\circ - (B + P).$$

$$\therefore \sin C = \sin (A + P), \text{ and } \sin D = \sin (B + P).$$

$$PC = \frac{m \sin A}{\sin (A + P)}, \quad AC = \frac{m \sin P}{\sin (A + P)},$$

$$\therefore APC = \frac{m^2 \sin A \sin P}{2 \sin (A + P)}$$

$$PD = \frac{n \sin B}{\sin (B + P)}, \quad BD = \frac{n \sin P}{\sin (B + P)},$$

$$\therefore BPD = \frac{n^2 \sin B \sin P}{2 \sin (B + P)}$$

$$d = \frac{m^2 \sin A \sin P}{2 \sin (A + P)} - \frac{n^2 \sin B \sin P}{2 \sin (B + P)}$$

$$2d = \frac{m^2}{\cot P + \cot A} - \frac{n^2}{\cot P + \cot B}$$

Use natural co-tangents, find $\cot P$, and then P .

331. Examples.

1. The boundaries of a tract of land are: AB , W. 25 ch.; BC , N. $32\frac{1}{2}^\circ$ W., 16.09 ch.; CD , N. 20° E., 15.50 ch.; DE , E. 25 ch.; EF , S. 30° E.; and FA , S. 25° W., to the point of beginning. A line is run from A , cutting off 70 A. 1 R. 33 P. from the west side. Required the end point in which this line cuts the boundary.

Ans. The side DE , 18 ch. East of P .

2. It is required to run a line through a point, P , within a field, so as to cut off 10 A. A guess line through P , intersecting opposite sides in A and B , cuts off 9 A. Required the angle which the true division line, CD , makes with AB , if $AP = 12$ ch., $PB = 4$ ch., $PAC = 90^\circ$, $PBD = 60^\circ$.

Ans. $8^\circ 18'$

LEVELING

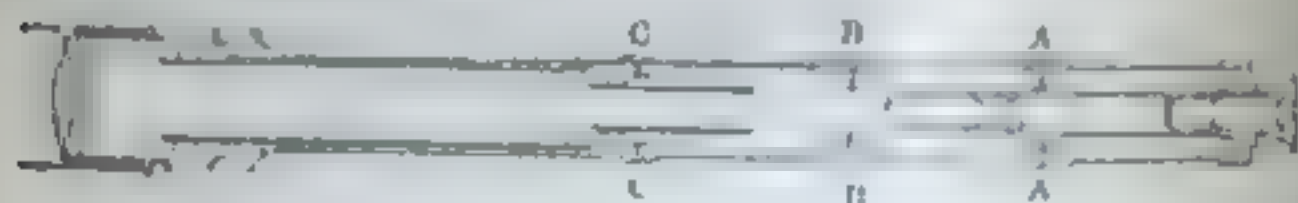
332. The Y Level.

The **Y level**, so called from the form of the supports in which the telescope rests, is exhibited in the annexed engraving.

The **telescope** is inclosed in rings, by which it can be revolved in the Y's or clamped in any position.

The **Y's** have each two nuts, adjustable with the steel pin, and the rings are clamped in the Y's by bringing the clips firmly on them by means of tapering Y pins.

The interior construction of the telescope is exhibited in the following figure.



The **rack and pinion**, AA and CC, are contrivances, the first for centering the eye-piece, and the second for insuring the accurate projection of the object-glass in a straight line.

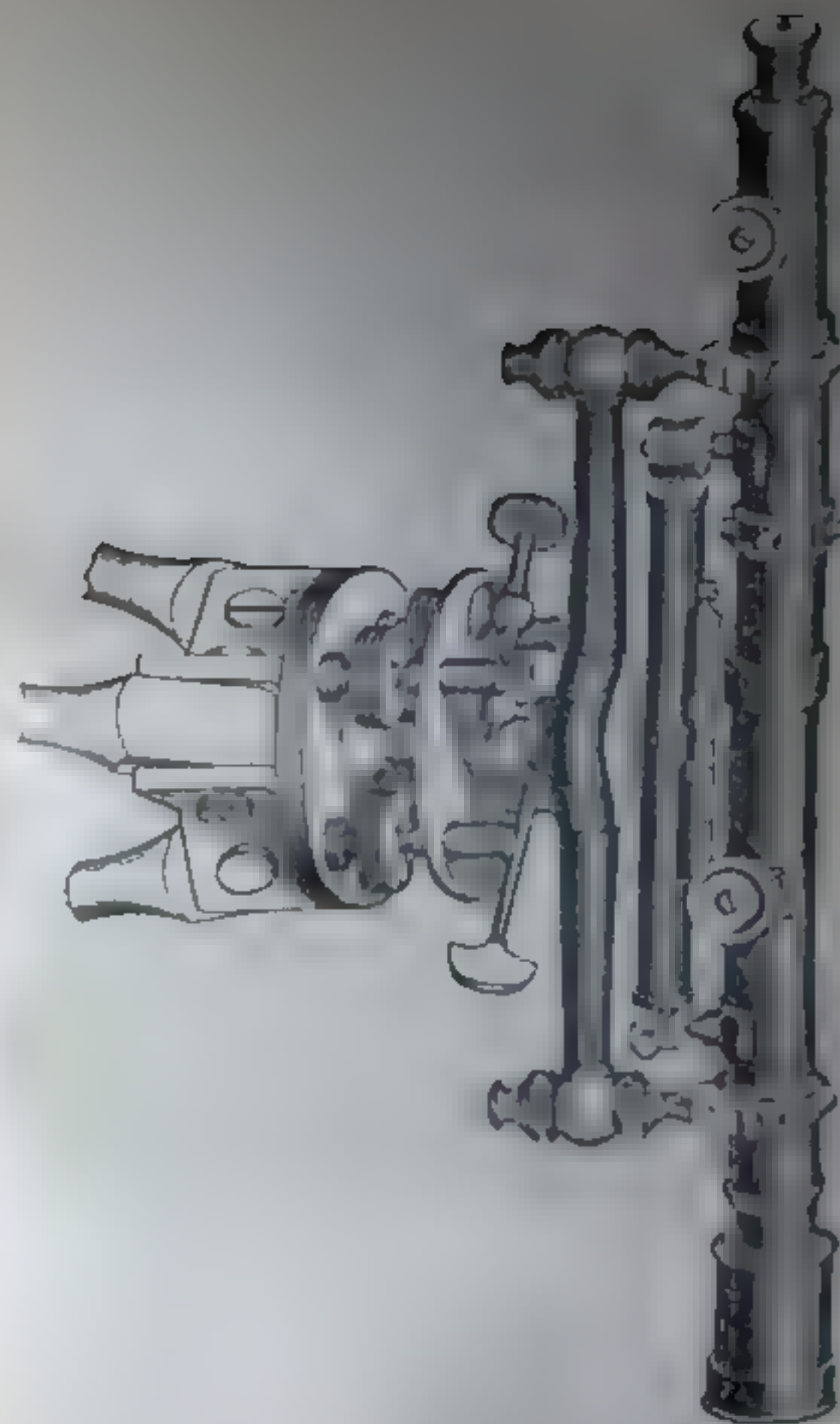
The **level** is a ground bubble tube, attached to the under side of the telescope, and furnished at each end with arrangements for the usual movements in both horizontal and vertical directions.

The **tripod head** is similar to that in the transit.

333. Adjustments.

1. To adjust the line of collimation, set the tripod firmly, remove the Y pins from the clips, so that the telescope shall turn freely, clamp the instrument to

THE Y LEVEL.



the tripod head, and by means of the leveling and tangent screws, bring either of the wires to bear on a clearly marked edge of an object, distant from two to five hundred feet.

Turn the telescope half-way round, so that the same wire is brought to bear on the same object.

Should the wire not range with the object, bring it half way back by moving the capstan head screws, *EE*, at right angles to it, in the opposite direction, on account of the inverting property of the eye-piece, and repeat the operation till it will reverse correctly.

Proceed in like manner with the other wire.

Should both wires be much out, adjust the second after having nearly completed the adjustment of the first, then complete the adjustment of the first.

To bring the intersection of the wires into the center of the field of view, slip off the covering of the eye-piece centering screws, shown at *LL*, and move, with a small screw-driver, each pair in succession, with a direct motion, as the inversion of the eye-piece does not affect this operation, till the wires are brought, as nearly as can be judged, into the required position.

Test the correctness of the centering by revolving the telescope and observing whether it appears to shift the position of an object.

If the position of the object is shifted by revolving the telescope, the centering is not perfectly accomplished.

Continue the operation till the centering is perfect.

2. To adjust the level bubble, clamp the instrument over either pair of leveling screws, and bring the bubble to the middle.

Revolve the telescope in the Y's so as to bring the level tube on either side of the center of the level bar.

Should the bubble run to one end, rectify the error by bringing it, as nearly as can be estimated, half-way back with the capstan screws in the level holder.

Again bring the level over the center of the bar, and bring the bubble to the center; turn the level to one side, and, if necessary, repeat the operation till the bubble will keep its position when the tube is turned to either side of the center of the bar.

Now bring the bubble to the center with the leveling screws, and reverse the telescope in the Y's without jarring the instrument. Should the bubble run to either end, lower that end, or raise the other by turning small adjusting nuts at one end of the level till, by estimation, half the correction is made.

Again bring the bubble to the middle, and repeat the operation till the reversion can be made without causing any change in the bubble.

3. To adjust the Y's, or to bring the level into a position at right angles with the vertical axis, so that the bubble will remain in the center during an entire revolution of the instrument, bring the level tube directly over the center of the bar, and clamp the telescope in the Y's, placing it, as before, over two of the leveling screws, unclamp the socket, level the bubble, and turn the instrument half-way around, so that the level bar may occupy the same position with respect to the leveling screws beneath.

Should the bubble run to either end, bring it half-way back by the Y nuts on either end of the bar.

Now move the telescope over the other set of leveling screws, bring the bubble again into the center, and proceed as before, changing to each pair of screws successively, till the adjustment is nearly completed, which may now be done over a single pair of screws.

334. The Use of the Level.

Set the legs firmly in the ground, test the adjustments, making corrections if necessary.

Bring the wires precisely in the focus, and the object distinctly in view, so that the spider lines will appear fastened to the surface of the object, and will not change in position however the eye be moved.

The bubble resting in the middle, the intersection of the spider lines will indicate the line of apparent level.

335. Leveling Rod.

The New York Leveling Rod, represented in the engraving with a piece cut out of the middle, so that both ends may be exhibited, consists of two pieces, one sliding from the other.

The graduation commences at the lower end, which is to rest on the ground, and is made to tenths and hundredths of a foot.

A circular target, divided into quadrants of different colors, so as to be easily seen, moves on the front surface of the rod, which reads to six and one-half feet.

If a greater height is required, the horizontal line of the target is fixed at $6\frac{1}{2}$ feet, on the front surface, and the upper part of the rod, which carries the target, is run out of the lower, and the reading is obtained on the graduated side up to an elevation of twelve ft.

A clamp screw on the back is used to fasten the rods together in any position.



336. Definitions.

A level surface is the surface of still water, or any surface parallel to that of still water.

Such a surface is convex, and conforms to the spheroidal form of the earth.

A level line is a line in a level surface.

The difference of level of two places is the distance of one above or below the level surface passing through the other.

Leveling is the art of ascertaining the difference of level of two places.

The apparent level of any place is the horizontal plane tangent to the level surface at that place.

The line of apparent level of any place is a horizontal line, tangent to a level line at that place.

The Y Level indicates the line of apparent level and not the true level, which is a curved line.

The correction for curvature is the amount of deviation for a given distance of the line of apparent level from the line of true level to which it is tangent at the point from which the distance is measured.

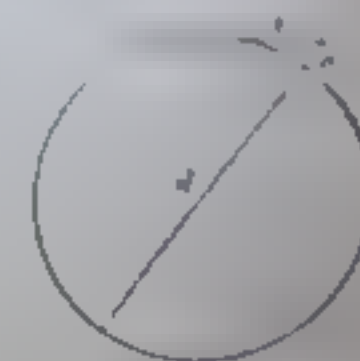
337. Problem.

To compute the correction for curvature.

Let t denote the tangent, c the correction for curvature, d the diameter of the earth.

Then, by Geometry, we have,

$$(d + c)c = t^2, \quad \therefore c = \frac{t^2}{d + c}$$



Since c is very small compared with d , it can be dropped from the denominator without sensibly affecting the result.

$$\therefore c = \frac{l^2}{d}$$

The arc, which is the distance measured, will not differ perceptibly from the tangent, for all distances at which observations are made, and may be substituted for it.

Calling another distance, l' , and the corresponding correction, c' , we have,

$$c' = \frac{l'^2}{d} \quad \therefore c : c' :: l^2 : l'^2$$

1. The correction for curvature, for a given distance, is equal to the square of the distance divided by the diameter of the earth.

2. The corrections for different distances are to each other as the squares of the distances.

Let us find the correction for the distance 100 chains, calling the diameter of the earth 7920 inches.

$$c = \frac{100^2}{7920} = \frac{65}{80} = 12\frac{1}{2} \text{ inches.}$$

The correction for any other distance, for example, 5 ch., can be found from the proportion.

$$100^2 : 5^2 :: 12\frac{1}{2} : c, \therefore c = .031 \text{ inches.}$$

For 1 mile, $100^2 : 80^2 :: 12\frac{1}{2} : c, \therefore c = 8 \text{ inches.}$

For m miles, $1^2 : m^2 :: 8 : c, \therefore c = 8 m^2 \text{ in.}$

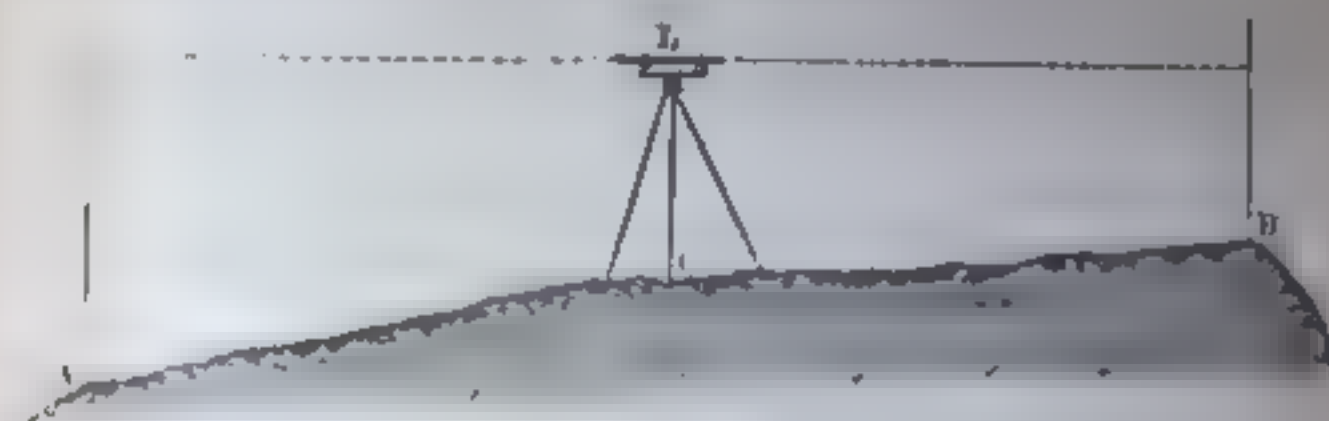
A correction for refraction is sometimes made by diminishing the correction for curvature by $\frac{1}{7}$ of itself.

If the leveling instrument is placed midway between the two places whose difference of level is to be found, the curvature and refraction on the two sides of the

instrument balance, and the difference of apparent level will be the difference of true level.

338. Problem.

To find the difference of level of two places visible from a point midway between them or from each other, when the difference of level does not exceed twelve feet.



Let A and B be the two places, and C the place midway from which both are visible.

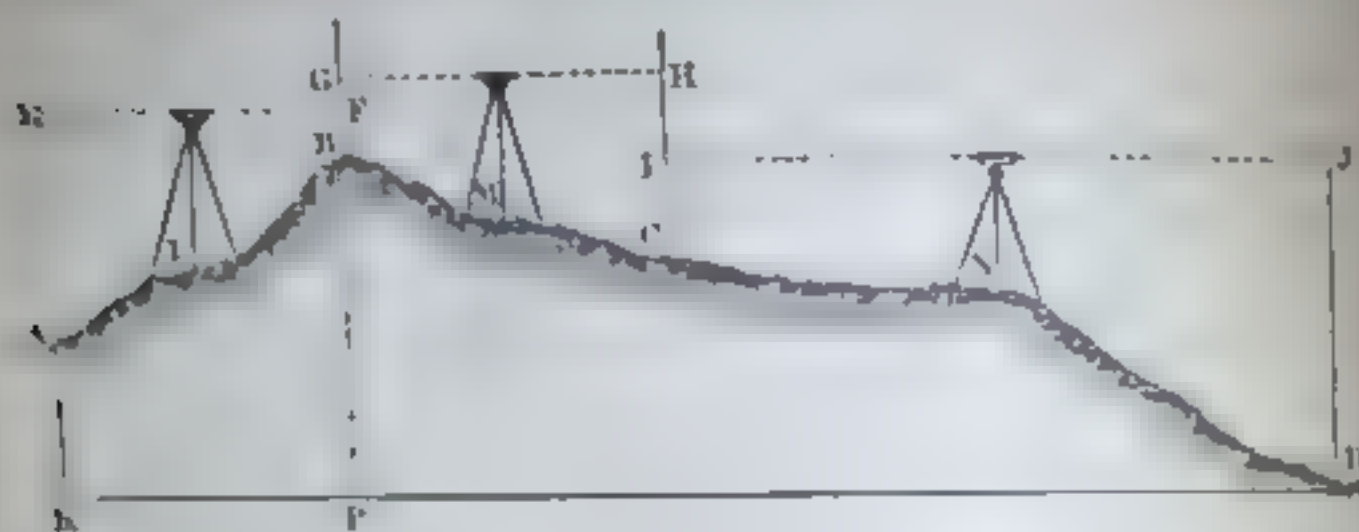
Place the level at C , and let the rod-man set up the leveling rod at A , and slide the vane till he learns, by signal from the surveyor at the level, that its horizontal line is in the line of apparent level. Let the height be accurately observed and noted, and the rod be transferred to B , and the height observed and noted as before.

The difference of these heights will be the difference of level.

If a gully intervene, so that the line of apparent level, from the intermediate station, would not cut the rod, place the instrument at one station, and take the height on the staff at the other station marked by the vane when in the line of apparent level, from which subtract the height of the instrument, and the difference corrected for curvature and refraction will be the difference of level required.

339. Problem.

To find the difference of level of two places which differ considerably in level, or which can not be seen from each other.



Let *A* and *D* be the places whose difference of level is required.

Place the level at the station *L*, midway between two convenient points, *A* and *B*. Take the backsight to *A*, and note the height of *E*. Send the rod to *B*, and note the height of the foresight at *F*. Remove the level to *M*, note the height of the backsight at *G* and the foresight at *H*. Remove the level to *N*, note the height of the backsight at *I*, and the foresight at *J*.

Then will the difference of the sum of the backsights and the sum of the foresights be the difference of level of *A* and *D*.

For, we find for the sum of the backsights,

$$AE + BG + CI = AE + BF + FG + CI.$$

And, we find for the sum of the foresights,

$$BF + CH + DJ = BF + CI + IH + DJ \\ BF + CI + PG.$$

The sum of the backsights, minus the sum of the foresights, $AE + FG - PG = AK$ difference of level, which in the field notes is denoted by *D. L.*

If the sum of the foresights exceeds the sum of the backsights, the point *D* is below *A*; if the reverse were true, the point *D* would be above *A*, as indicated by the sign.

It is not essential that the intermediate stations be directly between the places.

340. Field Notes.

Stations.	Backsights.	Foresights.
1	5.40	1.50
2	3.12	5.25
3	2.40	8.16
Sums ...	10.92	14.91
	14.91	
<i>D. L.</i>	— 3.99	

341. Leveling for Section.

Leveling for Section is leveling for the purpose of obtaining a section or profile of the surface along a given line.

A Bench-mark is made to indicate the beginning of the line by drilling a rock or driving a nail into the upper end of a post. Such marks should be made at different points along the line, to serve as checks in case of a new survey.

It is necessary also to measure the distance between the stations. The bearings of the lines should be taken in case a map or plot is to be made, representing the horizontal surface.

In the following table of specimen field notes, *S.* denotes stations; *B.*, bearings; *D.*, distances; *B. S.*, backsights; *F. S.*, foresights; *B. S. — F. S.*, backsights minus foresights; *T. D. L.*, total difference of level; *R.*, remarks, and *B. M.*, bench-mark.

The numbers in the column headed *B. S. — F. S.* are obtained by subtracting each foresight from the corresponding backsight, observing to write the proper sign.

The numbers in the column headed *T. D. L.* are obtained by continued additions of the numbers in the column *B. S. — F. S.*, each being the sum of the backsights minus the sum of the foresights, up to a given point, expresses the distance of that point above or below the bench-mark at the beginning of the line.

The minus sign of a result indicates that the sum of the foresights exceeds the sum of the backsights, and hence, that the corresponding station is below the first station; the plus sign indicates the reverse.

In order to bring out prominently the difference of level, the vertical distances are usually plotted on a much larger scale than the horizontal.

Let us suppose the numbers in the column *D.* express chains, and that the numbers in the following columns express feet.

In the following profile section the horizontal distances are plotted to the scale of 20 chains to an inch, and the vertical distances to the scale of 20 feet to an inch.

The profile of the section is therefore distorted, the vertical distances being 60 times too great to exhibit their true proportion to the horizontal distances.

The horizontal line, *AG*, through the point of beginning is called the *datum line*.

342. Field Notes.

<i>S.</i>	<i>B.</i>	<i>D.</i>	<i>B. S.</i>	<i>F. S.</i>	<i>B. S. — F. S.</i>	<i>T. D. L.</i>	<i>R.</i>
1	N.	10.00	3.25	11.63	— 8.38	— 8.38	BM. on post
2	N.	14.00	4.80	10.20	— 5.40	— 13.78	
3	N.	8.25	12.00	1.40	+ 10.60	— 3.18	BM. on rock.
4	N. 10° E.	12.00	10.80	2.30	+ 8.50	+ 5.32	
5	N. 10° E.	10.75	1.18	12.00	— 10.82	— 5.50	
6	N.	10.00	2.15	8.40	— 6.25	— 11.75	BM. on oak

343. Profile of Section.



SURVEYING RAILROADS.

344. General Plan.

The surveys for the construction of railroads, applicable also to canals, graded pikes, dikes, etc., are made in the following order.

1. The reconnoissance, to locate the route. The termini being agreed upon, sometimes several routes are examined, so that an approximate judgment can be formed in reference to the economy of construction and purchasing the right of way, the amount of stock taken at different towns along the route, and the profits from local business.

2. The transit survey, to determine definitely the

middle line along the surface, after the route has been decided upon by the preliminary reconnoissance.

3. **The section leveling**, to determine the profile of the middle line along the surface.

4. **The cross-section work**, to determine the position and slopes of the sides, so that the amount of earth to be removed or filled can be estimated.

345. Section Leveling.

Section leveling is simply an application, with slight modifications, of leveling for section, before described.

The first bench-mark is assumed at some convenient point near the beginning of the line, and its location described in the column of remarks.

The datum line is generally assumed at such a depth below the first bench-mark—for example, at mean high-tide water, in case one end of the route is in the vicinity of tide-water—that its whole length shall be below the section line at the surface.

The engineer's chain, 100 feet in length, is usually employed in taking the horizontal distance.

A turning-point is a hard point chosen as far in advance as possible, but not necessarily in exact line, upon which the rod rests while a correct reading is taken just before it is necessary to change the position of the instrument, whose exact height above the datum line thus becomes known in the new position.

The difference between a turning-point and a bench is this:

A turning-point is merely a temporary point, neither marked nor recorded, used to determine the height of

the instrument in a new position. A bench is both marked and noted, and thus made permanent.

If, however, it is thought best to make a turning-point permanent, it is marked and recorded, and becomes a bench.

In order that a bench be not destroyed in constructing the road, it should be a little removed from the line surveyed. The location of the benches should be carefully noted, so that they may be readily found from the field notes.

The plus sights are the first readings of the rod, made after each new position of the instrument, as the rod stands on a bench or turning-point, and are taken to thousandths of a foot.

The minus sights are the other readings, and are taken to tenths, except the last minus sight, before the position of the instrument is changed, which, being taken as the rod stands on a turning-point or bench, is taken to thousandths.

The height of the instrument above the datum line is equal to a plus sight, plus the height of the corresponding bench or turning-point.

The height of the surface above the datum line, at any position of the rod, is equal to the height of the instrument, minus the corresponding backsight.

These heights are taken at intervals of 1 chain, and at intermediate points where the irregularity of the surface is deemed sufficient to render it important.

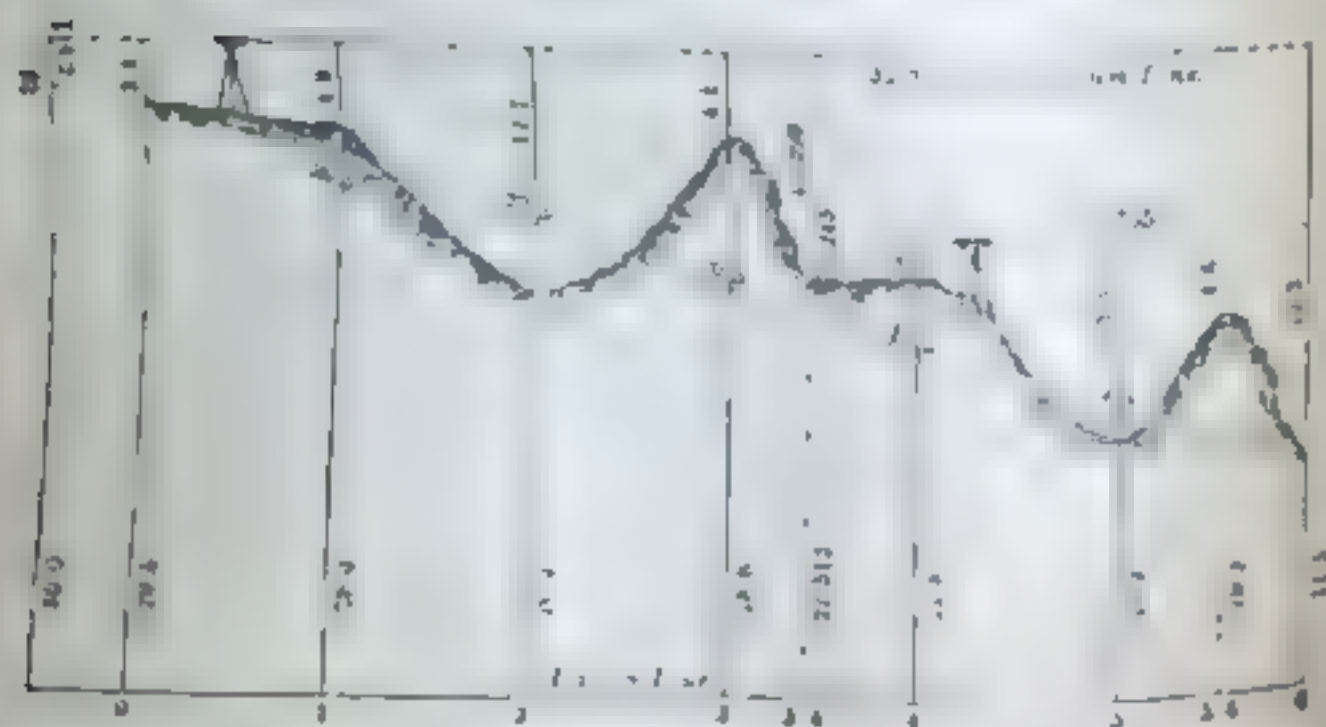
In the following field notes *D.* denotes distance; *B.* bench; *T. P.*, turning-point; *+ S.*, plus sight; *H I.*, height of instrument; *— S.*, minus sight; *S. H.*, surface height; *G. H.*, grade height; *C.*, cut; *F.*, fill; *R.*, remarks.

346. Field Notes.

D	S	H I	— S	S H	G H	C	F	R.
B	2 01	32 911		30				B. 50 ft.
0			34	29.5	29.5			E. of
1			49	28.0	26.5	1.5		0 stake
2			12.7	20.2	23.5		3.3	
3			41	28.8	20.5	8.3		
T. P.	2 243	23 755	11 399	21.512	19.2	2.3		
4			20	21.8	17.5	4.3		
5			12.5	11.3	14.5		1.2	
5.6			46	19.2	12.7			
6			12.3	11.5	11.5			

The numbers in the horizontal column, *T. P.*, are found thus: The — *S.*, 11.399, is obtained from the first position of the instrument by the reading of the rod on *T. P.* $21.512 = 32.911 - 11.399$. The + *S.*, 2.243, is the reading of the rod from the new position of the instrument. $23.775 = 21.512 + 2.243$. The cutting or filling is the difference of *S. H.* and *G. H.*

347. Profile of Section and Grade.



348. Remarks.

1. The grade height at 0, minus the grade at 6, which is $29.5 - 11.5 = 18$, the descent from 0 to 6. $18 \div 6 = 3 =$ the descent for 1 chain, $29.5 - 3 = 26.5 =$ *G. H.* at 1; $26.5 - 3 = 23.5 =$ *G. H.* at 2, etc.

2. The establishment of the grade is influenced by the object of the work, economy, the balance of cuttings and fillings, the points desirable for termini, etc.

3. The method exhibited above may be extended to any distance.

349. Example.

Fill out the notes of the following table, and make a profile of section and grade from *S. H.* at 0 to *S. H.* at 5.

D	S	H I	— S	S H	G H	C	F	R.
B	6 218	36 248		30				B. 20 ft.
0			5.3					S. of 0.
1			9.8					
2			2.3					
T. P.	10 718		11 811					
3			7.6					
4			12.0					
5			2.1					

350. Cross-Section Work.

Excavations and embankments are constructed with sloping sides, in order to prevent the sliding of earth down the surface.

The ratio of slope is the vertical distance divided by the horizontal, and is therefore the tangent of the angle which the sloping surface makes with a horizontal plane.

The usual ratio of slope is $\frac{3}{4}$, and the angle $33^\circ 41'$.

Slope stakes are driven to mark where the sloping surface, whether of cutting or filling, will intersect the surface, and thus indicate the boundaries of the work.

The rod used in cross-section leveling is 15 feet long, graduated and plainly marked to feet and tenths, and is held by the leveler at the instruments.

The assistants of the leveler are the rodman, arborer, and two tapemen.

The Field book is ruled into four columns, headed *D.* for distance; *L.* for left; *C. C.* for center-cut; *R.* for right.

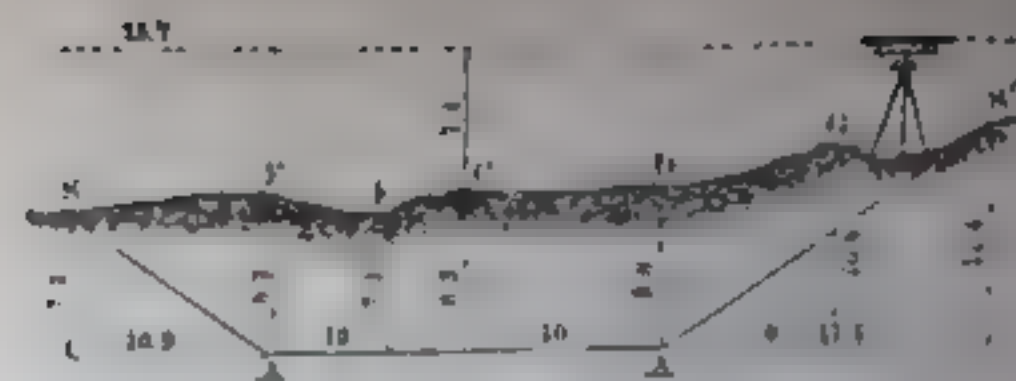
The numbers in the columns *D.* and *C. C.* are, respectively, the distance and the corresponding cut, or fill marked minus cut, taken from the field book for section leveling.

The fractions in the columns *L.* and *R.* have for their numerators the vertical distances of the cross-section, and for their denominators, the corresponding horizontal distances, from the center or from the vertex of the angle of slope, according as the vertical distance is taken within or without the limits of the horizontal portion of the road.

351. Cross-Section Excavations.

We give the following profile of cross-section, the method of performing the field operations and recording the notes.

Let us suppose the cross-section to be taken at the distance 3 of the field notes of article 341, where the center cut is 8.3; that the road bed is 20 feet wide, that the ratio of slope is $\frac{3}{4}$, and that both horizontal and vertical distances are plotted to the scale of 20 feet to 1 inch.



Take *AA'* for the datum line, and suppose the reading at the center stake to be 7.4. The height of the instrument above the datum line is therefore $8.3 + 7.4 = 15.7$.

The reading of the rod at the depression *F*, between the center and the angle *A*, is 8.5; hence, the cut is $15.7 - 8.5 = 7.2$. The horizontal distance, *CF*, is 4 feet; hence, the record in the field notes, as seen in the next article in the column *L*, is $\frac{7.2}{4}$.

The reading of the rod, at the temporary stake *E*, is 7.4; hence, the cut is $15.7 - 7.4 = 8.3$, and the entry, $\frac{8.3}{A}$.

The point *S*, where the slope intersects the surface, is found by trial. Since the vertical distance of the slope is $\frac{3}{4}$ of the horizontal, then *ES*, if horizontal, would be $\frac{3}{4}$ of *EA*, which is 12.4; but, on account of the inclination of the surface, *ES* will be less, say 10 feet. Setting the rod 10 feet out from *E*, the reading is 8.3, and hence the cut $= 15.7 - 8.3 = 7.4$. Now, $\frac{3}{4}$ of 7.4 is 5.55; hence, the assumed distance, 10 feet, is too small.

For a second trial, take 11 feet out from *E*, at which the reading of the rod is 8.4, and the cut 7.3. Now, $\frac{3}{4}$ of 7.3 is 5.475, which lacks but .1 of 11, and is sufficiently accurate. The record for the slope stake, in the column *L*, is $\frac{7.3}{10.9}$.

The reading of the rod at the stake D is 6.9; hence, the cut is 8.8, and the record in the column R is $\frac{8.8}{4}$.

The reading at the elevation G is 5.1; hence, the cut is 10.6. The horizontal distance, DG , is 9 feet; hence, the record is $\frac{10.6}{9}$.

To find S' where the slope intersects the surface, since, on account of the rising of the surface, it is more than $\frac{1}{2}$ of 8.8, which is 13.2, take, for a first trial, 18 feet out from D , at which point the reading of the rod is 4.5, and hence the cut $15.7 - 4.5 = 11.2$. Now, $\frac{1}{2}$ of $11.2 = 5.6$; hence, 18 feet is too far out.

For a second trial, take 17 feet out from D . The reading of the rod is 4.3, and the cut $15.7 - 4.3 = 11.4$. Now, $\frac{1}{2}$ of $11.4 = 5.7$, which is sufficiently accurate; hence, the record for the slope stake S' , in the column R , is $\frac{11.4}{17.1}$.

352. Field Notes.

D	L		C	C'	R
3	7.3	8.3	7.2	8.3	$\frac{8.8}{4}$
	10.9	4			$\frac{11.4}{17.1}$

353. Cross-Section Embankments.

The following is the profile of the cross section drawn to a scale of 20 feet to 1 inch, taken at the distance 5 of the field notes of article 346, where the filling is 3.2, now called a minus cut, and written -3.2 .

Take AA' , which is the horizontal top of the embankment 20 feet wide, for the datum line.



The ratio of slope, in case of embankments, is $\frac{1}{2}$.

The reading of the rod at the center stake is 6.6, and the height of the instrument, with reference to the datum line, is the algebraic sum of the reading of the rod and the minus cut, which is $6.6 - 3.2 = 3.4$.

If the instrument should be below the datum line, the reading of the rod would be numerically less than the minus cut, and the height of the instrument would be negative.

The readings of the other points along the surface SS' , subtracted from the height of the instrument, will give the corresponding minus cuts.

The reading at A is 7.4, the cut, -4 , and the record, $\frac{-4}{A}$.

The reading at G is 12.4, the cut, -9 , the horizontal distance FG , 6.3, and the record, $\frac{-9}{6.3}$.

To find the position of the slope stake S , take for the first trial 20 feet out from F , where the reading is 16, and the cut, -12.6 . Now, $-12.6 \times -\frac{1}{2} = 6.3$; hence 20 feet is too far out.

Next try 18 feet out, where the reading is 15.5, and the cut, -12.1 . Now, $-12.1 \times -\frac{1}{2} = 6.05$, which is sufficiently accurate; hence, the record for the slope stake S is $\frac{-12.1}{18.1}$.

The reading at A' is 6.4, the cut, -3 , and the record, $\frac{-3}{.4}$.

To find the position of the slope stake S' , take for the first trial 5 feet out from D , where the reading is 6.2, and the cut, -2.8 . Now, $-2.8 \times -\frac{1}{4} = .7$; hence, 5 feet is too far out.

Next take 4 feet out, where the reading is 6.1, and the cut, -2.7 . Now, $-2.7 \times -\frac{1}{4} = .675$; hence, the record for the slope stake S' is $\frac{-2.7}{.4}$.

354. Field Notes.

D	L	C	C'	R
5	12.1	9	4	-2.7
	18.1	6.3	.4	4

355. Remark.

It sometimes occurs that an excavation will be required on one side, and an embankment on the other. Guided by the stakes and field notes, the excavations and embankments can be correctly made.

356. Computation of Earth-work.

The computation of earth-work is the determination of the volume of excavation or embankment.

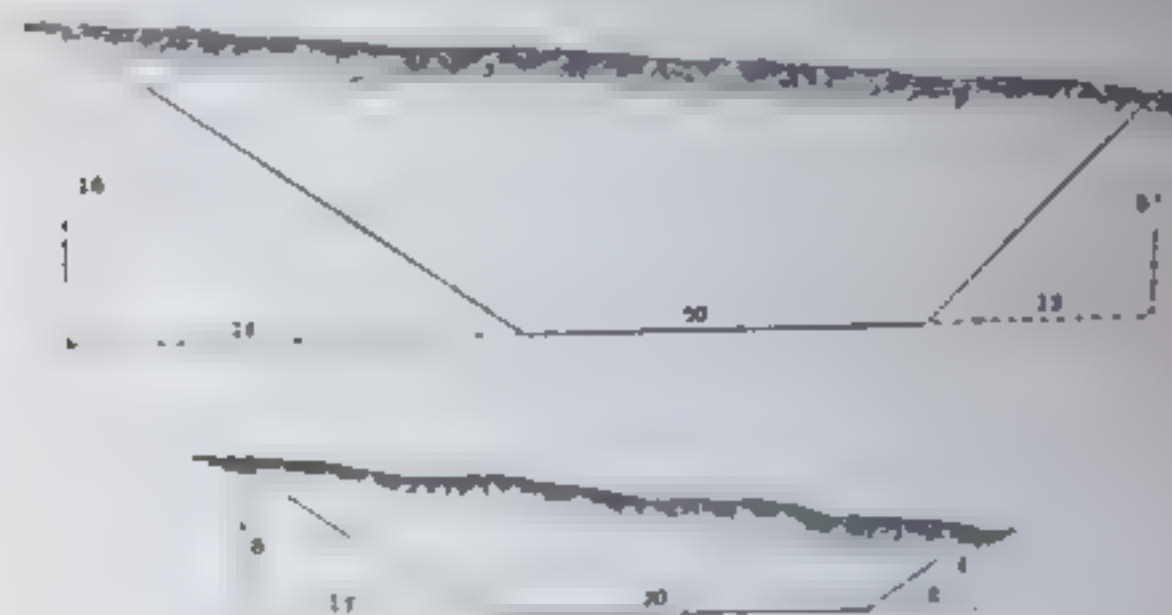
The cross-sections, being taken, wherever necessary, at every 100 feet or less, divide the excavations or embankments into blocks, which may be regarded as frustums of pyramids.

Denoting the areas of the sections regarded as bases of the frustum by b and b' , respectively, the length by l , and the volume by v , we have the formula,

$$v = \frac{1}{3} l (b + b' + \sqrt{bb'}).$$

357. Examples.

1. The length of an excavation is 100 feet; find the volume, the two ends being thus represented:



The area required, in each case, is the area of the whole figure, regarded as a trapezoid, which is one-half the altitude multiplied by the sum of the parallel bases, minus the sum of the two triangles; hence,

$$b = 28 \times 24 - (24 \times 8 + 12 \times 4) = 432.$$

$$b' = 19 \times 12 - (12 \times 4 + 6 \times 2) = 168.$$

$$v = \frac{1}{3} \times 100 (432 + 168 + \sqrt{432 \times 168}).$$

$$v = 28980 \text{ cubic feet} = 1073 \text{ cubic yards.}$$

2. Compute the volume of the embankment whose horizontal breadth at the top is 16 feet, from the following field notes:

$$S \quad N \quad A$$

D	L	C. C.	R.
5	11.6	-10.5	-9.5
	17.4	.1	.13
6	-17.4	-15.5	14.2
	26.1	.4	.19.5

Ans. 1607 cu. yds.

358. Remarks.

1. The above method of computing earth-work is called by engineers *The mean average method*.

2. The method known as *The arithmetical mean method* is easier than the above, though less accurate.

The following is the formula:

$$v = \frac{1}{2} l (b + B)$$

3. The volume can also be computed as a rectangular prismoid.

4. Irregularities in the cross-section surface line, as elevations, depressions, or a curvature of the line, must be considered.

Thus, the elevation may be regarded as a triangle, its area computed and added to the trapezoid before the area of the two triangles at the right and left be deducted.



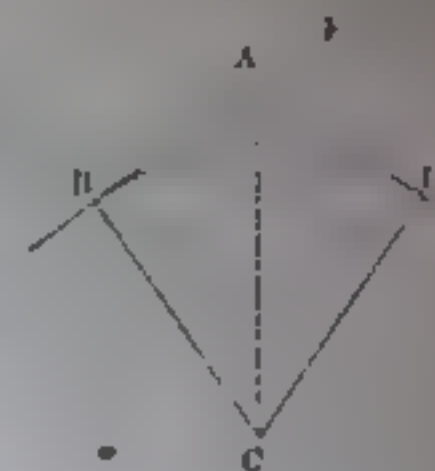
359. Railroad Curves.

In the preliminary survey of a railroad, any change in direction is made by an angle which must, in the final survey, be replaced by a curve, to which the sides of the angle are tangents.

Let the annexed diagram represent such an angle and curve.

Run out one of the tangents, as *B.A.*, to *E*, and let *A* denote the external angle *EAD*.

Then we shall have $C = A$, since each is the supplement of *BAD*, the angles *B* and *D* being right angles.



Let $r = BC$, the radius of curvature, and $t = AB$, the tangent.

$$\text{Then, (1) } t = r \tan \frac{1}{2} A, \quad (2) \quad r = \frac{t}{\tan \frac{1}{2} A}$$

The **degree of curvature** is the number of degrees in an arc whose length is 1 chain or 100 feet.

360. Problem.

Given the degree of curvature, to find the radius; and, conversely, given the radius of curvature, to find the degree.

$2\pi r =$ the circumference,

$$\frac{2\pi r}{360} = \frac{\pi r}{180} = 1^\circ \text{ of circumference,}$$

$$\frac{d\pi r}{180} = d^\circ \text{ of circumference.}$$

$$\text{Hence, } \frac{d\pi r}{180} = 100. \quad \therefore \begin{cases} (1) \quad r = \frac{18000}{d\pi} \\ (2) \quad d = \frac{18000}{\pi r} \end{cases}$$

Having found the radius of curvature, we can find t , the tangent, or the distance from the vertex of the angle to the point where the curve begins by formula (1) of the preceding article.

361. Examples.

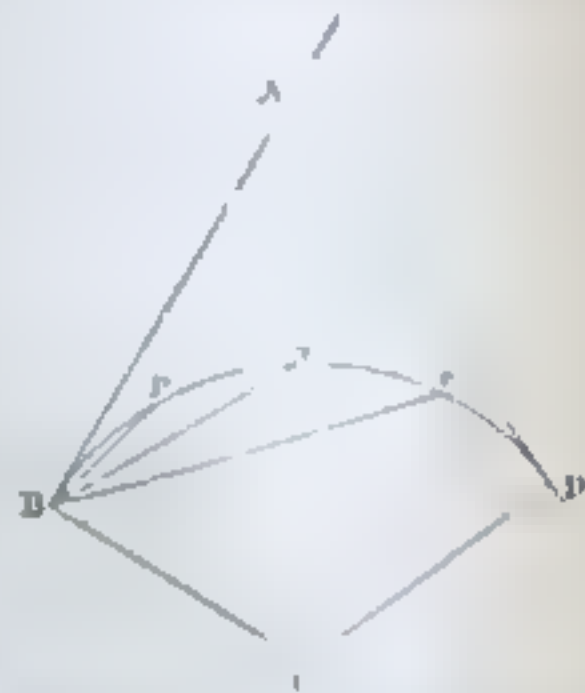
1. Find r of 1° of curvature and l , if $A = 40^\circ$.
Ans. $r = 5729.58$ ft., $l = 2087.4$ ft.
2. Find r of 2° of curvature and l , if $A = 40^\circ$.
Ans. $r = 2864.79$ ft., $l = 1043.7$ ft.
3. Find r of 3° of curvature and l , if $A = 50^\circ$.
Ans. $r = 1909.86$ ft., $l = 890.6$ ft.
4. Find r and d , if $A = 35^\circ$ and $l = 1000$ ft.
Ans. $r = 3171.6$ ft., $d = 1^\circ 48' 23''$.
5. Find r and d , if $A = 100^\circ$ and $l = 1$ mile.
Ans. $r = 4430.4$ ft., $d = 1^\circ 17' 35''$.

362. Location of the Curve.

First Method.

Let each of the arcs, Bp , pq , qr , ... be 1 chain, then will the number of degrees in each, or in the corresponding angle at the center, be equal to d , the degree of curvature.

The angle ABp , formed by a tangent and a chord, is measured by one-half the arc Bp , and is therefore equal to $\frac{1}{2}d$.



Each of the inscribed angles, pBq , qBr , is measured by one-half the intercepted arc, and is therefore equal to $\frac{1}{2}d$.

Having determined the point B , where the curve begins, the transitman sets his instrument at this point, and directs it to A . He then turns it an angle equal to $\frac{1}{2}d$, on the side toward the curve.

The chainmen then take the chain, the follower placing his end at B , and the leader drawing out the chain at full length toward A , is directed by the transitman into line so as to locate the point p , at which the axman drives a stake.

The transitman again turns his instrument an angle equal to $\frac{1}{2}d$, the chainmen advance, the follower placing his end of the chain at p , the leader again drawing out the chain at full length, is directed by the transitman so as to locate the point q , at which the axman drives a stake, and so on.

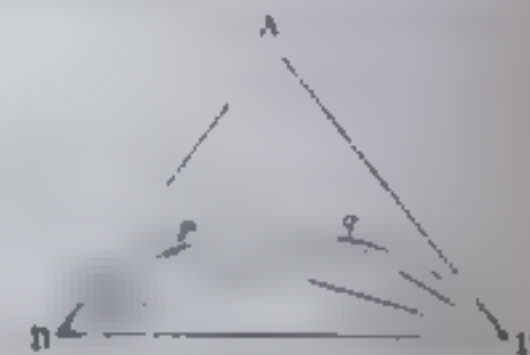
The last distance will usually not be 1 chain; but if n be the number of preceding deflections, the last angle of deflection, since the sum of all the deflections is equal to $\frac{1}{2}C = \frac{1}{2}A$, will be equal to

$$\frac{1}{2}A - \frac{1}{2}dn.$$

It is to be observed that the chord is made equal to 1 chain instead of the arc; but as the radius is much greater than the chord, the arc and chord will not differ materially, and no appreciable error arises in practice.

Second Method.

Points on the curve may be located by the use of two transits, without the use of the center, as may be desirable, in case the curve is to be located in marshy ground or shallow water.



Let one transit be placed at B and another at D , the extremities of the curve.

Direct the transit at B to A , the one at D to B , then turn each to the right an angle equal to $\frac{1}{2}d^\circ$.

The intersection of the lines will determine p , where the axman, directed by both transitmen, drives a stake.

In like manner other points can be located.

If A is visible from D , but not B , direct the transit at D to A ; then, to locate p , turn it to the left an angle equal to $\frac{1}{2}A^\circ - \frac{1}{2}d^\circ$.

To locate q , turn the transit at D from p to the right an angle equal to $\frac{1}{2}d^\circ$, or from A to the left an angle equal to $\frac{1}{2}A^\circ - d^\circ$, and the transit at B to the right from p an angle equal to $\frac{1}{2}d^\circ$, or to the right from A an angle equal to d° , and so on.

Third Method.

Let B be the point where the curve begins. Take Bm equal to 1 chain. Then, to find the length of the offset mp , complete the circle, draw the diameter BE , let fall the perpendicular pn to BE , and draw pE .

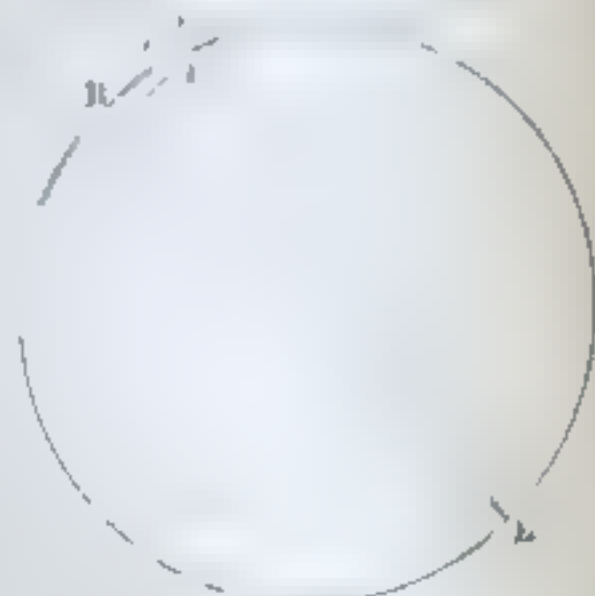
In the right triangle BpE , Bp is a mean proportional between BE and Bn ; hence, $BE \times Bn = Bp^2$; but $BE = 2r$, $Bp = 1$, and $Bn = mp$,

$$mp = \frac{1}{2r}.$$

To find q , produce Bp till $pm = 1$ chain, and draw tr , tangent to the curve at p .

Then, $spv = tpB = mBp = rjq$.

For the first and second are vertical, and all the rest are included between tangents and equal chords.



$\therefore sq = 2mBp$, \therefore the arc $sq - 2$ arc mp ,

Or, the arcs being small, do not differ materially from their chords,

$$\therefore sq = 2mp = \frac{1}{r}.$$

Hence, to locate a curve by this method without the transit, commence at B , where the curve is to begin, take $Bm = 1$ chain in the direction of the straight track, make the offset $mp = \frac{1}{2r}$, produce Bp till $pm = 1$ chain, make the offset sq equal to twice the first offset, produce pq till the produced part $= 1$ chain, make an offset equal to the last, and so on.

Fourth Method.

It is evident from the diagram that

$$mp = BC - nC.$$

But $BC = r$, and $nC = \sqrt{r^2 - t^2}$.

$$\therefore mp = r - \sqrt{r^2 - t^2}.$$

By giving to t different values, other points of the curve can be determined.



Fifth Method.

It is evident from the diagram that

$$mp = mC - Cp.$$

But $mC = \sqrt{r^2 + t^2}$, and $Cp = r$.

$$\therefore mp = \sqrt{r^2 + t^2} - r.$$

In this method the offset is not made at right angles to the tangent, but in a direction toward the center, which is supposed to be visible from m .



The preceding methods apply to points of the curve 1 chain or 100 feet from each other, which will be sufficient for the excavations or embankments.

Before laying the track, stakes are driven at points on the curve, distant from each other about 10 feet.

363. Problem.

To locate intermediate points on the curve.

Let the diameter in the diagram be parallel to the chord, which is equal to 1 chain = 100 feet, the ordinates $a, b, c, d, e, f, e, d, c, b, a$ be 10 feet from each other, and $v, w, x, y, z, y, x, w, v$ be offsets from the chord to the curve, corresponding to the ordinates $b, c, d, e, f, e, d, c, b$.



The square of an ordinate is equal to the rectangle of the segments into which it divides the diameter.

$$a^2 = (r - 50)(r + 50), \quad a = \sqrt{(r - 50)(r + 50)}.$$

$$b = \sqrt{(r - 40)(r + 40)}, \quad v = b - a$$

$$c = \sqrt{(r - 30)(r + 30)}, \quad w =$$

$$d = \sqrt{(r - 20)(r + 20)}, \quad x = d - a.$$

$$e = \sqrt{(r - 10)(r + 10)}, \quad y = e - a.$$

$$f = r, \quad z = f - a.$$

364. Example.

Find the radius of a 1° curvature, and the offsets from the chord of 100 feet to the curve.

$$\text{Ans } \begin{cases} r = 5729.58 \text{ ft.}, & v = .08 \text{ ft.}, & w = .14 \text{ ft.} \\ x = .19 \text{ ft.}, & y = .21 \text{ ft.}, & z = .22 \text{ ft.} \end{cases}$$

TOPOGRAPHICAL SURVEYING.

365. Definition and Method.

Topographical surveying is that branch in which the form of the surface, the situation of ponds, streams, marshes, rocks, trees, buildings, etc., are considered and delineated.

The surface is supposed to be intersected by horizontal planes equally distant from each other, and the curves formed by the intersection of the planes and the surface projected on a horizontal plane.

These projections will be nearer together or farther apart, according as the slope of the surface approaches a vertical or a horizontal position.

The operations are of two kinds—*field operations* and *plotting*.

366. Field Operations.

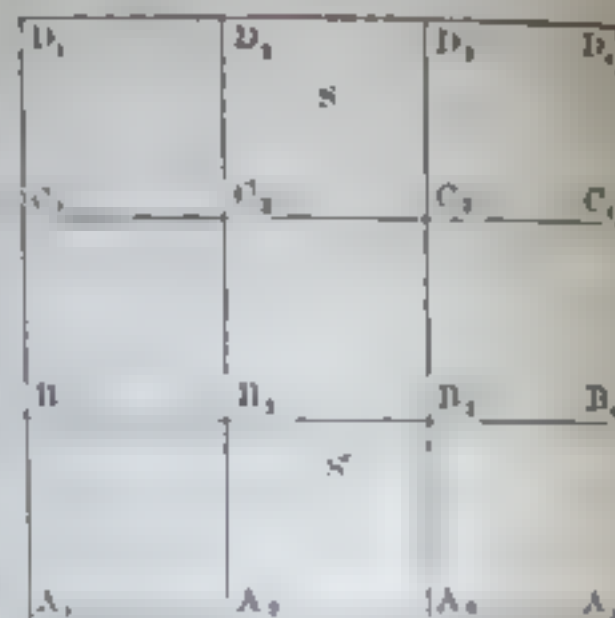
Field operations consist in finding and recording points of the curves of intersection of the surface and the horizontal planes, the course of streams, and the situation of noteworthy objects on the surface.

Range with the level, or transit theodolite, which is more convenient in topographical operations, stakes marked as in the annexed diagram, and cause them to be driven into the ground, at a horizontal distance from each other of 100 feet or less, varying with the inequality of the surface and the degree of accuracy with which it is desirable that the work be executed.

Find by the eye, or by the instrument if necessary, the lowest point in the field, at which make a *permanent bench-mark*, and assume for the plane of reference the

horizontal plane passing through this point, which we will suppose to be C_1 .

Place the instrument at some convenient station, S , from which take the reading of the rod at C_1 , which suppose to be 10.378, and enter this as a backsight in the field notes.



Take the readings of the rod at as many stakes as possible from the station S . Suppose these readings to be C_2 , 6.481; C_3 , 1.214; D_1 , 8.235; D_2 , 6.378; D_3 , 4.102; D_4 , 2.304, and enter these readings in the field notes as foresights, placing the smallest reading, C_3 , last.

At C_3 drive a small stake for a check.

Subtract the foresight C_2 , 6.481 from the backsight 10.378, and enter the difference in the column of difference, headed D ; also in the column of total difference of level above C_1 , headed $T. D. L.$

Subtract each of the remaining foresights from the next preceding one, and enter the results, with their proper signs, in the column D .

Add each result to the previous total difference of level, and enter the results in the column $T. D. L.$

The total difference of level for C_3 is also found by subtracting the foresight of C_3 from the backsight of C_1 , which, compared with the result before found, will serve as a check.

Move the instrument to S' , and take a backsight to the check stake C_3 , and the foresights to as many of the remaining stakes as possible, suppose all of them and enter the readings in the field notes as before.

Subtract the first of these foresights from the backsight C_3 , and add the result to the total difference of level for C_2 , and enter the sum in the column $T. D. L.$

Subtract each of the following foresights from the next preceding foresight, and enter the result, with its proper sign, in the column D , and add it to the next preceding difference of level, and enter the sum in the column $T. D. L.$

As a check, subtract the foresight of B_3 from the backsight C_3 ; the difference will be the height of B_3 above C_3 , which add to the former check number, which is the difference of level of C_3 and C_1 , and the sum will be the total difference of level of B_3 and C_1 .

Compare the explanations of this article with the field notes of the following article.

367. Field Notes.

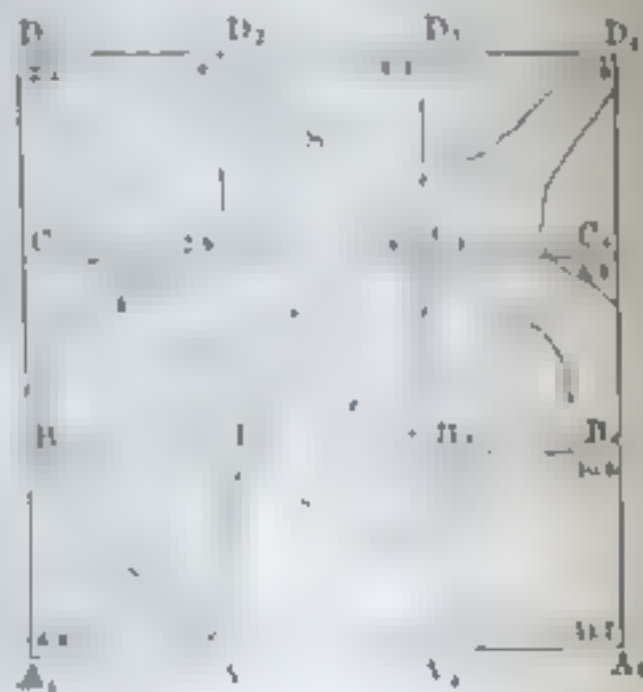
B. S.	F. S.	D.	T. D. L.	R.
			C_1 0.000	
C_1 10.378	C_2 6.481	+ 3.897	C_2 3.897	
	D_1 8.235	+ 1.751	D_1 2.143	
	D_2 6.378	+ 1.857	D_2 4.000	
	D_3 4.102	+ 2.276	D_3 6.276	
	D_4 2.304	+ 1.798	D_4 8.074	
	C_3 1.214	+ 1.090	C_3 9.164	Check 9.164
C_3 9.687	C_4 12.000	- 2.313	C_4 6.851	
	B_1 11.845	+ 0.155	B_1 7.006	
	B_2 5.184	+ 6.661	B_2 13.667	
	B_3 8.311	- 3.150	B_3 10.517	
	A_1 12.000	- 3.683	A_1 6.851	
	A_2 11.321	+ 0.670	A_2 7.520	
	A_3 10.687	+ 0.834	A_3 7.364	
	A_4 7.125	+ 3.862	A_4 11.726	
	B_4 0.112	+ 6.003	B_4 18.719	Check 9.555 18.719

368. Plotting.

Let the annexed diagram be a plot of the ground on which is written, with red ink, the height to tenths, taken from the field notes, of the surface, at each stake, above the plane of reference passing through C_1 .

Let us suppose that the horizontal planes intersecting the surface are 4 feet apart.

The intersection of the surface and the plane 4 feet above the plane of reference crosses the line $A_1 D_1$ between the points B_1 C_1 , at a point 4 feet above C'_1 .



To determine this point, observe that the rise from C_1 to B_1 is 7 feet. Then the distance on this line from C_1 to the point where the height above C_1 is 4 feet is found by the proportion,

$$7 : 4 :: 100 : x, \therefore x = 57.1.$$

This method assumes the ascent to be uniform between B_1 and C_1 ; but this point can be tested and other points of the curve found as follows: Set up the instrument at S , and make the backsight to C_1 10.378, the same as before, then depress the vane on the rod 4 feet—that is, to the reading 6.378.

Now let the rodman set up the rod at the point between C_1 and B_1 determined from the proportion, and let the surveyor observe whether the horizontal wire of the telescope ranges with the horizontal line of the vane; if not, let the rod be moved a little toward B_1 or

C_1 till they do range, and at the point thus determined let a stake marked 4 be driven by the axman.

An inspection of the plot will show that the curve passes between B_2 and C_2 at a distance from C_2 found from the proportion,

$$9.8 : .1 :: 100 : x, \therefore x = 1.$$

Let the rodman advance toward this point, pausing at one or two intermediate points, and at this point, whose positions are definitely determined and marked

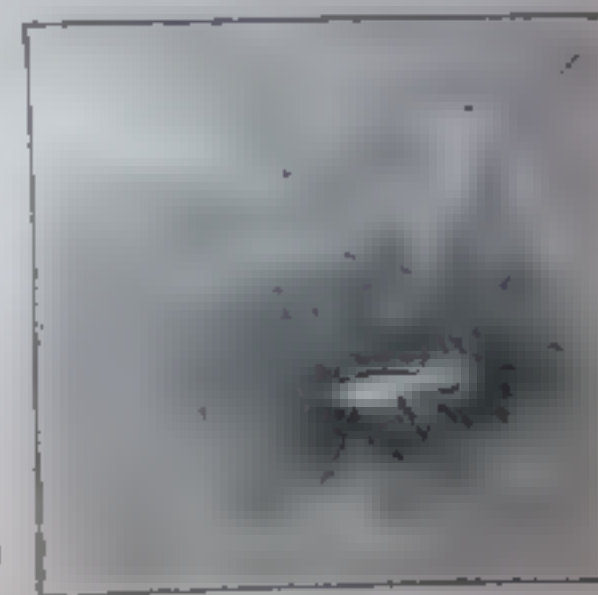
In a similar manner determine where the curve crosses C_2 C_3 and trace it to D_2 .

In like manner, trace the curves of intersection of the surface and planes, 8 feet, 12 feet, and 16 feet above the plane of reference, and let these curves be marked on the ground by stakes numbered 8, 12, and 16, respectively.

The horizontal distance of each stake from two sides of a square can be measured and recorded. From this record the surveyor can draw the curves on the plot as exhibited above.

369. Shading.

The slopes may be represented to the eye by short lines drawn perpendicular to the curves, marking the intersection of the surface with the horizontal planes. These lines are heaviest and closest where the slopes are steepest, and lighter where the slopes are less abrupt.



Increased accuracy is attained by making repeated observations, and taking the mean of the results.

To guard against varying local conditions of the atmosphere affecting pressure, beside difference of elevation, the stations should not be distant from each other more than four or five miles; and the observations should be made when there is no wind.

373. Bailey's Formula.

The subjoined formula requires a knowledge, at both stations, of the height of the column of mercury, its temperature as indicated by an attached thermometer, the temperature of the air as indicated by a detached thermometer, and the latitude of the locality.

Let d denote the difference of level in feet;

L , the latitude of the place in degrees;

h , T , t , respectively, the height of the barometer, the temperature of the mercury, and the temperature of the air at the lower station;

h' , T' , t' , respectively, the same at the upper station.

Then, $d = 60345.51 [1 + .001111 (t + t' - 64)]$

$$\times (1 + .002695 \cos 2L) \times \log \frac{h}{h' [1 + .0001 (T - T')]}.$$

Let $A = \log \{60345.51 [1 + .001111 (t + t' - 64)]\}$,

$B = \log (1 + .002695 \cos 2L)$,

$C = \log [1 + .0001 (T - T')]$,

$D = \log h - (\log h' + C)$.

$\therefore \log d = A + B + \log D$.

This formula is applied by the aid of the tables:

374. Howlet's Tables.

Table A, for Detached Thermometer.

$t - t'$	A.	$t - t'$	A.	$t - t'$	A.	$t - t'$	A.
1°	4.74914	46°	4.77187	91°	4.79348	136°	4.81407
2°	4.74966	47°	4.77236	92°	4.79395	137°	4.81452
3°	4.75017	48°	4.77285	93°	4.79442	138°	4.81496
4°	4.75069	49°	4.77335	94°	4.79489	139°	4.81541
5°	4.75120	50°	4.77384	95°	4.79535	140°	4.81585
6°	4.75172	51°	4.77433	96°	4.79582	141°	4.81630
7°	4.75223	52°	4.77482	97°	4.79628	142°	4.81674
8°	4.75274	53°	4.77530	98°	4.79675	143°	4.81719
9°	4.75326	54°	4.77579	99°	4.79721	144°	4.81763
10°	4.75377	55°	4.77628	100°	4.79768	145°	4.81807
11°	4.75428	56°	4.77677	101°	4.79814	146°	4.81851
12°	4.75479	57°	4.77725	102°	4.79861	147°	4.81896
13°	4.75531	58°	4.77774	103°	4.79907	148°	4.81940
14°	4.75582	59°	4.77823	104°	4.79953	149°	4.81984
15°	4.75633	60°	4.77871	105°	4.79999	150°	4.82028
16°	4.75684	61°	4.77919	106°	4.80045	151°	4.82072
17°	4.75735	62°	4.77968	107°	4.80091	152°	4.82116
18°	4.75786	63°	4.78016	108°	4.80137	153°	4.82160
19°	4.75837	64°	4.78065	109°	4.80183	154°	4.82204
20°	4.75888	65°	4.78113	110°	4.80229	155°	4.82248
21°	4.75938	66°	4.78161	111°	4.80275	156°	4.82291
22°	4.75989	67°	4.78209	112°	4.80321	157°	4.82335
23°	4.76039	68°	4.78257	113°	4.80367	158°	4.82379
24°	4.76090	69°	4.78305	114°	4.80413	159°	4.82423
25°	4.76140	70°	4.78353	115°	4.80458	160°	4.82466
26°	4.76190	71°	4.78401	116°	4.80504	161°	4.82510
27°	4.76241	72°	4.78449	117°	4.80550	162°	4.82553
28°	4.76291	73°	4.78497	118°	4.80595	163°	4.82597
29°	4.76342	74°	4.78544	119°	4.80641	164°	4.82640
30°	4.76392	75°	4.78592	120°	4.80686	165°	4.82684
31°	4.76442	76°	4.78640	121°	4.80731	166°	4.82727
32°	4.76492	77°	4.78687	122°	4.80777	167°	4.82770
33°	4.76542	78°	4.78735	123°	4.80822	168°	4.82814
34°	4.76592	79°	4.78782	124°	4.80867	169°	4.82857
35°	4.76642	80°	4.78829	125°	4.80913	170°	4.82900
36°	4.76692	81°	4.78877	126°	4.80958	171°	4.82943
37°	4.76742	82°	4.78925	127°	4.81003	172°	4.82986
38°	4.76792	83°	4.78972	128°	4.81048	173°	4.83029
39°	4.76842	84°	4.79019	129°	4.81093	174°	4.83072
40°	4.76891	85°	4.79066	130°	4.81138	175°	4.83115
41°	4.76940	86°	4.79113	131°	4.81183	176°	4.83158
42°	4.76990	87°	4.79160	132°	4.81228	177°	4.83201
43°	4.77039	88°	4.79207	133°	4.81273	178°	4.83244
44°	4.77089	89°	4.79254	134°	4.81317	179°	4.83287
45°	4.77138	90°	4.79301	135°	4.81362	180°	4.83330

Table B, for Latitude.

	B	L	B	L	B	L	B
0°	0.00117	27°	0.00069	50°	1.00080	50°	1.00045
1°	0.00116	30°	0.00058	51°	0.99976	60°	0.99941
2°	0.00114	33°	0.00048	52°	0.99972	63°	0.99931
3°	0.00111	36°	0.00036	53°	0.99968	66°	0.99922
4°	0.00107	39°	0.00024	54°	0.99964	69°	0.99913
5°	0.00104	42°	0.00012	55°	0.99960	75°	0.99899
6°	0.00095	45°	0.00000	56°	0.99956	80°	0.99890
7°	0.00087	48°	0.99988	57°	0.99952	85°	0.99885
8°	0.00078	49°	0.99984	58°	0.99949	90°	0.99883

Table C, for an Attached Thermometer.

T-T'	C	T-T'	C	T-T'	C	T-T'	C
0°	0.00000	12°	0.00052	24°	0.00104	36°	0.00156
1°	0.00004	13°	0.00056	25°	0.00108	37°	0.00161
2°	0.00009	14°	0.00061	26°	0.00113	38°	0.00165
3°	0.00013	15°	0.00065	27°	0.00117	39°	0.00169
4°	0.00017	16°	0.00069	28°	0.00121	40°	0.00174
5°	0.00022	17°	0.00074	29°	0.00125	41°	0.00178
6°	0.00026	18°	0.00078	30°	0.00129	42°	0.00182
7°	0.00030	19°	0.00082	31°	0.00133	43°	0.00187
8°	0.00035	20°	0.00087	32°	0.00137	44°	0.00191
9°	0.00039	21°	0.00091	33°	0.00141	45°	0.00195
10°	0.00043	22°	0.00095	34°	0.00145	46°	0.00200
11°	0.00048	23°	0.00100	35°	0.00149	47°	0.00204

375. Examples.

1. At the mountain Guanaxuato, in Mexico, lat. 21°, Humboldt made the following observations:

Lower Station. Upper Station.

Barometric column, $h = 30.05$, $h' = 23.66$.

Attached thermometer, $T = 77°.6$, $T' = 70°.4$.

Detached thermometer, $t = 77°.6$, $t' = 70°.4$.

$$\log d = A + B + \log D.$$

$$\log h (30.05) = 1.47784 \quad A = 1.81940$$

$$\log h' (23.66) = 1.37402 \quad B = 0.00087$$

$$\text{Table C gives } C = 0.00031 \quad \log D = 1.01498$$

$$\log h' + C = 1.37433 \quad \log d = 3.8525$$

$$D = \log h - (\log h' + C) = 0.10351 \quad \therefore d = 6843 \text{ ft.}$$

2. Find the difference of level of two stations, lat. 42°, from the following data:

$$\left. \begin{array}{l} h = 30, \quad T = 75°.5, \quad t = 75°. \\ h' = 25, \quad T' = 70°.3, \quad t' = 70°. \end{array} \right\} \text{Ans. 5195 ft.}$$

3. Find the difference of level of two stations, lat. 45°, from the following data:

$$\left. \begin{array}{l} h = 29.2, \quad T = 80°.3, \quad t = 80°. \\ h' = 27.1, \quad T' = 77°.4, \quad t' = 77°. \end{array} \right\} \text{Ans. 2149.9 ft.}$$

4. Find d , lat. 50°, from the following data:

$$\left. \begin{array}{l} h = 29, \quad T = 60°.1, \quad t = 60°. \\ h' = 28, \quad T' = 59°.1, \quad t' = 59°.1. \end{array} \right\} \text{Ans. 973.8 ft.}$$

376. Leveling with one Barometer.

Take the observations at the lower station, then proceed to the upper station and take the observations there, and note the interval of time which has intervened, then go back to the lower station and at the expiration of an equal interval repeat the observations.

Reduce the mercurial column of the second observation at the lower station to what it would have been at the temperature of the first observation, on the principle that mercury expands or contracts .001 of its volume for each degree of increase or diminution of temperature.

Then take the arithmetical mean of this reduced height and the first observed height for the height at the lower station, the mean of the temperature denoted

by the detached thermometer at the lower station for the temperature of the air at that station, and the temperature denoted by the attached thermometer at the first observation for the temperature of the mercury, then proceed as if the observations had been taken with two barometers.

377. Examples.

1. { Lower sta. { 1st obv., $h = 29.62$, $T = 56^{\circ}.5$, $t = 56^{\circ}$.
 { 2d obv., $h = 29.63$, $T = 63^{\circ}$, $t = 61^{\circ}$.
 { Lat. $41^{\circ}.4$, upper sta. $h' = 28.94$, $T' = 57^{\circ}.5$, $t' = 57^{\circ}$.

Reducing h of 2d obv. from $T = 63^{\circ}$ to $T = 56^{\circ}.5$, we have,

$$\text{Reduced } h = 29.63 (1 - 6.5 \times .0001) = 29.611.$$

$$\therefore \text{Mean } h = \frac{29.62 + 29.611}{2} = 29.6155$$

$$\text{Mean } t = \frac{56^{\circ} + 61^{\circ}}{2} = 58^{\circ}.5$$

$$\therefore t + t' = 58^{\circ}.5 + 57^{\circ} = 115^{\circ}.5$$

$$\text{and } T - T' = 56^{\circ}.5 - 57^{\circ}.5 = -1^{\circ}$$

$$\log h = 29.6155 \quad 1.47172 \quad 1.80481$$

$$\log h' = 28.94 \quad 1.46150 \quad 1.00014$$

$$C = -0.00004 \quad \log D = 2.00260$$

$$\log h + C = 1.46146 \quad \log d = 2.80755$$

$$D = \log h - (\log h' + C) = 0.01006 \quad d = 642 \text{ feet}$$

2. { Lower sta. { 1st obv., $h = 29.7$, $T = 60$, $t = 60^{\circ}$.
 { 2d obv., $h = 29.75$, $T = 60$, $t = 66^{\circ}$.
 { Lat. 40° ; upper sta. $h' = 28.6$, $T' = 62$, $t' = 62^{\circ}$.

$$\text{Ans. } d = 1077 \text{ ft}$$

3. { Lower sta. { 1st obv., $h = 29.6$, $T = 70$, $t = 50^{\circ}$.
 { 2d obv., $h = 29.65$, $T = 70$, $t = 46^{\circ}$.
 { Lat. 50° ; upper sta. $h' = 27.6$, $T' = 70$, $t' = 45^{\circ}$.

$$\text{Ans. } d = 1000 \text{ ft.}$$

NAVIGATION.

PRELIMINARIES.

378. Definition and Classification.

Navigation is the art of ascertaining the place of a ship at sea, and of conducting it from port to port.

There are two methods of finding the place of a ship:

1. **By dead reckoning**; that is, by tracing from the record the courses and distances sailed.

2. **By Nautical Astronomy**; that is, by deducing the latitude and longitude of the place of the ship from celestial observations.

The first method is subdivided into the following:

Plane sailing, parallel sailing, middle latitude sailing, Mercator's sailing, and current sailing.

379. The Mariner's Compass.

The magnetic needle rests on a pivot, so as to turn freely.

The compass box is suspended by gimbals or rings, turning on axes at right angles to each other, thus securing a horizontal position notwithstanding the rolling motion of the ship.

A circular card, whose circumference is divided into thirty-two equal parts, called *points*, each of which is

is divided into four equal parts, called *quarter points*, rests upon the needle, with which it turns freely.



N. b. E. is read north by east; *N. N. E.*, north north-east, etc.

380. Table of Points and Angles.

	North.		South		Angles
1	N.b.E.	N.b.W.	S.b.E.	S.b.W.	11° 15'
2	N.N.E.	N.N.W.	S.S.E.	S.S.W.	22° 30'
3	N.E.b.N.	N.W.b.N.	S.E.b.S.	S.W.b.S.	33° 45'
4	N.E.	N.W.	S.E.	S.W.	45° 0'
5	N.E.b.E.	N.W.b.W.	S.E.b.E.	S.W.b.W.	56° 15'
6	E.N.E.	W.N.W.	E.S.E.	W.S.W.	67° 30'
7	E.b.N.	W.b.N.	E.b.S.	W.b.S.	78° 45'
8	E.	W.	E.	W.	90° 0'

Note 1.— $\frac{1}{4}$ point = $2^{\circ} 48'$, $\frac{1}{2}$ point = $5^{\circ} 37'$, $\frac{3}{4}$ point = $8^{\circ} 26'$.

Note 2.—The compass is placed near the helm, at the stern, and the line from the center of the compass to the ship's head indicates the track of the ship.

381. Variation and Deviation of the Compass.

The **variation** of the compass is the angle included between the magnetic meridian and the true meridian.

The amount of variation is ascertained by Nautical Astronomy.

The **deviation** of the compass is the deflection of the needle from the magnetic meridian, caused by the iron in the ship.

The amount of deviation is ascertained by special experiments.

382. Course, Leeway, Rhumb Line.

The **compass course** of a ship, at any point, is the angle which her track makes with the magnetic meridian at that point.

The **true course** of a ship, at any point, is the angle which her track makes with the true meridian at that point.

In the compass course, the deviation is supposed to be ascertained and allowed for, but not the variation; but in the true course, both the deviation and variation.

The **leeway** is the oblique motion of the ship, caused by a side wind driving the ship along a track oblique to the fore-and-aft line, and therefore not indicated by the compass.

The amount of leeway, under a wind of a given obliquity and velocity, for each ship with a given freight, is best found by trial.

A **rhumb line** is the track of a ship which continues to make the same angle with the meridians. It is also called a *loxodromic curve*.

Since the meridians converge, the rhumb line is a spiral curve.

In what follows we shall suppose that proper allowances have been made for the variation and deviation of the compass, and, therefore, that the courses given are the true courses.

383. The Log and Log Line.

The log, a drawing of which is annexed, is a board in the form of a quadrant whose radius is about six inches, the circular part of which is loaded with lead, sufficient to give it a vertical position and to cause it to sink so that the vertex shall be just above the surface.



The log line is a line about 120 fathoms in length, and so attached to the log as to keep its face toward the ship, that it may, by the resistance it encounters from the water, unwind the line from a reel as the vessel advances.

The log line is divided into equal parts called knots, each knot being $7\frac{1}{8}$ of a nautical mile, or 50 $\frac{1}{2}$ feet.

The time is measured by a sand glass, through which the sand passes in $7\frac{1}{8}$ of an hour, or in $\frac{1}{2}$ of a minute.

Since the number of knots in a nautical mile is equal to the number of half-minutes in an hour, it follows that the number of knots run off in half a minute is equal to the number of miles the ship is sailing an hour.

The divisions of the line are marked by strings passing through the line and knotted, the number of knots in the string indicating the number of parts between

it and that point of the line where the divisions commence at that end of the line next to the log.

The stray line is about 10 fathoms of the end of the line from the log to the point where the divisions begin. This portion allows the log to settle in the water, clear of the ship, before the measurement of the rate begins.

The termination of the stray line is marked by a piece of red cloth.

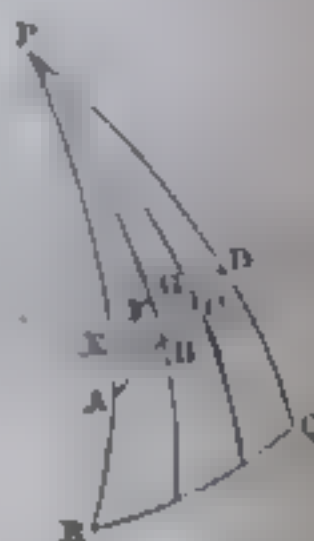
The sand glass is turned the instant this cloth passes the reel, which is stopped the moment the sand has run out.

The number of knots on the string which marks the last division run from the reel, indicates the rate of sailing.

PLANE SAILING.

384. Single Courses.

Let P be the pole of the earth; RQ , the equator; AD , a rhumb line divided into AB , BC , CD , etc., parts so small that we may regard them as straight lines; and the triangles ABE , BCF , CDG , plane triangles and similar, which give the continued proportions:



$$AB : AE :: BC : BF :: CD : CG.$$

$$AB : EB :: BC : FC :: CD : GD.$$

Since the sum of the antecedents is to the sum of the consequents as one antecedent is to its consequent, we have,

$$AD : AE + BF + CG :: AB : AE.$$

$$AD : EB + FC + GD :: AB : EB.$$

Now let a right triangle, ABC , be constructed, in which C is the course or the angle which the rhumb line makes with the meridian. $r = CB = AD$, the rhumb line of the first figure; $l = CA = AE + EF + FG =$ difference of latitude; $d = AB = EB + FC + GD =$ the sum of the elementary departures.



We may now, without supposing the ship to sail on a plane, replace the surface on which it actually sails by a plane surface, and hence the name *plane sailing*.

385. Table of Cases.

	Given.	Req.	Formulae.
1	r, C, l, d	l	$r \cos C, \quad d = r \sin C$
2	r, l, C, d	$\cos C$	$\frac{l}{r}, \quad 1 - r^2 = l^2$
3	r, d, C, l	$\sin C$	$\frac{d}{r}, \quad 1 - r^2 = d^2$
4	C, l, r, d	r	$\frac{l}{\cos C}, \quad l \tan C$
5	C, d, r, l	r	$\frac{d}{\sin C}, \quad \tan C$
6	l, d, r, C	r	$1 - l^2 = d^2, \quad \tan C = \frac{d}{l}$

Note 1.— l in miles may be reduced to degrees by dividing by 60.

Note 2.—Examples in case I. may be solved by the Traverse table.

386. Examples.

1. A ship sails 105 miles N. E. by N., from latitude 50° ; required the latitude in which the ship then is, and the departure made.

Ans. $51^\circ 27' 3''$ N., $d = 58.34$ mi.

2. A ship sailed between S. and W. 118 miles, making the difference of latitude 114.4, required the course and the departure made.

Ans. $3\frac{1}{2}$ pts W. of S., $d = 93.9$ mi.

3. A ship in latitude $3^\circ 52'$ S. sails between N. and W. 1065 miles, making a departure of 939 miles; required the course and the latitude in which she then is.

Ans. N. W. b. W. $\frac{1}{2}$ W., lat. $4^\circ 30'$ N.

4. A ship ran from latitude $38^\circ 32'$ N. to latitude $36^\circ 56'$ N. on a course S. E. by S. $\frac{1}{4}$ E., required the distance sailed and the departure made.

Ans. $r = 129.56$ mi., $d = 87.009$ mi.

5. A ship sailed S. $56^\circ 47'$ E. from latitude $50^\circ 13'$ N. till her departure was 82 miles; required r and latitude in.

Ans. $r = 98$ mi., lat. $49^\circ 19'$ N.

6. A ship from latitude $36^\circ 12'$ N. sails between S. and W. till she is in latitude $35^\circ 1'$ N., having made 76 miles of departure; required r and C .

Ans. $r = 104$ mi., $C =$ S. $46^\circ 57'$ W.

387. Compound Courses.

A compound course or traverse is the zigzag course which a ship usually takes in a voyage of considerable length.

Working the traverse is the computation of a single course and distance from the place of departure to the place of destination.

To do this, find by the Traverse table the latitude and departure of each course. The difference of the sum of the northings and the sum of the southings will be the latitude of the single course required, and the difference of the sum of the eastings and the sum of the westings will be the departure, both of the name of the greater. Then proceed as in last article.

388. Examples.

1. A ship sailed from latitude $51^{\circ} 24' N.$ as follows: S. E. 40 miles, N. E. 28 miles, S. W. by W. 52 miles, N. W. by W. 30 miles, S. S. E. 36 miles, S. E. by E. 58 miles; required the latitude in, and the single equivalent course and distance.

Solution.

Courses	Dist	N L	S L	E D	W D
S. E.	40		28.3	28.3	
N. E.	28	19.8		10.8	13.2
S. W. b W.	52		28.9		21.9
N W. b W	30	16.7			
S. S. E	36		33.3	13.8	
S. E. b. E.	58		32.2	48.2	
		36.5	122.7	110.1	68.1
			36.5	68.1	
			86.2	42	

$$\tan C = \frac{d}{l} = \frac{42}{86.2} \therefore C = 25^{\circ} 59'$$

$$r = \sqrt{l^2 + d^2} = 95.87 \text{ mi.}$$

$$l = 86.2 \text{ mi.} = 1^{\circ} 20' \quad 51^{\circ} 24' - 1^{\circ} 20' = 49^{\circ} 58' N.$$

2 Given the following courses and distances S. W. $\frac{1}{2}$ W. 62 miles, S. by W. 16 miles, W. $\frac{1}{4}$ S. 40 miles, S. W.

$\frac{1}{4}$ W. 29 miles, S. by E. 30 miles, S. $\frac{1}{4}$ E. 14 miles; required l , C , and r .

$$\text{Ans. } l = 1^{\circ} 55' S, C = S. 43^{\circ} 11' W., r = 158 \text{ mi.}$$

3. A ship, from latitude $1^{\circ} 12' S.$, has sailed as follows: E. by N. $\frac{1}{2}$ N. 56 miles, N. $\frac{1}{4}$ E. 80 miles, S. by E. $\frac{1}{2}$ E. 96 miles, N. $\frac{1}{4}$ E. 68 miles, E. S. E. 40 miles, N. N. W. $\frac{1}{2}$ W. 86 miles, E. by S. 65 miles; required the latitude in, C , and r .

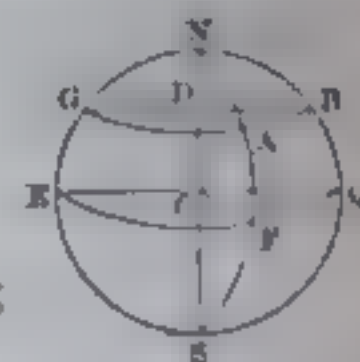
$$\text{Ans. Lat. in, } 0^{\circ} 48' N., C = 51^{\circ} 47' E., r = 193.8 \text{ mi.}$$

PARALLEL SAILING.

389. Definition and Principles.

Parallel sailing is that case of sailing in which the track is on a parallel of latitude.

Let EFQ be the equator;
 GAB , the parallel of the track;
 $r = AB$ = the distance sailed;
 $L = FQ$ = the difference of longitude;
 $l = QB$ = the latitude of the track.



Since similar arcs are to each other as their radii,

$$(1) \quad DB : CQ :: AB : FQ.$$

Consider the radius CQ as the unit of the first couplet, then DB will be the natural co-sine of latitude; and take 1 mile as the unit in the second couplet, put r for AB , L for FQ , then (1) becomes,

$$(2) \quad \cos l = 1 : r :: L, \therefore (3) \quad L = \frac{r}{\cos l}.$$

We can compute L in (3) by taking $\text{nat. cos } l$, or by introducing R and taking $\log \cos l$. In either case L will be found in miles, since r is given in miles; but L can be reduced to degrees by dividing by 60.

Let r and r' , measured on the parallels whose latitudes are l and l' , respectively, be the distances between two meridians whose difference of longitude is L .

$$\left. \begin{aligned} \cos l : 1 :: r : L, \\ \cos l' : 1 :: r' : L, \end{aligned} \right\} \therefore \cos l : \cos l' :: r : r'.$$

Hence, *The distances between two meridians, measured on different parallels, are as the co-sines of the latitudes of those parallels.*

To find the length of a degree of longitude on any parallel, observe that at the equator 1° of lon. = 60 nautical miles, and that $\cos l = 1$, then we shall have,

$$1 : \cos l :: 60 : r', \therefore r' = 60 \cos l'.$$

390. Examples.

1. A ship in latitude $49^\circ 32'$ N., and longitude $10^\circ 16'$ W., sails due W. 118 miles; required the longitude arrived at.
Ans. $13^\circ 18'$ W.

2. A ship in latitude $53^\circ 36'$ N., and longitude $10^\circ 18'$ E., sails due W. 236 miles; required the longitude arrived at.
Ans. $3^\circ 40'$ E.

3. A ship in latitude 32° N. sails $6^\circ 21'$ due W.; required d .
Ans. $d = 325.6$ mi.

4. A ship sails 310 miles from longitude $81^\circ 36'$ W. to longitude $91^\circ 50'$ W.; required the latitude of the track.
Ans. $59^\circ 41'$.

MIDDLE LATITUDE SAILING

391. Definition and Principles.

Middle latitude sailing is a combination of plane sailing and parallel sailing, on the supposition that the departure in plane sailing is equal to the distance

between the meridians passing through the extreme points of the rhumb line, measured on the middle parallel between these points.

Let AD be a rhumb line; JK , the middle parallel; m , the latitude of JK ; then $d = EB + FC + GD = JK$.

For r , formula (3), parallel sailing, substitute d or its value as found in plane sailing; and for $\cos l$ substitute $\cos m$, then we shall have,



$$L = \frac{d}{\cos m} = \frac{r \sin C}{\cos m} = \frac{r^2 \tan C}{\cos m} = \frac{l \tan C}{\cos m}.$$

Note 1.—Remember that in these formulas l denotes the difference of latitude; L , the difference of longitude in miles; d , the departure; r , the distance run or the rhumb line; C , the course, and m , the middle latitude.

Note 2.—The middle latitude is the half sum of the extreme latitudes; or the less latitude, plus the half difference of latitude; or the greater latitude, minus the half difference of latitude.

Note 3.—That the departure is not strictly equal to the middle-latitude distance between the meridians, through the extremities of the rhumb line, is thus shown:

Suppose a ship to sail on this middle latitude from one of the meridians to the other, then the distance sailed will be the departure; but if a second ship were to sail from a lower latitude on the first meridian, and a third ship, from a higher, to the same place, the departure of the second would be greater, and the departure of the third would be less than that of the first.

It is necessary, therefore, to make the correction for middle latitude as found in the table for such corrections.

The following is the rule for correcting the middle latitude.

Add to the uncorrected middle latitude the correction found in the table under the difference of latitude, and opposite the middle latitude - the sum m' is the corrected middle latitude.

$$\therefore L = \frac{d}{\cos m'} = \frac{r \sin C}{\cos m'} = \frac{1}{\cos m'} \sqrt{r^2 - l^2} = \frac{l \tan C}{\cos m'}$$

392. Examples.

1. A ship from latitude $51^\circ 18'$ N., longitude $9^\circ 50'$ W., sails S. $33^\circ 8'$ W. 1024 miles; required the latitude and longitude in.

$$l = r \cos C, \therefore l = 857.4 \text{ mi.} = 14^\circ 17'.$$

$$\therefore 51^\circ 18' - 14^\circ 17' = 37^\circ 1', \text{ the lat. in.}$$

$$\frac{1}{2}(51^\circ 18' + 37^\circ 1') = 44^\circ 9\frac{1}{2}' = \text{mid. lat., correction } 27'.$$

$$44^\circ 9\frac{1}{2}' + 27' = 44^\circ 36\frac{1}{2}' = m' = \text{corrected mid. lat.}$$

$$L = \frac{r \sin C}{\cos m'}, \therefore L = 786.3 \text{ mi. } 13^\circ 6'.$$

$$9^\circ 50' + 13^\circ 6' = 22^\circ 56' \text{ W., the lon. in.}$$

2. A ship, from latitude $52^\circ 6'$ N., and longitude $35^\circ 6'$ W., sails N. W. by W. 229 miles; required the latitude and longitude arrived at.

$$\text{Ans. Lat. } 54^\circ 13' \text{ N. and lon. } 40^\circ 23' \text{ W.}$$

3. A ship from latitude $49^\circ 57'$ N., and longitude $5^\circ 11'$ W., sails between S. and W. till she is in latitude $38^\circ 27'$ N., when she has made 440 miles departure; required C , r , and the longitude in.

$$\text{Ans. } C = \text{S. } 32^\circ 32' \text{ W.; } r = 818 \text{ mi.; lon. in, } 15^\circ 28' \text{ W.}$$

4. A ship from latitude 37° N., longitude $22^\circ 56'$ W., sails N. $33^\circ 19'$ E. till she is in latitude $51^\circ 18'$ N. What longitude is she in? Ans. $9^\circ 45'$ W.

5. A ship from latitude $40^\circ 41'$ N., longitude $16^\circ 37'$ W., sails between N and E. till she is in latitude $43^\circ 57'$ N., and finds that she has made 218 miles departure; required C , r , and longitude in.

$$\text{Ans. } C = 51^\circ 41' \text{ E.; } r = 316 \text{ mi.; lon. in, } 11^\circ \text{ W.}$$

MERCATOR'S SAILING.

393. Definitions and Principles.

Mercator's chart, so called from its originator, Gerrard Mercator, a Fleming, who first published it in 1556, is a representation of the surface of the earth on the supposition that the earth is a cylinder.

The meridians are thus represented parallel and every-where too far apart except at the equator.

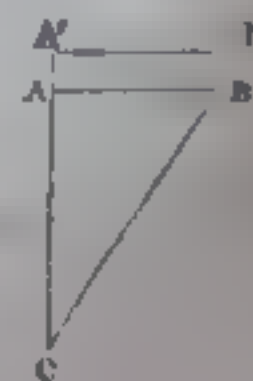
To guard as much as possible against distortion, the distances between the parallels are proportionally increased.

The surface is thus relatively magnified more and more toward the poles.

Mercator's sailing is the method of computing the difference of longitude from the principle on which Mercator's chart is projected.

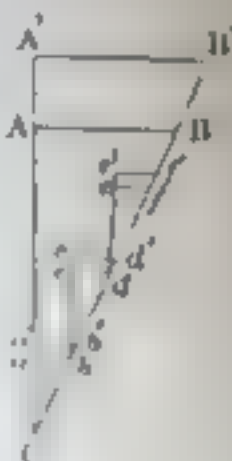
The mathematical theory of this method was developed, and the *Table of Meridional Parts*, necessary to its application, computed by Edward Wright, an Englishman, in 1599.

Let CA and AB , respectively, be the difference of latitude and departure corresponding to the rhumb line CB , and let CA be produced to A' till $A'B'$, the corresponding departure, is equal to the differ-



ence of longitude of C and B . CA' is called the *meridional difference of latitude*, which is simply the proper difference of latitude increased till the corresponding departure is equal to the difference of longitude corresponding to the proper departure.

To find the meridional difference of latitude, let Cb , bd , df , ... be indefinitely small portions of the rhumb line CB . Ca , bc , de , ... corresponding differences of latitude; ab , cd , ef , ... corresponding differences of departure; Ca' , bc' , de' , ... corresponding meridional differences of latitude; $a'b'$, $c'd'$, ef' , ... differences of longitude corresponding to the departures ab , cd , ef , ... whose latitudes are l , l' , l'' , ... Then, as found in Parallel sailing,



$$ab : a'b' :: \cos l : 1.$$

$$\text{but } ab : a'b' :: Ca : Ca'.$$

$$\therefore \cos l : 1 :: Ca : Ca', \therefore Ca' = \frac{Ca}{\cos l}.$$

$$\text{but } \frac{1}{\cos l} = \sec l, \therefore Ca' = Ca \sec l.$$

$$\text{In like manner, } bc' = bc \sec l',$$

$$de' = de \sec l'',$$

...

$$\text{But } CA' = Ca' + bc' + de' + \dots$$

Substituting the values of Ca' , bc' , de' , ... and making $Ca = bc = de = \dots = 1'$, we have,

$$CA' = \sec l + \sec l' + \sec l'' + \dots$$

Commencing at the equator, and putting *m. p.* for meridional parts, and taking natural secants, we have,

$$m. p. \text{ of } 1' = \sec 1'.$$

$$m. p. \text{ of } 2' = \sec 1' + \sec 2'.$$

$$m. p. \text{ of } 3' = \sec 1' + \sec 2' + \sec 3'.$$

$$m. p. \text{ of } 4' = \sec 1' + \sec 2' + \sec 3' + \sec 4'.$$

$$\dots \dots \dots$$

By substituting and condensing, we have,

$$m. p. \text{ of } 1' = 1.0000000 \quad 1.0000000$$

$$m. p. \text{ of } 2' = 1.0000000 + 1.0000002 \quad 2.0000002$$

$$m. p. \text{ of } 3' = 2.0000002 + 1.0000004 \quad 3.0000006$$

$$m. p. \text{ of } 4' = 3.0000006 + 1.0000007 \quad 4.0000013$$

$$\dots \dots \dots$$

The accuracy of the result is increased by taking the parts still smaller, as $\frac{1}{2}'$.

Having found the meridional latitude corresponding to C' , and also to A , their difference will be the meridional difference of latitude found from the table; and the corresponding departure, $A'B'$, will be the difference of longitude.

Denoting the proper difference of latitude CA by l , the meridional difference of latitude by l' , the departure AB by d , and the difference of longitude $A'B'$ by L , the triangles CAB and $CA'B'$ give,

$$1 : \tan C :: l' : L, \therefore L = l' \tan C.$$

$$l : d :: l' : L, \therefore L = \frac{l'd}{l}.$$

394. Examples in Single Courses.

1. A ship from latitude $52^\circ 6' N.$, and longitude $35^\circ 6' W.$, sails N. W. by W. 229 miles; required the latitude and longitude in.

$$l = r \cos C = 229 \cos 56^\circ 15', \therefore l = 127.3 \text{ mi. } 2^\circ 7'$$

$$\text{lat. in} = 52^\circ 6' N. + 2^\circ 7' N. = 54^\circ 13' N$$

m. p. of $54^{\circ} 13'$ 3868 But $L = l' \tan C$,
 m. p. of $52^{\circ} 6'$ 3657 . . . $L = 211 \tan 56^{\circ} 15'$.
 . . . $l' = 211$ | or $L = 315.8$ mi. $5^{\circ} 16'$.

. lon in $35^{\circ} 6' W. + 5^{\circ} 16' W. = 40^{\circ} 22' W.$

2. A ship from latitude $51^{\circ} 18' N.$, and longitude $9^{\circ} 50' W.$, sails S. $33^{\circ} 8' W.$ 1024 miles; required the latitude and longitude in.

Ans. Lat. in $37^{\circ} 1' N.$; lon. in $22^{\circ} 50' W.$

3. Required the course and distance from Ushant, latitude $48^{\circ} 28' N.$, longitude $5^{\circ} 3' W.$, to St. Michael's, latitude $37^{\circ} 44' N.$, longitude $25^{\circ} 40' W.$

Ans. S. $54^{\circ} 30' W.$, $r = 1106$ mi.

4. A ship from latitude $51^{\circ} 9' N.$ sails S. W. b. W. 216 miles; required the latitude in, and the difference of longitude made. Ans. Lat. $49^{\circ} 9' N.$, $L = 4^{\circ} 39'$.

5. A ship sails from latitude $37^{\circ} N.$, longitude $22^{\circ} 56' W.$, on the course N. $33^{\circ} 19' E.$, till she arrives at latitude $51^{\circ} 18' N.$; required the distance sailed and the longitude arrived at. Ans. 1027 mi., lon $9^{\circ} 47' W.$

6. A ship sails N. E. b. E. from latitude $42^{\circ} 25' N.$, and longitude $15^{\circ} 6' W.$, till she finds herself in latitude $46^{\circ} 20' N.$; required the distance sailed and the longitude in. Ans. Dist., 423 mi.; lon. $6^{\circ} 55' W.$

395. Examples in Compound Courses.

1. A ship from latitude $60^{\circ} 9' N.$, and longitude $1^{\circ} 7' W.$, sailed as follows: N. E. b. N., 69 miles; N. N. E., 48 miles; N. b. W. $\frac{1}{2} W.$, 78 miles; N. E., 108 miles; S. E. b. E., 50 miles; required the latitude and longitude in, and the direct course and distance.

Courses.	Dist	N. L.	S. L.	Lat	m. p.	m d l.	F. L.	W. L.
N. E. b. N.	69	57.4		$60^{\circ} 9'$	4525			
N. N. E.	48	44.4		$61^{\circ} 6'$	4641	116	77.5	
N b W $\frac{1}{2} W$	78	74.6		$61^{\circ} 50'$	4733	92	38.1	
N E.	108	76.4		$63^{\circ} 5'$	4895	102		49.
S. E. b. E.	50		27.8	$64^{\circ} 21'$	5067	172	172.0	
		252.8		$63^{\circ} 53'$	5003	64	95.8	
		27.8						

Dif lat. $l = 225$ mi. $= 3^{\circ} 45' N.$ 383.4

49.

Dif. lon. $L = 334.4$ mi.

Lat. Left $= 60^{\circ} 9' N.$

Dif. lon. $= 5^{\circ} 34' E$

Dif. Lat. $= 3^{\circ} 45' N.$

Lon. left $1^{\circ} 7' W.$

Lat. in $63^{\circ} 54' N.$

Lon. in $= 4^{\circ} 27' E.$

m. p. of lat. in ($63^{\circ} 54'$) $= 5005$.

m. p. of lat. left ($60^{\circ} 9'$) $= 4525$.

Meridional dif. lat. $= l' = 480$.

$\tan C = \frac{L}{l'} = \frac{334.4}{480}$, . . . $C = N. 34^{\circ} 53' E.$

$r = \frac{l}{\cos C} = \frac{225}{\cos 34^{\circ} 53'}$, . . . $r = 273$ mi.

2. A ship from latitude $38^{\circ} 14' N.$, and longitude $25^{\circ} 56' W.$, has sailed the following courses: N. E. b. N. $\frac{1}{2} E.$, 56 miles; N. N. W., 38 miles; N. W. b. W., 46 miles; S. S. E., 30 miles; S. b. W., 20 miles; N. E. b. N., 60 miles; required the latitude and longitude in, and the direct single course and distance.

Ans. Lat. in, $40^{\circ} 2' 3 N.$; lon. in, $25^{\circ} 30' W.$;
 $C = N. 10^{\circ} 33' E.$, $r = 110.2$ mi.

396. Correction for Middle Latitude.

We are now prepared to understand how the correction for middle latitude, before used, is found.

d , the proper difference of latitude;

l , the meridional difference of latitude;

l' , the difference of longitude;

m , the middle latitude uncorrected;

c , the correction;

m' , the middle latitude corrected.

Then, by Plane, Middle latitude, and Mercator's sailing,

$$\tan C = \frac{d}{l} = \frac{L \cos m'}{l} = \frac{L}{l'}, \therefore \cos m' = \frac{l}{l'}.$$

From which m' is readily found.

Then, $c = m' - m$. $\therefore m' = m + c$.

CURRENT SAILING.

397. Definition and Principles.

Current sailing is the sailing of a ship as affected by a current.

Irrespective of the current the ship would move, in a certain time, a certain course and distance.

The current alone would carry the ship, in the same time, a certain other course and distance.

The actual track of the ship, which is the resultant of the two, will bring her to the same position as if she had sailed separately the two tracks.

Current sailing may therefore be treated as Plane sailing, compound courses.

The **set** of the current is its direction.

The **drift** of the current is its velocity.

The set and drift of a current may be ascertained by taking, a short distance from the ship, a boat, which is kept from being carried by the current by letting

down, to a considerable depth, a heavy weight, which is attached by a rope to the stern of the boat.

The log being thrown from the boat into the current, the direction in which it is carried, or set of the current, is determined by the boat compass, and the rate at which it is carried, or drift of the current, by the number of knots of the log line run out in half a minute.

398. Examples.

1. A ship sails N. W. a distance, by the log, of 60 miles, in a current that sets S. S. W., drifting 25 miles in the same time; required the course and distance.

Course.	Dist.	N. L.	S. L.	E. D.	W. D.
N. W.	60	42.4			42.4
S. S. W.	25		23.1		9.6
		l 19.3.		d 52.	

$$\tan C = \frac{d}{l} = \frac{52}{19.3}, \therefore C = \text{N. } 69^\circ 38' \text{ W.}$$

$$r = \sqrt{l^2 + d^2} = \sqrt{(19.3)^2 + (52)^2} = 55.5.$$

2. A ship, sailing 7 knots an hour, is bound to a port bearing S. 52° W., through a current S. S. E., 2 miles an hour; required the course.

Let AB be the direction of the port.

AE , the direction of the current,

2.

AD , the required direction, = 7.

Complete the parallelogram, DEA

= $BAE = 52^\circ + 22^\circ 30' = 74^\circ 30'$. Then we have,



$$AD : DB :: \sin DBA : \sin DAB.$$

$$\therefore \sin DAB = \frac{2 \sin DBA}{7}.$$

$$\therefore DAB = 15^\circ 59'. \therefore C = 15^\circ 59' + 52^\circ = 67^\circ 59'.$$

3. A ship runs N. E. by N. 18 miles in 3 hours, in a current W. by S. 2 miles an hour; required the course and distance. *Ans.* $C = N. b. E. \frac{1}{2}E.$, $r = 14$ mi.

4. In a current S. E. by S. $1\frac{1}{2}$ miles an hour, a ship sails 24 hours as follows: S.W., 40 miles; W. S W., 27 miles; S by E, 47 miles; required the direct course and the distance. *Ans.* $C = S. 11^\circ 50' W.$, $r = 117$ mi.

5. The port bears due E., the current sets S. W. by S. 3 knots an hour, the rate of sailing is 4 knots an hour; required the course steered. *Ans.* $N. 51^\circ E.$

6. A ship sailing in a current has, by her reckoning, run S. by E. 42 miles, and, by observations, is found to have made 55 miles of difference of latitude, and 18 miles of departure; required the set and drift of the current. *Ans.* Set, S. $62^\circ 12' W.$; whole drift, 30 mi.

PLYING TO WINDWARD.

399. Definitions.

Plying to windward is the zigzag course which a ship makes by tacking when she encounters a foul wind.

Starboard signifies the right side.

Larboard signifies the left side.

The **starboard tacks** are aboard when a ship plies with the wind on the right.

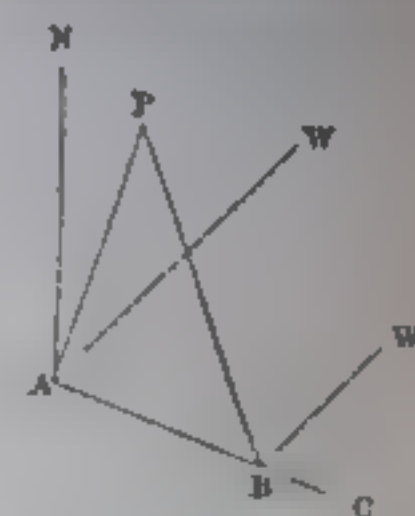
The **larboard tacks** are aboard when a ship plies with the wind on the left.

A ship is said to be *close-hauled* when she sails as nearly as possible toward the point from which the wind is blowing.

400. Examples.

1. Being within sight of my port bearing N. by E $\frac{1}{2}E.$, distant 18 miles, a fresh gale sprung up from the N. E. With my larboard tacks aboard, and close-hauled within six points of the wind, how far must I run before tacking about, and what will be my distance from the port on the second board?

Let A be the place of the ship; P , the port; AB , the distance of the first board; BP , that of the second; WA or $W'B$, the direction of the wind.



Then, $WAB = W'BC = W'BP = 6$ points.

$$\therefore ABP = 16 \text{ points} - 12 \text{ points} = 4 \text{ points.}$$

$$PAW = NAW - NAP = 4 \text{ points} - 1\frac{1}{2} \text{ points} = 2\frac{1}{2} \text{ points.}$$

$$PAB = PAW + WAB = 2\frac{1}{2} \text{ points} + 6 \text{ points} = 8\frac{1}{2} \text{ points.}$$

$$APB = 16 \text{ points} - (PAB + ABP) = 3\frac{1}{2} \text{ points.}$$

$$\sin ABP : \sin APB :: AP : AB, \therefore AB = 16 \cdot 15 \text{ mi.}$$

$$\sin ABP : \sin BAP :: AP : BP, \therefore BP = 25 \cdot 23 \text{ mi.}$$

2. If a ship can lie within 6 points of the wind on the larboard tack, and within $5\frac{1}{2}$ points on the starboard tack; required her course and distance on each tack to reach a port lying S. by E. 22 miles, the wind being at S. W.

$$\text{Ans. } \begin{cases} \text{Starboard tack, S. b. E. } \frac{1}{2}E. & 23 \cdot 66 \text{ mi.} \\ \text{Larboard tack, W. N W} & 2 \cdot 79 \text{ mi.} \end{cases}$$

3. A ship is bound to a port 80 miles distant, and directly to windward, which is N. E. by N. $\frac{1}{2}$ E., and proposes to reach her port at two boards, each within 6 points of the wind, and to lead with the starboard tack, required her course and distance on each tack.

Ans. { Starboard tack, N. N. W. $\frac{1}{2}$ W., 104.5 mi.
 { Larboard tack, E. S. E. $\frac{1}{2}$ E., 104.5 mi.

4. Wishing to reach a point bearing N. N. W. 15 miles, but the wind being at W. by N. I was obliged to ply to windward the ship, close-hauled could make way within 6 points of the wind; required the course and distance on each tack.

Ans. { Larboard tack, N. b. W. 17.65 mi.
 { Starboard tack, S. W. b. S. 4.138 mi.

TAKING DEPARTURES.

401. Explanation.

Before losing sight of land, at the beginning of a voyage, the bearing and distance of some well known object, as a light-house or headland, &c. the reverse bearing and distance of which are entered as the first course and distance on the log book.

The bearing is taken by the compass; but the distance is sometimes estimated by the eye, as can be done with considerable accuracy by navigators of experience.

A more correct method of taking a departure is by means of data, obtained by taking the bearing at two different positions of the ship, the distance between these positions being measured by the log.

402. Examples.

1. Sailing down the channel, the Eddystone bore N. W. by N., and after running W. S. W. 18 miles, it bore N. by E.; required the course and distance from the Eddystone to the place of the last observation.

$$E = N.1E + N'BE = 4 \text{ points.}$$

$$A = 16 \text{ points} - (NAE + BAS) = 7 \text{ pts.}$$

$$\sin E : \sin A :: AB : BE,$$

$$\therefore BE = 24.97.$$



2. At 3 o'clock P. M. the Lizard bore N. by W. $\frac{1}{2}$ W., and after sailing 7 knots an hour, W. by N. $\frac{1}{4}$ N., till 6 o'clock, the Lizard bore N. E. $\frac{1}{2}$ E.; required the course and distance from the Lizard to the place of the last observation.

Ans. S. W. $\frac{1}{2}$ W., 19.35 mi.

3. In order to get a departure, I observe a headland of known latitude and longitude to bear N. E. by N., and after sailing E. by N. 15 miles, the same headland bore W. N. W.; required my distance from the headland at each place of observation.

Ans. 8.5 mi. and 10.8 mi.

Remark—To find the latitude and longitude of a ship by means of celestial observations, requires a knowledge of Nautical Astronomy; but a thorough discussion of this subject would require an amount of space far exceeding our limits.

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Logarithms of Numbers to 100.

1	0.00000	21	1.32222	41	1.61278	61	1.78533	81	1.90849
2	0.30103	22	1.34242	42	1.62325	62	1.79239	82	1.91381
3	0.47712	23	1.36173	43	1.63347	63	1.79934	83	1.91908
4	0.60206	24	1.38021	44	1.64345	64	1.80618	84	1.92428
5	0.69897	25	1.39794	45	1.65321	65	1.81291	85	1.92942
6	0.77815	26	1.41497	46	1.66276	66	1.81954	86	1.93450
7	0.84510	27	1.43136	47	1.67210	67	1.82607	87	1.93952
8	0.90309	28	1.44716	48	1.68124	68	1.83251	88	1.94448
9	0.95424	29	1.46240	49	1.68920	69	1.83885	89	1.94939
10	1.00000	30	1.47712	50	1.69697	70	1.84510	90	1.95424
11	1.04139	31	1.49136	51	1.70457	71	1.85126	91	1.95904
12	1.07918	32	1.50515	52	1.71160	72	1.85733	92	1.96379
13	1.11334	33	1.51851	53	1.71828	73	1.86332	93	1.96848
14	1.14613	34	1.53148	54	1.72439	74	1.86923	94	1.97313
15	1.17609	35	1.54407	55	1.73036	75	1.87506	95	1.97772
16	1.20412	36	1.55630	56	1.73619	76	1.88081	96	1.98227
17	1.23045	37	1.56820	57	1.74187	77	1.88649	97	1.98677
18	1.25527	38	1.57978	58	1.74741	78	1.89200	98	1.99123
19	1.27875	39	1.59106	59	1.75285	79	1.89733	99	1.99564
20	1.30103	40	1.60206	60	1.75815	80	1.90259	100	2.00000

N	0	1	2	3	4	5	6	7	8	9	D.
100	8840	041	087	130	173	217	260	303	346	389	43
101	432	473	518	561	604	647	689	732	775	817	41
102	860	895	935	988	030	072	115	157	199	242	42
103	184	226	268	310	352	394	436	478	520	562	42
104	700	743	787	828	870	912	953	995	036	078	42
105	02114	160	202	243	284	325	366	407	449	490	41
106	51	552	593	633	674	715	756	796	837	878	41
107	88	929	969	1000	1000	141	181	222	262	302	40
108	0342	075	115	155	195	235	275	315	355	395	40
109	715	755	795	835	875	915	955	995	035	075	40
110	8113	170	218	258	297	336	376	415	454	493	39
111	512	551	590	629	668	707	746	785	824	863	39
112	022	061	099	138	177	216	255	294	333	372	39
113	058	096	135	173	212	250	289	327	366	404	38
114	090	129	167	205	243	281	319	357	395	433	38
115	06070	108	145	183	221	258	296	333	371	408	38
116	416	453	491	528	565	602	639	676	713	750	37
117	819	856	893	930	967	1004	1041	1078	1115	1152	37
118	07188	225	262	298	335	372	408	445	482	518	37
119	555	591	628	664	700	737	773	809	845	882	36
120	918	954	990	027	063	099	135	171	207	243	36
121	08279	114	150	186	222	258	294	330	366	402	36
122	626	662	697	733	768	804	839	875	910	946	35
123	941	976	1011	1046	1081	1116	1151	1186	1221	1256	35
124	09342	377	412	447	482	517	552	587	622	657	35
125	691	726	761	795	830	864	899	933	968	1003	35
126	10047	072	106	140	175	209	243	277	311	346	34
127	389	423	457	491	525	559	593	627	661	695	34
128	721	755	789	823	857	891	925	959	993	1027	34
129	11053	093	126	159	193	227	261	294	328	361	34
130	344	428	461	494	528	561	594	627	660	693	33
131	727	760	793	826	859	892	925	958	991	1024	33
132	12057	090	123	156	189	222	255	288	321	354	33
133	385	418	450	483	516	548	581	614	646	679	33
134	719	751	783	815	848	880	912	944	976	1008	32
135	11073	066	098	131	162	194	226	258	290	322	32
136	554	586	618	650	681	713	745	776	808	839	32
137	672	704	735	767	798	830	861	892	923	954	32
138	988	019	051	082	114	145	176	207	238	269	31
139	11101	363	394	425	456	487	518	549	580	611	31
140	613	644	675	706	737	768	799	829	860	891	31
141	922	953	984	1015	1046	1076	1107	1137	1168	1198	31
142	15229	220	250	280	310	341	371	401	431	461	31
143	554	584	614	644	674	704	734	764	794	824	30
144	850	880	910	940	970	1000	1030	1060	1090	1120	30

N	0	1	2	3	4	5	6	7	8	9	D.
145	16157	167	197	227	256	286	316	346	376	406	29
146	435	465	495	524	554	584	613	643	673	702	30
147	752	761	791	820	850	879	909	938	967	997	29
148	17026	056	085	114	143	173	202	231	260	289	29
149	319	348	377	406	435	464	493	522	551	580	29
150	609	638	667	696	725	754	782	811	840	869	29
151	898	926	955	984	013	041	070	099	127	156	29
152	18184	213	241	270	298	327	355	384	412	441	29
153	469	498	526	554	583	611	639	667	696	724	28
154	752	780	808	837	865	893	921	949	977	1005	28
155	19071	061	089	117	145	173	201	229	257	285	28
156	512	540	568	596	624	651	679	707	735	763	28
157	755	783	811	839	867	895	923	951	979	1007	28
158	806	834	862	890	918	946	974	1002	1030	1058	27
159	20115	167	194	222	249	276	303	330	358	385	27
160	412	439	466	493	521	548	575	602	629	656	27
161	657	684	711	738	765	792	819	846	873	900	27
162	922	948	975	1002	1029	1056	1083	1110	1137	1164	27
163	1207	1234	1261	1288	1315	1342	1369	1396	1423	1450	27
164	1507	1534	1561	1588	1615	1642	1669	1696	1723	1750	26
165	1807	1834	1861	1888	1915	1942	1969	1996	2023	2050	26
166	2107	2134	2161	2188	2215	2242	2269	2296	2323	2350	26
167	2407	2434	2461	2488	2515	2542	2569	2596	2623	2650	26
168	2707	2734	2761	2788	2815	2842	2869	2896	2923	2950	26
169	3007	3034	3061	3088	3115	3142	3169	3196	3223	3250	26
170	3307	3334	3361	3388	3415	3442	3469	3496	3523	3550	26
171	3607	3634	3661	3688	3715	3742	3769	3796	3823	3850	26
172	3907	3934	3961	3988	4015	4042	4069	4096	4123	4150	26
173	4207	4234	4261	4288	4315	4342	4369	4396	4423	4450	26
174	4507	4534	4561	4588	4615	4642	4669	4696	4723	4750	26
175	4807	4834	4861	4888	4915	4942	4969	4996	5023	5050	26
176	5107	5134	5161	5188	5215	5242	5269	5296	5323	5350	26
177	5407	5434	5461	5488	5515	5542	5569	5596	5623	5650	26
178	5707	5734	5761	5788	5815	5842	5869	5896	5923	5950	26
179	6007	6034	6061	6088	6115	6142	6169	6196	6223	6250	26
180	6307	6334	6361	6388	6415	6442	6469	6496	6523	6550	26
181	6607	6634	6661	6688	6715	6742	6769	6796	6823	6850	26
182	6907	6934	6961	6988	7015	7042	7069	7096	7123	7150	26
183	7207	7234	7261	7288	7315	7342	7369	7396	7423	7450	26
184	7507	7534	7561	7588	7615	7642	7669	7696	7723	7750	26
185	7807	7834	7861	7888	7915	7942	7969	7996	8023	8050	26
186	8107	8134	8161	8188	8215	8242	8269	8296	8323	8350	26
187	8407	8434	8461	8488	8515	8542	8569	8596	8623	8650	26
188	8707	8734	8761	8788	8815	8842	8869	8896	8923	8950	26
189	9007	9034	9061	9088	9115	9142	9169	9196	9223	9250	26

N.	0	1	2	3	4	5	6	7	8	9	D.
190	2875	818	821	944	867	989	612	635	658	681	23
191	2893	136	143	171	194	217	240	262	285	307	23
192	2910	285	313	338	421	443	466	488	511	533	23
193	2927	336	378	601	623	646	668	691	713	735	22
194	2944	380	803	825	847	870	892	914	937	959	22
195	2961	926	018	070	092	115	137	159	181	203	22
196	2978	218	270	292	314	336	358	380	403	425	22
197	2995	409	491	513	535	557	579	601	623	645	22
198	3012	688	710	732	754	776	798	820	842	863	22
199	3029	807	929	951	973	994	016	038	060	081	22
200	3046	125	146	168	190	211	233	255	276	298	22
201	3063	311	363	384	406	428	449	471	492	514	22
202	3080	555	577	578	600	643	664	685	707	728	21
203	3097	730	771	792	814	836	878	899	920	942	21
204	3114	963	984	005	027	069	091	112	133	154	21
205	3131	197	218	239	260	281	302	323	345	366	21
206	3148	408	429	450	471	492	513	534	555	576	21
207	3165	597	618	639	660	702	723	744	765	785	21
208	3182	806	827	848	869	911	931	952	973	994	21
209	3199	035	056	077	098	118	139	160	181	201	21
210	3216	243	263	284	305	325	346	366	387	408	21
211	3233	449	469	490	510	531	552	572	593	613	20
212	3250	654	675	695	715	736	756	777	797	818	20
213	3267	858	879	899	919	940	960	980	001	021	20
214	3284	062	082	102	122	142	162	182	202	221	20
215	3301	264	284	304	324	344	364	384	404	424	20
216	3318	465	485	505	525	545	565	585	605	625	20
217	3335	666	686	706	726	746	766	786	806	826	20
218	3352	867	887	907	927	947	967	987	007	027	20
219	3369	064	084	104	124	144	164	184	204	224	20
220	3386	265	285	305	325	345	365	385	405	425	20
221	3403	466	486	506	526	546	566	586	606	626	20
222	3420	667	687	707	727	747	767	787	807	827	20
223	3437	868	888	908	928	948	968	988	008	028	20
224	3454	069	089	109	129	149	169	189	209	229	20
225	3471	270	290	310	330	350	370	390	410	430	19
226	3488	471	491	511	531	551	571	591	611	631	19
227	3505	672	692	712	732	752	772	792	812	832	19
228	3522	873	893	913	933	953	973	993	013	033	19
229	3539	074	094	114	134	154	174	194	214	234	19
230	3556	275	295	315	335	355	375	395	415	435	19
231	3573	476	496	516	536	556	576	596	616	636	19
232	3590	677	697	717	737	757	777	797	817	837	19
233	3607	878	898	918	938	958	978	998	018	038	19
234	3624	079	099	119	139	159	179	199	219	239	19
N.	0	1	2	3	4	5	6	7	8	9	D.

N.	0	1	2	3	4	5	6	7	8	9	D.
235	37107	425	144	162	181	191	218	236	254	273	18
236	294	310	328	346	365	384	411	420	438	457	18
237	475	493	511	530	548	566	585	603	621	639	18
238	658	676	694	712	731	749	767	785	803	822	18
239	841	858	876	894	912	931	949	967	985	103	18
240	38021	059	057	075	093	112	130	148	166	184	18
241	202	221	238	256	274	292	310	328	346	364	18
242	382	399	417	435	453	471	489	507	525	543	18
243	564	578	596	614	632	650	668	686	704	721	18
244	739	757	775	792	810	828	846	863	881	899	18
245	917	934	952	970	987	005	023	041	058	076	18
246	1004	111	129	146	164	182	199	217	235	252	18
247	233	287	305	322	340	358	375	393	410	428	18
248	445	463	480	498	515	533	550	568	585	602	18
249	627	647	665	682	699	707	724	742	759	777	17
250	794	811	829	846	863	881	898	915	933	950	17
251	967	984	1002	1019	1037	1054	1071	1088	1106	1123	17
252	1140	1157	1174	1192	1209	1226	1243	1261	1278	1295	17
253	1312	1329	1346	1363	1381	1398	1415	1432	1449	1466	17
254	1483	1500	1517	1534	1551	1568	1585	1602	1619	1636	17
255	1653	1670	1687	1704	1721	1738	1755	1772	1789	1806	17
256	1823	1840	1857	1874	1891	1908	1925	1942	1959	1976	17
257	1993	2010	2027	2044	2061	2078	2095	2112	2129	2146	17
258	2163	2180	2197	2214	2231	2248	2265	2282	2299	2316	17
259	2333	2350	2367	2384	2401	2418	2435	2452	2469	2486	17
260	2503	2520	2537	2554	2571	2588	2605	2622	2639	2656	17
261	2673	2690	2707	2724	2741	2758	2775	2792	2809	2826	17
262	2843	2860	2877	2894	2911	2928	2945	2962	2979	2996	17
263	3013	3030	3047	3064	3081	3098	3115	3132	3149	3166	17
264	3183	3200	3217	3234	3251	3268	3285	3302	3319	3336	17
265	3353	3370	3387	3404	3421	3438	3455	3472	3489	3506	17
266	3523	3540	3557	3574	3591	3608	3625	3642	3659	3676	17
267	3693	3710	3727	3744	3761	3778	3795	3812	3829	3846	17
268	3863	3880	3897	3914	3931	3948	3965	3982	3999	4016	17
269	4033	4050	4067	4084	4101	4118	4135	4152	4169	4186	17
270	4203	4220	4237	4254	4271	4288	4305	4322	4339	4356	17
271	4373	4390	4407	4424	4441	4458	4475	4492	4509	4526	17
272	4543	4560	4577	4594	4611	4628	4645	4662	4679	4696	17
273	4713	4730	4747	4764	4781	4798	4815	4832	4849	4866	17
274	4883	4900	4917	4934	4951	4968	4985	5002	5019	5036	17
275	5053	5070	5087	5104	5121	5138	5155	5172	5189	5206	17
276	5223	5240	5257	5274	5291	5308	5325	5342	5359	5376	17
277	5393	5410	5427	5444	5461	5478	5495	5512	5529	5546	17
278	5563	5580	5597	5614	5631	5648	5665	5682	5699	5716	17
279	5733	5750	5767	5784	5801	5818	5835	5852	5869	5886	17
N.	0	1	2	3	4	5	6	7	8	9	N.

N.	0	1	2	3	4	5	6	7	8	9	D.
280						703	809	824	840	855	15
281						618	965	971	984	10	15
282						102	117	133	148	163	15
283						255	271	286	301	317	15
284						408	425	440	454	469	15
285						561	576	591	606	621	15
286						712	728	743	758	773	15
287						864	879	894	909	924	15
288						619	635	649	664	679	15
289						165	180	195	210	225	15
290						374	390	405	420	435	15
291						583	599	614	629	644	15
292						792	808	823	838	853	15
293						901	917	932	947	962	15
294						110	126	141	156	171	15
295						219	235	250	265	280	15
296						328	344	359	374	389	15
297						437	453	468	483	498	15
298						546	562	577	592	607	15
299						655	671	686	701	716	15
300						765	780	795	810	825	15
301						834	849	864	879	894	15
302						903	918	933	948	963	15
303						102	117	132	147	162	15
304						211	226	241	256	271	15
305						320	335	350	365	380	15
306						429	444	459	474	489	15
307						538	553	568	583	598	15
308						647	662	677	692	707	15
309						756	771	786	801	816	15
310						865	880	895	910	925	15
311						934	949	964	979	994	15
312						103	118	133	148	163	15
313						212	227	242	257	272	15
314						321	336	351	366	381	15
315						430	445	460	475	490	15
316						539	554	569	584	599	15
317						648	663	678	693	708	15
318						757	772	787	802	817	15
319						866	881	896	911	926	15
320						935	950	965	980	995	15
321						104	119	134	149	164	15
322						213	228	243	258	273	15
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324						431	446	461	476	491	15

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325	51188	202	215	228	242	255	268	282	295	308	13
326	322	335	348	362	375	388	402	415	428	441	13
327	455	468	481	495	508	521	534	548	561	574	13
328	587	601	614	627	640	654	667	680	693	706	13
329	720	733	746	759	772	786	799	812	825	838	13
330	851	865	878	891	904	917	930	943	957	970	13
331	983	996	609	622	635	648	661	675	688	701	13
332	72114	127	140	153	166	179	192	205	218	231	13
333	244	257	270	284	297	310	323	336	349	362	13
334	375	388	401	414	427	440	453	466	479	492	13
335	504	517	530	543	556	569	582	595	608	621	13
336	644	647	660	673	686	699	711	724	737	750	13
337	773	776	789	802	815	827	840	853	866	879	13
338	892	905	917	930	943	956	969	982	994	607	13
339	129	142	155	168	181	194	207	220	233	246	13
340	148	161	173	186	199	212	224	237	250	263	13
341	275	288	301	314	326	339	352	364	377	390	13
342	403	415	428	441	453	466	479	491	504	517	13
343	529	542	555	567	580	593	605	618	631	643	13
344	668	681	694	706	719	732	744	757	769	781	13
345	789	794	807	820	832	845	857	870	882	895	13
346	918	931	944	956	968	979	983	995	608	620	13
347	1000	015	028	040	053	065	078	090	103	115	13
348	128	140	153	165	178	190	203	215	228	240	12
349	259	271	283	296	308	320	332	345	357	369	12
350	387	400	412	424	437	449	461	474	486	498	12
351	516	528	540	552	564	576	588	600	612	624	12
352	643	655	667	679	691	703	715	727	739	751	12
353	778	790	802	814	826	838	850	862	874	886	12
354	900	912	924	936	948	960	972	984	996	608	12
355	622	634	646	658	670	682	694	706	718	730	12
356	742	754	766	778	790	802	814	826	838	850	12
357	860	872	884	896	908	920	932	944	956	968	12
358	980	992	604	616	628	640	652	664	676	688	12
359	701	713	725	737	749	761	773	785	797	809	12
360	821	833	845	857	869	881	893	905	917	929	12
361	949	961	973	985	997	609	621	633	645	657	12
362	679	691	703	715	727	739	751	763	775	787	12
363	807	819	831	843	855	867	879	891	903	915	12
364	937	949	961	973	985	997	609	621	633	645	12
365	665	677	689	701	713	725	737	749	761	773	12
366	795	807	819	831	843	855	867	879	891	903	12
367	925	937	949	961	973	985	997	609	621	633	12
368	655	667	679	691	703	715	727	739	751	763	12
369	785	797	809	821	833	845	857	869	881	893	12

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370	8880	8881	8882	8883	8884	8885	8886	8887	8888	8889	12
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373	8910	8911	8912	8913	8914	8915	8916	8917	8918	8919	12
374	8920	8921	8922	8923	8924	8925	8926	8927	8928	8929	12
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377	8950	8951	8952	8953	8954	8955	8956	8957	8958	8959	12
378	8960	8961	8962	8963	8964	8965	8966	8967	8968	8969	12
379	8970	8971	8972	8973	8974	8975	8976	8977	8978	8979	12
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381	8990	8991	8992	8993	8994	8995	8996	8997	8998	8999	12
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387	9050	9051	9052	9053	9054	9055	9056	9057	9058	9059	12
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392	9100	9101	9102	9103	9104	9105	9106	9107	9108	9109	12
393	9110	9111	9112	9113	9114	9115	9116	9117	9118	9119	12
394	9120	9121	9122	9123	9124	9125	9126	9127	9128	9129	12
395	9130	9131	9132	9133	9134	9135	9136	9137	9138	9139	12
396	9140	9141	9142	9143	9144	9145	9146	9147	9148	9149	12
397	9150	9151	9152	9153	9154	9155	9156	9157	9158	9159	12
398	9160	9161	9162	9163	9164	9165	9166	9167	9168	9169	12
399	9170	9171	9172	9173	9174	9175	9176	9177	9178	9179	12
400	9180	9181	9182	9183	9184	9185	9186	9187	9188	9189	12
401	9190	9191	9192	9193	9194	9195	9196	9197	9198	9199	12
402	9200	9201	9202	9203	9204	9205	9206	9207	9208	9209	12
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404	9220	9221	9222	9223	9224	9225	9226	9227	9228	9229	12
405	9230	9231	9232	9233	9234	9235	9236	9237	9238	9239	12
406	9240	9241	9242	9243	9244	9245	9246	9247	9248	9249	12
407	9250	9251	9252	9253	9254	9255	9256	9257	9258	9259	12
408	9260	9261	9262	9263	9264	9265	9266	9267	9268	9269	12
409	9270	9271	9272	9273	9274	9275	9276	9277	9278	9279	12
410	9280	9281	9282	9283	9284	9285	9286	9287	9288	9289	12
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412	9300	9301	9302	9303	9304	9305	9306	9307	9308	9309	12
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415	61805	815	826	836	847	857	868	878	888	899	10
416	909	920	930	941	951	962	972	982	993	603	10
417	62014	024	034	045	055	066	076	086	097	107	10
418	118	128	138	149	159	170	180	190	201	211	10
419	221	232	242	252	263	273	284	294	304	315	10
420	325	335	346	356	366	377	387	397	408	418	10
421	428	439	449	459	469	480	490	500	511	521	10
422	531	542	552	562	572	583	593	603	614	624	10
423	634	644	655	665	675	685	696	706	716	726	10
424	737	747	757	767	778	788	798	808	818	829	10
425	839	849	859	870	880	890	900	910	921	931	10
426	941	951	961	972	982	992	602	612	622	632	10
427	643	653	663	673	683	694	704	714	724	734	10
428	745	755	765	775	785	795	805	815	825	835	10
429	846	856	866	876	886	896	906	916	926	936	10
430	947	957	967	977	987	997	607	617	627	637	10
431	648	658	668	678	688	698	708	718	728	738	10
432	749	759	769	779	789	799	809	819	829	839	10
433	840	850	860	870	880	890	900	910	920	930	10
434	941	951	961	971	981	991	601	611	621	631	10
435	642	652	662	672	682	692	702	712	722	732	10
436	743	753	763	773	783	793	803	813	823	833	10
437	844	854	864	874	884	894	904	914	924	934	10
438	945	955	965	975	985	995	605	615	625	635	10
439	646	656	666	676	686	696	706	716	726	736	10
440	747	757	767	777	787	797	807	817	827	837	10
441	848	858	868	878	888	898	908	918	928	938	10
442	949	959	969	979	989	999	609	619	629	639	10
443	640	650	660	670	680	690	700	710	720	730	10
444	741	751	761	771	781	791	801	811	821	831	10
445	842	852	862	872	882	892	902	912	922	932	10
446	943	953	963	973	983	993	603	613	623	633	10
447	644	654	664	674	684	694	704	714	724	734	10
448	745	755	765	775	785	795	805	815	825	835	10
449	846	856	866	876	886	896	906	916	926	936	10
450	947	957	967	977	987	997	607	617	627	637	10
451	648	658	668	678	688	698	708	718	728	738	10
452	749	759	769	779	789	799	809	819	829	839	10
453	840	850	860	870	880	890	900	910	920	930	10
454	941	951	961	971	981	991	601	611	621	631	10
455	642	652	662	672	682	692	702	712	722	732	10
456	743	753	763	773	783	793	803	813	823	833	10
457	844	854	864	874	884	894	904	914	924	934	10
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460	66276	280	283	304	314	323	332	342	351	361	9
461	70	380	383	398	408	417	427	436	445	455	9
462	154	474	483	492	502	511	521	530	539	549	9
463	338	607	577	586	596	605	614	624	633	642	9
464	62	661	671	680	689	699	708	717	727	736	9
465	745	755	764	773	783	792	801	811	820	829	9
466	831	848	857	867	876	885	894	904	913	922	9
467	862	941	950	960	969	978	987	997	1006	1015	9
468	67023	054	043	052	062	071	080	089	099	108	9
469	117	127	136	145	154	164	173	182	191	201	9
470	210	219	228	237	247	256	265	274	284	293	9
471	302	311	321	330	339	348	357	367	376	385	9
472	394	403	413	422	431	440	449	459	468	477	9
473	486	495	504	514	523	532	541	550	560	569	9
474	578	587	596	605	614	624	633	642	651	660	9
475	669	679	688	697	706	715	724	733	742	752	9
476	761	770	779	788	797	806	815	825	834	843	9
477	852	861	870	879	888	897	906	915	925	934	9
478	943	952	961	970	979	988	997	1006	1015	1024	9
479	68034	043	052	061	070	079	088	097	106	115	9
480	124	133	142	151	160	169	178	187	196	205	9
481	210	219	228	237	246	255	264	273	282	291	9
482	300	309	318	327	336	345	354	363	372	381	9
483	390	399	408	417	426	435	444	453	462	471	9
484	480	489	498	507	516	525	534	543	552	561	9
485	570	579	588	597	606	615	624	633	642	651	9
486	660	669	678	687	696	705	714	723	732	741	9
487	750	759	768	777	786	795	804	813	822	831	9
488	840	849	858	867	876	885	894	903	912	921	9
489	930	939	948	957	966	975	984	993	1002	1011	9
490	69021	028	037	046	055	064	073	082	091	100	9
491	108	117	126	135	144	153	162	171	180	189	9
492	197	206	215	224	233	242	251	260	269	278	9
493	286	295	304	313	322	331	340	349	358	367	9
494	376	385	394	403	412	421	430	439	448	457	9
495	466	475	484	493	502	511	520	529	538	547	9
496	556	565	574	583	592	601	610	619	628	637	9
497	646	655	664	673	682	691	700	709	718	727	9
498	736	745	754	763	772	781	790	799	808	817	9
499	826	835	844	853	862	871	880	889	898	907	9
500	916	925	934	943	952	961	970	979	988	997	9
501	944	953	962	971	980	989	998	1007	1016	1025	9
502	70070	079	088	097	106	115	124	133	142	151	9
503	157	166	175	184	193	202	211	220	229	238	9
504	247	256	265	274	283	292	301	310	319	328	9

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505	70329	338	346	355	364	372	381	389	398	406	9
506	415	424	432	441	449	458	467	475	484	492	9
507	501	509	518	526	535	544	552	561	569	578	9
508	586	595	603	612	621	629	638	646	655	664	9
509	672	680	689	697	706	714	723	731	740	749	9
510	757	766	774	783	791	800	808	817	825	834	9
511	842	851	859	868	876	885	893	902	910	919	9
512	927	935	944	952	961	969	978	986	995	1003	9
513	71012	020	029	037	046	054	063	071	079	088	8
514	096	105	113	122	130	139	147	155	164	172	8
515	181	189	198	206	214	223	231	240	248	257	8
516	265	273	282	290	299	307	315	324	332	341	8
517	349	357	366	374	383	391	399	408	416	425	8
518	433	441	450	458	466	475	483	492	500	508	8
519	517	525	533	542	550	559	567	575	584	592	8
520	600	609	617	625	634	642	650	659	667	675	8
521	684	692	700	709	717	725	734	742	750	759	8
522	767	775	784	792	801	809	817	825	834	842	8
523	850	858	867	875	884	892	900	908	917	925	8
524	933	941	950	958	966	975	983	991	999	1008	8
525	1016	1024	1032	1041	1049	1057	1066	1074	1082	1090	8
526	1099	1107	1115	1123	1132	1140	1148	1156	1165	1173	8
527	1181	1189	1198	1206	1214	1222	1230	1239	1247	1255	8
528	1263	1271	1280	1288	1296	1304	1313	1321	1329	1337	8
529	1346	1354	1362	1370	1378	1387	1395	1403	1411	1419	8
530	1428	1436	1444	1452	1460	1469	1477	1485	1493	1501	8
531	1510	1518	1526	1534	1542	1550	1558	1567	1575	1583	8
532	1591	1599	1607	1616	1624	1632	1640	1648	1656	1665	8
533	1673	1681	1689	1697	1705	1713	1722	1730	1738	1746	8
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535	1835	1843	1851	1859	1867	1876	1884	1892	1900	1908	8
536	1916	1924	1932	1940	1948	1956	1965	1973	1981	1989	8
537	1997	2005	2013	2021	2029	2037	2046	2054	2062	2070	8
538	71078	086	094	102	111	119	127	135	143	151	8
539	159	167	175	183	191	199	207	215	223	231	8
540	239	247	255	263	272	280	288	296	304	312	8
541	320	328	336	344	352	360	368	376	384	392	8
542	400	408	416	424	432	440	448	456	464	472	8
543	480	488	496	504	512	520	528	536	544	552	8
544	560	568	576	584	592	600	608	616	624	632	8
545	640	648	656	664	672	680	688	696	704	712	8
546	720	728	736	744	752	760	768	776	784	792	8
547	800	808	816	824	832	840	848	856	864	872	8
548	880	888	896	904	912	920	928	936	944	952	8
549	960	968	976	984	992	1000	1008	1016	1024	1032	8

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500	74	6	044	052	060	076	084	092	099	107	8
501	115	125	134	142	147	155	162	170	178	186	8
502	194	202	210	218	225	233	241	249	257	265	8
503	273	280	288	296	304	312	320	327	335	343	8
504	351	358	367	374	382	390	398	406	414	421	8
505	429	437	445	453	461	468	476	484	492	500	8
506	507	515	523	531	539	547	554	562	570	578	8
507	586	593	601	609	617	624	632	640	648	656	8
508	663	671	679	687	695	702	710	718	726	733	8
509	741	749	757	764	772	780	788	796	803	811	8
510	819	827	834	842	850	858	865	873	881	889	8
511	896	904	912	920	927	935	943	950	958	966	8
512	974	981	989	997	005	012	020	028	035	043	8
513	7001	009	006	014	082	089	097	105	112	120	8
514	128	136	143	151	159	166	174	182	189	197	8
515	205	213	220	228	236	243	251	259	266	274	8
516	282	289	297	305	312	320	328	335	343	351	8
517	358	366	374	381	389	397	404	411	419	427	8
518	435	442	450	458	465	473	481	488	495	504	8
519	511	519	526	534	542	549	557	565	572	580	8
520	587	595	603	610	618	626	633	641	648	656	8
521	664	671	679	686	694	702	709	717	724	732	8
522	740	747	755	762	770	778	785	793	800	808	8
523	815	823	831	838	846	853	861	868	876	884	8
524	891	899	906	914	921	929	937	944	952	959	8
525	967	974	982	989	997	005	012	020	028	035	8
526	70012	050	057	064	072	080	087	095	102	110	8
527	118	125	133	140	148	155	163	170	178	186	8
528	193	200	208	215	223	230	238	245	253	260	8
529	268	275	283	290	298	305	313	320	328	335	8
530	343	350	358	365	373	381	388	396	403	411	8
531	418	425	433	440	448	455	463	470	478	485	8
532	492	500	507	515	522	530	537	545	552	560	8
533	567	574	582	589	597	604	612	619	627	634	8
534	641	649	656	664	671	678	686	693	701	708	8
535	716	723	730	738	745	753	760	768	775	782	8
536	790	797	805	812	820	827	834	842	850	857	8
537	864	871	879	886	893	901	908	916	923	931	8
538	938	945	953	960	967	975	982	989	997	004	8
539	77012	019	026	034	041	048	056	063	070	078	8
540	085	093	100	107	115	122	129	137	144	151	8
541	159	166	173	181	188	195	203	210	217	225	8
542	232	240	247	254	262	269	276	283	291	298	8
543	305	313	320	327	335	342	349	357	364	371	8
544	379	386	394	401	408	415	422	430	437	444	8
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596	525	532	539	546	554	561	568	576	583	590	7
597	597	605	612	619	627	634	641	648	656	663	7
598	670	677	685	692	699	706	714	721	728	735	7
599	743	750	757	764	772	779	786	793	801	808	7
600	815	822	830	837	844	851	859	866	873	880	7
601	887	895	902	909	916	924	931	938	945	952	7
602	960	967	974	981	988	996	003	010	017	025	7
603	78032	039	046	053	061	068	075	082	089	097	7
604	104	111	118	125	132	140	147	154	161	168	7
605	176	183	190	197	204	211	219	226	233	240	7
606	247	254	262	269	276	283	290	297	305	312	7
607	319	326	333	340	347	355	362	369	376	383	7
608	390	398	405	412	419	426	433	440	447	455	7
609	462	469	476	483	490	497	504	512	519	526	7
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611	604	611	618	625	633	640	647	654	661	668	7
612	674	682	689	696	704	711	718	725	732	739	7
613	746	753	760	767	774	781	789	796	803	810	7
614	817	824	831	838	845	852	859	866	873	880	7
615	888	895	902	909	916	923	930	937	944	951	7
616	958	965	972	979	986	993	000	007	014	021	7
617	023	030	037	044	051	058	065	072	079	086	7
618	094	101	108	115	122	129	136	143	150	157	7
619	164	171	178	185	192	200	207	214	221	228	7
620	234	241	248	255	262	270	277	284	291	298	7
621	305	312	319	326	333	340	347	354	361	368	7
622	375	382	389	396	403	410	417	424	431	438	7
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624	515	522	529	536	543	550	557	564	571	578	7
625	585	592	599	606	613	620	627	634	641	648	7
626	655	662	669	676	683	690	697	704	711	718	7
627	725	732	739	746	753	760	767	774	781	788	7
628	795	802	809	816	823	830	837	844	851	858	7
629	865	872	879	886	893	900	906	913	920	927	7
630	934	941	948	955	962	969	975	982	989	996	7
631	003	010	017	024	030	037	044	051	058	065	7
632	072	079	086	092	099	106	113	120	127	134	7
633	140	147	154	161	168	175	182	188	195	202	7
634	210	217	224	230	236	243	250	257	264	271	7
635	277	284	291	298	305	312	318	325	332	339	7
636	346	353	359	366	373	380	387	393	400	407	7
637	414	421	428	434	441	448	455	462	468	475	7
638	482	489	496	502	509	516	523	530	536	543	7
639	550	557	564	570	577	584	591	598	604	611	7
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615	893	963	669	656	653	660	666	672	679	686	7
616	894	030	670	657	654	661	667	673	680	687	7
617	895	097	671	658	655	662	668	674	681	688	7
618	896	164	672	659	656	663	669	675	682	689	7
619	897	231	673	660	657	664	670	676	683	690	7
620	898	298	674	661	658	665	671	677	684	691	7
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622	900	431	676	663	660	667	673	679	686	693	7
623	901	498	677	664	661	668	674	680	687	694	7
624	902	564	678	665	662	669	675	681	688	695	7
625	903	631	679	666	663	670	676	682	689	700	7
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627	905	764	681	668	665	672	678	684	691	702	7
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637	915	431	691	678	675	682	688	694	701	712	7
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648	926	164	702	689	686	693	699	705	712	723	7
649	927	231	703	690	687	694	700	706	713	724	7
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651	929	365	705	692	689	696	702	708	715	726	7
652	930	431	706	693	690	697	703	709	716	727	7
653	931	498	707	694	691	698	704	710	717	728	7
654	932	564	708	695	692	699	705	711	718	729	7
655	933	631	709	696	693	700	706	712	719	730	7
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657	935	764	711	698	695	702	708	714	721	732	7
658	936	830	712	699	696	703	709	715	722	733	7
659	937	897	713	700	697	704	710	716	723	734	7
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661	939	030	715	702	699	706	712	718	725	736	7
662	940	097	716	703	700	707	713	719	726	737	7
663	941	164	717	704	701	708	714	720	727	738	7
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665	943	298	719	706	703	710	716	722	729	740	7
666	944	365	720	707	704	711	717	723	730	741	7
667	945	431	721	708	705	712	718	724	731	742	7
668	946	498	722	709	706	713	719	725	732	743	7
669	947	564	723	710	707	714	720	726	733	744	7
670	948	631	724	711	708	715	721	727	734	745	7
671	949	697	725	712	709	716	722	728	735	746	7
672	950	764	726	713	710	717	723	729	736	747	7
673	951	830	727	714	711	718	724	730	737	748	7
674	952	897	728	715	712	719	725	731	738	749	7
675	953	963	729	716	713	720	726	732	739	750	7
676	954	030	730	717	714	721	727	733	740	751	7
677	955	097	731	718	715	722	728	734	741	752	7
678	956	164	732	719	716	723	729	735	742	753	7
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688	739	765	771	778	784	790	797	803	809	816	6
689	822	828	835	841	847	853	860	866	872	879	6
690	885	891	897	904	910	916	923	929	935	942	6
691	948	954	960	967	973	979	985	992	998	004	6
692	84014	017	023	029	036	042	048	055	061	067	6
693	075	080	086	092	098	105	111	117	123	130	6
694	136	142	148	155	161	167	173	180	186	192	6
695	198	205	211	217	223	230	236	242	248	255	6
696	264	267	273	280	286	292	298	305	311	317	6
697	323	330	336	342	348	354	361	367	373	379	6
698	387	392	398	404	410	417	423	429	435	442	6
699	448	454	460	466	473	479	485	491	497	504	6
700	510	516	522	528	535	541	547	553	559	566	6
701	572	578	584	590	597	603	609	615	621	628	6
702	641	647	653	659	665	671	677	683	689	696	6
703	709	715	721	727	733	739	745	751	757	764	6
704	771	777	783	789	795	801	807	813	819	826	6
705	838	844	850	856	862	868	874	880	886	893	6
706	899	905	911	917	923	929	935	941	947	953	6
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708	019	025	031	037	043	049	055	061	067	073	6
709	079	085	091	097	103	109	115	121	127	133	6
710	139	145	151	157	163	169	175	181	187	193	6
711	199	205	211	217	223	229	235	241	247	253	6
712	259	265	271	277	283	289	295	301	307	313	6
713	319	325	331	337	343	349	355	361	367	373	6
714	379	385	391	397	403	409	415	421	427	433	6
715	439	445	451	457	463	469	475	481	487	493	6
716	499	505	511	517	523	529	535	541	547	553	6
717	559	565	571	577	583	589	595	601	607	613	6
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722	859	865	871	877	883	889	895	901	907	913	6
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724	979	985	991	997	003	009	015	021	027	033	6
725	039	045	051	057	063	069	075	081	087	093	6
726	099	105	111	117	123	129	135	141	147	153	6
727	159	165	171	177	183	189	195	201	207	213	6
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732	16	22	50	11	17	23	29	35	41	47	6
733	20	26	51	12	18	24	30	36	42	48	6
734	24	30	52	13	19	25	31	37	43	49	6
735	28	34	53	14	20	26	32	38	44	50	6
736	32	38	54	15	21	27	33	39	45	51	6
737	36	42	55	16	22	28	34	40	46	52	6
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742	56	62	60	21	27	33	39	45	51	57	6
743	60	66	61	22	28	34	40	46	52	58	6
744	64	70	62	23	29	35	41	47	53	59	6
745	68	74	63	24	30	36	42	48	54	60	6
746	72	78	64	25	31	37	43	49	55	61	6
747	76	82	65	26	32	38	44	50	56	62	6
748	80	86	66	27	33	39	45	51	57	63	6
749	84	90	67	28	34	40	46	52	58	64	6
750	88	94	68	29	35	41	47	53	59	65	6
751	92	98	69	30	36	42	48	54	60	66	6
752	96	102	70	31	37	43	49	55	61	67	6
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754	104	110	72	33	39	45	51	57	63	69	6
755	108	114	73	34	40	46	52	58	64	70	6
756	112	118	74	35	41	47	53	59	65	71	6
757	116	122	75	36	42	48	54	60	66	72	6
758	120	126	76	37	43	49	55	61	67	73	6
759	124	130	77	38	44	50	56	62	68	74	6
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762	136	142	80	41	47	53	59	65	71	77	6
763	140	146	81	42	48	54	60	66	72	78	6
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765	148	154	83	44	50	56	62	68	74	80	6
766	152	158	84	45	51	57	63	69	75	81	6
767	156	162	85	46	52	58	64	70	76	82	6
768	160	166	86	47	53	59	65	71	77	83	6
769	164	170	87	48	54	60	66	72	78	84	6
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771	172	178	89	50	56	62	68	74	80	86	6
772	176	182	90	51	57	63	69	75	81	87	6
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777	89042	048	053	059	064	070	076	081	087	092	6
778	098	104	109	115	120	126	131	137	143	148	6
779	154	159	165	170	176	182	187	193	198	204	6
780	209	215	221	226	232	237	243	248	254	260	6
781	265	271	276	282	287	293	298	304	310	315	6
782	321	326	332	337	343	348	354	360	365	371	6
783	376	382	387	393	398	404	409	415	421	426	6
784	432	437	443	448	454	459	465	470	476	481	6
785	487	492	498	504	509	515	520	526	531	537	6
786	542	548	553	559	564	570	575	581	586	592	6
787	597	603	609	614	620	625	631	636	642	647	6
788	652	658	664	669	675	680	686	691	697	702	6
789	708	713	719	724	730	735	741	746	752	757	6
790	762	768	774	779	785	790	796	801	807	812	5
791	818	823	829	834	840	845	851	856	862	867	5
792	872	878	883	889	894	900	905	911	916	922	5
793	927	932	938	944	949	955	960	966	971	977	5
794	982	988	993	998	1004	1009	1015	1020	1026	1031	5
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796	1091	1097	1102	1108	1113	1119	1124	1130	1135	1140	5
797	1145	1151	1157	1162	1168	1173	1179	1184	1189	1195	5
798	1200	1206	1211	1217	1222	1227	1233	1238	1244	1249	5
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801	1363	1369	1374	1380	1385	1390	1396	1401	1407	1412	5
802	1417	1423	1428	1434	1439	1445	1450	1456	1461	1466	5
803	1471	1477	1482	1488	1493	1499	1504	1510	1515	1520	5
804	1525	1531	1536	1542	1547	1553	1558	1564	1569	1574	5
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812	1955	1961	1966	1971	1977	1982	1988	1993	1998	2004	5
813	2009	2014	2020	2025	2030	2036	2041	2047	2052	2057	5
814	2062	2068	2073	2078	2084	2089	2094	2100	2105	2110	5
815	2115	2121	2126	2131	2137	2142	2148	2153	2158	2164	5
816	2169	2174	2180	2185	2190	2196	2201	2207	2212	2217	5
817	2222	2228	2233	2238	2243	2249	2254	2260	2265	2270	5
818	2275	2281	2286	2291	2297	2302	2307	2312	2318	2323	5
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823	540	545	551	556	561	566	572	577	582	587	5
824	593	598	603	609	614	619	624	630	635	640	5
825	645	651	656	661	666	672	677	682	687	693	5
826	698	703	709	714	719	724	730	735	740	745	5
827	747	753	758	764	769	774	780	785	790	795	5
828	800	806	811	816	821	827	832	837	843	848	5
829	853	858	863	869	874	879	884	890	895	900	5
830	905	910	915	921	926	931	936	941	946	951	5
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834	1105	1110	1115	1121	1126	1131	1136	1141	1146	1151	5
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836	1205	1210	1215	1221	1226	1231	1236	1241	1246	1251	5
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841	1456	1461	1466	1471	1476	1481	1486	1491	1496	1500	5
842	1505	1510	1515	1521	1526	1531	1536	1541	1546	1551	5
843	1556	1561	1566	1571	1576	1581	1586	1591	1596	1600	5
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846	1705	1710	1715	1721	1726	1731	1736	1741	1746	1751	5
847	1756	1761	1766	1771	1776	1781	1786	1791	1796	1800	5
848	1805	1810	1815	1821	1826	1831	1836	1841	1846	1851	5
849	1856	1861	1866	1871	1876	1881	1886	1891	1896	1900	5
850	1905	1910	1915	1921	1926	1931	1936	1941	1946	1951	5
851	1956	1961	1966	1971	1976	1981	1986	1991	1996	2000	5
852	2005	2010	2015	2021	2026	2031	2036	2041	2046	2051	5
853	2056	2061	2066	2071	2076	2081	2086	2091	2096	2100	5
854	2105	2110	2115	2121	2126	2131	2136	2141	2146	2151	5
855	2156	2161	2166	2171	2176	2181	2186	2191	2196	2200	5
856	2205	2210	2215	2221	2226	2231	2236	2241	2246	2251	5
857	2256	2261	2266	2271	2276	2281	2286	2291	2296		

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865	3502	707	712	717	722	727	732	737	742	747	5
866	752	757	762	767	772	777	782	787	792	797	5
867	802	807	812	817	822	827	832	837	842	847	5
868	852	857	862	867	872	877	882	887	892	897	5
869	902	907	912	917	922	927	932	937	942	947	5
870	952	957	962	967	972	977	982	987	992	997	5
871	04002	007	012	017	022	027	032	037	042	047	5
872	052	057	062	067	072	077	082	087	091	096	5
873	101	106	111	116	121	126	131	136	141	146	5
874	151	156	161	166	171	176	181	186	191	196	5
875	201	206	211	216	221	226	231	246	240	245	5
876	251	255	260	265	270	275	280	285	290	295	5
877	301	305	310	315	320	325	330	335	340	345	5
878	346	354	359	364	369	374	379	384	389	394	5
879	399	404	409	414	419	424	429	435	438	443	5
880	448	453	458	463	468	473	478	483	488	493	5
881	498	503	507	512	517	522	527	532	537	542	5
882	547	552	557	562	567	571	576	581	586	591	5
883	596	601	606	611	616	621	626	630	635	640	5
884	645	650	655	660	665	670	675	680	685	689	5
885	694	699	704	709	714	719	724	729	734	738	5
886	743	748	753	758	763	768	773	778	783	787	5
887	792	797	802	807	812	817	822	827	832	836	5
888	841	846	851	856	861	866	871	876	880	885	5
889	889	895	900	905	910	915	919	924	929	934	5
890	939	944	949	954	959	963	968	973	978	983	5
891	988	993	998	002	007	012	017	022	027	032	5
892	037	041	046	051	056	061	066	071	075	080	5
893	085	090	095	100	105	109	114	119	124	129	5
894	134	139	145	148	153	158	163	168	173	177	5
895	182	187	192	197	202	207	211	216	221	226	5
896	231	236	241	246	251	255	260	265	270	274	5
897	279	284	289	294	299	303	308	313	318	323	5
898	328	332	337	342	347	352	357	361	366	371	5
899	376	381	386	390	395	400	405	410	415	419	5
900	424	429	434	439	444	448	453	458	463	468	5
901	473	477	482	487	492	497	501	506	511	516	5
902	521	526	530	535	540	545	550	554	559	564	5
903	569	574	578	583	588	593	598	602	607	612	5
904	617	622	626	631	636	641	646	650	655	660	5
905	665	670	674	679	684	689	694	698	703	708	5
906	713	718	722	727	731	737	742	746	751	756	5
907	761	766	771	775	780	785	789	794	799	804	5
908	809	813	818	823	828	832	837	842	847	852	5
909	856	861	866	871	875	880	885	890	895	899	5
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910	8004	8014	8024	8034	8044	8054	8064	8074	8084	8094	5
911	8104	8114	8124	8134	8144	8154	8164	8174	8184	8194	5
912	8204	8214	8224	8234	8244	8254	8264	8274	8284	8294	5
913	8304	8314	8324	8334	8344	8354	8364	8374	8384	8394	5
914	8404	8414	8424	8434	8444	8454	8464	8474	8484	8494	5
915	8504	8514	8524	8534	8544	8554	8564	8574	8584	8594	5
916	8604	8614	8624	8634	8644	8654	8664	8674	8684	8694	5
917	8704	8714	8724	8734	8744	8754	8764	8774	8784	8794	5
918	8804	8814	8824	8834	8844	8854	8864	8874	8884	8894	5
919	8904	8914	8924	8934	8944	8954	8964	8974	8984	8994	5
920	9004	9014	9024	9034	9044	9054	9064	9074	9084	9094	5
921	9104	9114	9124	9134	9144	9154	9164	9174	9184	9194	5
922	9204	9214	9224	9234	9244	9254	9264	9274	9284	9294	5
923	9304	9314	9324	9334	9344	9354	9364	9374	9384	9394	5
924	9404	9414	9424	9434	9444	9454	9464	9474	9484	9494	5
925	9504	9514	9524	9534	9544	9554	9564	9574	9584	9594	5
926	9604	9614	9624	9634	9644	9654	9664	9674	9684	9694	5
927	9704	9714	9724	9734	9744	9754	9764	9774	9784	9794	5
928	9804	9814	9824	9834	9844	9854	9864	9874	9884	9894	5
929	9904	9914	9924	9934	9944	9954	9964	9974	9984	9994	5
930	1004	1014	1024	1034	1044	1054	1064	1074	1084	1094	5
931	1104	1114	1124	1134	1144	1154	1164	1174	1184	1194	5
932	1204	1214	1224	1234	1244	1254	1264	1274	1284	1294	5
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935	1504	1514	1524	1534	1544	1554	1564	1574	1584	1594	5
936	1604	1614	1624	1634	1644	1654	1664	1674	1684	1694	5
937	1704	1714	1724	1734	1744	1754	1764	1774	1784	1794	5
938	1804	1814	1824	1834	1844	1854	1864	1874	1884	1894	5
939	1904	1914	1924	1934	1944	1954	1964	1974	1984	1994	5
940	2004	2014	2024	2034	2044	2054	2064	2074	2084	2094	5
941	2104	2114	2124	2134	2144	2154	2164	2174	2184	2194	5
942	2204	2214	2224	2234	2244	2254	2264	2274	2284	2294	5
943	2304	2314	2324	2334	2344	2354	2364	2374	2384	2394	5
944	2404	2414	2424	2434	2444	2454	2464	2474	2484	2494	5
945	2504	2514	2524	2534	2544	2554	2564	2574	2584	2594	5
946	2604	2614	2624	2634	2644	2654	2664	2674	2684	2694	5
947	2704	2714	2724	2734	2744	2754	2764	2774	2784	2794	5
948	2804	2814	2824	2834	2844	2854	2864	2874	2884	2894	5
949	2904	2914	2924	2934	2944	2954	2964	2974	2984	2994	5
950	3004	3014	3024	3034	3044	3054	3064	3074	3084	3094	5
951	3104	3114	3124	3134	3144	3154	3164	3174	3184	3194	5
952	3204	3214	3224	3234	3244	3254	3264	3274	3284	3294	5
953	3304	3314	3324	3334	3344	3354	3364	3374	3384	3394	5
954	3404	3414	3424	3434	3444	3454	3464	3474	3484	3494	5

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955	98000	98005	98010	98015	98020	98025	98030	98035	98040	98045	5
956	98050	98055	98060	98065	98070	98075	98080	98085	98090	98095	5
957	98100	98105	98110	98115	98120	98125	98130	98135	98140	98145	5
958	98150	98155	98160	98165	98170	98175	98180	98185	98190	98195	5
959	98200	98205	98210	98215	98220	98225	98230	98235	98240	98245	5
960	98250	98255	98260	98265	98270	98275	98280	98285	98290	98295	5
961	98300	98305	98310	98315	98320	98325	98330	98335	98340	98345	5
962	98350	98355	98360	98365	98370	98375	98380	98385	98390	98395	5
963	98400	98405	98410	98415	98420	98425	98430	98435	98440	98445	5
964	98450	98455	98460	98465	98470	98475	98480	98485	98490	98495	5
965	98500	98505	98510	98515	98520	98525	98530	98535	98540	98545	5
966	98550	98555	98560	98565	98570	98575	98580	98585	98590	98595	5
967	98600	98605	98610	98615	98620	98625	98630	98635	98640	98645	5
968	98650	98655	98660	98665	98670	98675	98680	98685	98690	98695	5
969	98700	98705	98710	98715	98720	98725	98730	98735	98740	98745	5
970	98750	98755	98760	98765	98770	98775	98780	98785	98790	98795	5
971	98800	98805	98810	98815	98820	98825	98830	98835	98840	98845	5
972	98850	98855	98860	98865	98870	98875	98880	98885	98890	98895	5
973	98900	98905	98910	98915	98920	98925	98930	98935	98940	98945	5
974	98950	98955	98960	98965	98970	98975	98980	98985	98990	98995	5
975	99000	99005	99010	99015	99020	99025	99030	99035	99040	99045	5
976	99050	99055	99060	99065	99070	99075	99080	99085	99090	99095	5
977	99100	99105	99110	99115	99120	99125	99130	99135	99140	99145	5
978	99150	99155	99160	99165	99170	99175	99180	99185	99190	99195	5
979	99200	99205	99210	99215	99220	99225	99230	99235	99240	99245	5
980	99250	99255	99260	99265	99270	99275	99280	99285	99290	99295	5
981	99300	99305	99310	99315	99320	99325	99330	99335	99340	99345	5
982	99350	99355	99360	99365	99370	99375	99380	99385	99390	99395	5
983	99400	99405	99410	99415	99420	99425	99430	99435	99440	99445	5
984	99450	99455	99460	99465	99470	99475	99480	99485	99490	99495	5
985	99500	99505	99510	99515	99520	99525	99530	99535	99540	99545	5
986	99550	99555	99560	99565	99570	99575	99580	99585	99590	99595	5
987	99600	99605	99610	99615	99620	99625	99630	99635	99640	99645	5
988	99650	99655	99660	99665	99670	99675	99680	99685	99690	99695	5
989	99700	99705	99710	99715	99720	99725	99730	99735	99740	99745	5
990	99750	99755	99760	99765	99770	99775	99780	99785	99790	99795	5
991	99800	99805	99810	99815	99820	99825	99830	99835	99840	99845	5
992	99850	99855	99860	99865	99870	99875	99880	99885	99890	99895	5
993	99900	99905	99910	99915	99920	99925	99930	99935	99940	99945	5
994	99950	99955	99960	99965	99970	99975	99980	99985	99990	99995	5
995	100000	100005	100010	100015	100020	100025	100030	100035	100040	100045	5
996	100050	100055	100060	100065	100070	100075	100080	100085	100090	100095	5
997	100100	100105	100110	100115	100120	100125	100130	100135	100140	100145	5
998	100150	100155	100160	100165	100170	100175	100180	100185	100190	100195	5
999	100200	100205	100210	100215	100220	100225	100230	100235	100240	100245	5

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1000	0000	004	009	013	017	022	026	030	035	039	4
1001	043	048	052	056	061	065	069	074	078	082	4
1002	087	091	095	100	104	108	113	117	121	126	4
1003	130	134	139	143	147	152	156	160	165	169	4
1004	173	178	182	186	191	195	199	204	208	212	4
1005	217	221	225	230	234	238	243	247	251	255	4
1006	260	264	268	273	277	281	286	290	294	299	4
1007	303	307	312	316	320	325	329	333	337	342	4
1008	346	350	355	359	363	368	372	376	381	385	4
1009	389	393	398	402	406	411	415	419	424	428	4
1010	432	436	441	445	449	454	458	462	467	471	4
1011	475	479	484	488	492	497	501	505	510	514	4
1012	518	522	527	531	535	540	544	548	553	557	4
1013	561	565	570	574	578	582	587	591	595	600	4
1014	604	608	612	617	621	625	629	634	638	642	4
1015	647	651	655	659	664	668	672	677	681	685	4
1016	689	693	698	702	706	711	715	719	723	728	4
1017	732	736	741	745	749	753	758	762	767	771	4
1018	775	779	783	788	792	796	800	805	809	813	4
1019	817	822	826	830	834	839	843	847	851	856	4
1020	860	864	869	873	877	881	886	890	894	898	4
1021	903	907	911	915	920	924	928	932	937	941	4
1022	945	949	954	958	962	966	971	975	979	983	4
1023	988	992	996	1000	1005	1009	1013	1017	1021	1025	4
1024	01030	034	038	043	047	051	055	059	063	067	4
1025	072	077	081	085	089	094	098	100	104	108	4
1026	113	117	121	125	129	133	137	141	145	149	4
1027	153	157	161	165	170	174	178	182	186	190	4
1028	194	198	202	206	210	214	218	222	226	230	4
1029	234	238	242	246	250	254	258	262	266	270	4
1030	274	278	282	286	290	294	298	302	306	310	4
1031	314	318	322	326	330	334	338	342	346	350	4
1032	354	358	362	366	370	374	378	382	386	390	4
1033	394	398	402	406	410	414	418	422	426	430	4
1034	434	438	442	446	450	454	458	462	466	470	4
1035	474	478	482	486	490	494	498	502	506	510	4
1036	514	518	522	526	530	534	538	542	546	550	4
1037	554	558	562	566	570	574	578	582	586	590	4
1038	594	598	602	606	610	614	618	622	626	630	4
1039	634	638	642	646	650	654	658	662	666	670	4
1040	674	678	682	686	690	694	698	702	706	710	4
1041	714	718	722	726	730	734	738	742	746	750	4
1042	754	758	762	766	770	774	778	782	786	790	4
1043	794	798	802	806	810	814	818	822	826	830	4
1044	834	838	842	846	850	854	858	862	866	870	4

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1045	01912	916	920	924	928	932	937	941	945	949	4
1046	953	957	961	966	970	974	978	982	986	991	4
1047	995	999	1003	1007	1011	1015	1020	1024	1028	1032	4
1048	02936	040	044	049	053	057	061	065	069	073	4
1049	078	082	086	090	094	098	102	107	111	115	4
1050	119	123	127	131	135	140	144	148	152	156	4
1051	160	164	169	173	177	181	185	189	193	197	4
1052	202	206	210	214	218	222	226	230	235	239	4
1053	243	247	251	255	259	263	268	272	276	280	4
1054	284	288	292	296	301	305	309	313	317	321	4
1055	325	329	333	338	342	346	350	354	358	362	4
1056	366	371	375	379	383	387	391	395	399	403	4
1057	407	412	416	420	424	428	432	436	440	444	4
1058	449	453	457	461	465	469	473	477	481	485	4
1059	489	493	498	502	506	510	514	518	522	526	4
1060	531	535	539	543	547	551	555	559	563	567	4
1061	571	575	580	584	588	592	596	600	604	608	4
1062	612	617	621	625	629	633	637	641	645	649	4
1063	653	657	661	665	670	674	678	682	686	690	4
1064	694	698	702	706	710	715	719	723	727	731	4
1065	735	739	743	747	751	755	759	763	768	772	4
1066	776	780	784	788	792	796	800	804	808	812	4
1067	816	820	824	829	833	837	841	845	849	853	4
1068	857	861	865	869	873	877	882	886	890	894	4
1069	898	902	906	910	914	918	922	926	930	934	4
1070	938	942	946	951	955	959	963	967	971	975	4
1071	979	983	987	991	995	999	1003	1007	1011	1015	4
1072	03019	024	028	032	036	040	044	048	052	056	4
1073	060	064	068	072	076	080	084	088	092	096	4
1074	100	104	109	113	117	121	125	129	133	137	4
1075	141	145	149	153	157	161	165	169	173	177	4
1076	181	185	189	193	197	201	205	209	214	218	4
1077	222	226	230	234	238	242	246	250	254	258	4
1078	262	266	270	274	278	282	286	290	294	298	4
1079	302	306	310	314	318	322	326	330	334	338	4
1080	342	346	350	354	358	362	366	371	375	379	4
1081	383	387	391	395	399	403	407	411	415	419	4
1082	423	427	431	435	439	443	447	451	455	459	4
1083	463	467	471	475	479	483	487	491	495	499	4
1084	503	507	511	515	519	523	527	531	535	539	4
1085	543	547	551	555	559	563	567	571	575	579	4
1086	583	587	591	595	599	603	607	611	615	619	4
1087	623	627	631	635	639	643	647	651	655	659	4
1088	663	667	671	675	679	683	687	691	695	699	4
1089	703	707	711	715	719	723	727	731	735	739	4

II. NATURAL SINES.

Deg.	0	10	20	30	40	50		Deg.
0	00000	00291	00582	00873	01164	01454	01745	89
1	00743	01036	01327	01618	01908	02199	02490	88
2	01440	01731	02021	02312	02603	02893	03184	87
3	02484	02774	03064	03355	03645	03935	04226	86
4	04376	04666	04956	05246	05536	05826	06116	85
5	06406	06696	06986	07276	07566	07856	08146	84
6	08436	08726	09016	09306	09596	09886	10176	83
7	10466	10756	11046	11336	11626	11916	12206	82
8	12496	12786	13076	13366	13656	13946	14236	81
9	14526	14816	15106	15396	15686	15976	16266	80
10	16556	16846	17136	17426	17716	18006	18296	79
11	18586	18876	19166	19456	19746	20036	20326	78
12	20616	20906	21196	21486	21776	22066	22356	77
13	22646	22936	23226	23516	23806	24096	24386	76
14	24676	24966	25256	25546	25836	26126	26416	75
15	26706	26996	27286	27576	27866	28156	28446	74
16	28736	29026	29316	29606	29896	30186	30476	73
17	30766	31056	31346	31636	31926	32216	32506	72
18	32796	33086	33376	33666	33956	34246	34536	71
19	34826	35116	35406	35696	35986	36276	36566	70
20	36856	37146	37436	37726	38016	38306	38596	69
21	38886	39176	39466	39756	40046	40336	40626	68
22	40916	41206	41496	41786	42076	42366	42656	67
23	42946	43236	43526	43816	44106	44396	44686	66
24	44976	45266	45556	45846	46136	46426	46716	65
25	47006	47296	47586	47876	48166	48456	48746	64
26	49036	49326	49616	49906	50196	50486	50776	63
27	51066	51356	51646	51936	52226	52516	52806	62
28	53096	53386	53676	53966	54256	54546	54836	61
29	55126	55416	55706	55996	56286	56576	56866	60
30	57156	57446	57736	58026	58316	58606	58896	59
31	59186	59476	59766	60056	60346	60636	60926	58
32	61216	61506	61796	62086	62376	62666	62956	57
33	63246	63536	63826	64116	64406	64696	64986	56
34	65276	65566	65856	66146	66436	66726	67016	55
35	67306	67596	67886	68176	68466	68756	69046	54
36	69336	69626	69916	70206	70496	70786	71076	53
37	71366	71656	71946	72236	72526	72816	73106	52
38	73396	73686	73976	74266	74556	74846	75136	51
39	75426	75716	76006	76296	76586	76876	77166	50
40	77456	77746	78036	78326	78616	78906	79196	49
41	79486	79776	80066	80356	80646	80936	81226	48
42	81516	81806	82096	82386	82676	82966	83256	47
43	83546	83836	84126	84416	84706	84996	85286	46
44	85576	85866	86156	86446	86736	87026	87316	45
Deg.	50	40	30	20	10	0		Deg.

NATURAL COSINES

21

II. NATURAL SINES.

Deg.	0	10	20	30	40	50		Deg.
45	70711	70916	71121	71325	71529	71732	71934	44
46	72137	72340	72543	72745	72947	73148	73349	43
47	73551	73752	73953	74154	74355	74556	74757	42
48	74958	75159	75360	75561	75762	75963	76164	41
49	76365	76566	76767	76968	77169	77370	77571	40
50	77772	77973	78174	78375	78576	78777	78978	39
51	79179	79380	79581	79782	79983	80184	80385	38
52	80586	80787	80988	81189	81390	81591	81792	37
53	81993	82194	82395	82596	82797	82998	83199	36
54	83400	83601	83802	84003	84204	84405	84606	35
55	84807	85008	85209	85410	85611	85812	86013	34
56	86214	86415	86616	86817	87018	87219	87420	33
57	87621	87822	88023	88224	88425	88626	88827	32
58	89028	89229	89430	89631	89832	90033	90234	31
59	90435	90636	90837	91038	91239	91440	91641	30
60	91842	92043	92244	92445	92646	92847	93048	29
61	93249	93450	93651	93852	94053	94254	94455	28
62	94656	94857	95058	95259	95460	95661	95862	27
63	96063	96264	96465	96666	96867	97068	97269	26
64	97470	97671	97872	98073	98274	98475	98676	25
65	98877	99078	99279	99480	99681	99882	100083	24
66	100284	100485	100686	100887	101088	101289	101490	23
67	101691	101892	102093	102294	102495	102696	102897	22
68	103098	103299	103500	103701	103902	104103	104304	21
69	104505	104706	104907	105108	105309	105510	105711	20
70	105912	106113	106314	106515	106716	106917	107118	19
71	107319	107520	107721	107922	108123	108324	108525	18
72	108726	108927	109128	109329	109530	109731	109932	17
73	110133	110334	110535	110736	110937	111138	111339	16
74	111540	111741	111942	112143	112344	112545	112746	15
75	112947	113148	113349	113550	113751	113952	114153	14
76	114354	114555	114756	114957	115158	115359	115560	13
77	115761	115962	116163	116364	116565	116766	116967	12
78	117168	117369	117570	117771	117972	118173	118374	11
79	118575	118776	118977	119178	119379	119580	119781	10
80	119982	120183	120384	120585	120786	120987	121188	9
81	121389	121590	121791	121992	122193	122394	122595	8
82	122796	122997	123198	123399	123600	123801	124002	7
83	124203	124404	124605	124806	125007	125208	125409	6
84	125610	125811	126012	126213	126414	126615	126816	5
85	127017	127218	127419	127620	127821	128022	128223	4
86	128424	128625	128826	129027	129228	129429	129630	3
87	129831	130032	130233	130434	130635	130836	131037	2
88	131238	131439	131640	131841	132042	132243	132444	1
89	132645	132846	133047	133248	133449	133650	133851	0
Deg.	50	40	30	20	10	0		Deg.

NATURAL COSINES

22

III. NATURAL TANGENTS.

[illegible]

NATURAL COTANGENTS

444

III.—NATURAL TANGENTS.

Deg.	0'	10'	20'	30'	40'	50	Deg.
45	1.00000	1.0058	1.0117	1.0176	1.0235	1.0294	44
46	1.0353	1.0413	1.0476	1.0538	1.0599	1.0661	43
47	1.0723	1.0786	1.0849	1.0913	1.0976	1.1041	42
48	1.1106	1.1171	1.1236	1.1302	1.1369	1.1436	41
49	1.1503	1.1571	1.1639	1.1708	1.1777	1.1847	40
50	1.1917	1.1988	1.2059	1.2130	1.2201	1.2273	39
51	1.2346	1.2427	1.2499	1.2571	1.2643	1.2726	38
52	1.2799	1.2874	1.2949	1.3025	1.3101	1.3178	37
53	1.3254	1.3331	1.3408	1.3486	1.3564	1.3643	36
54	1.3721	1.3800	1.3879	1.3958	1.4038	1.4118	35
55	1.4215	1.4313	1.4411	1.4509	1.4608	1.4707	34
56	1.4826	1.4926	1.5026	1.5126	1.5226	1.5327	33
57	1.5437	1.5539	1.5641	1.5743	1.5846	1.5949	32
58	1.6052	1.6156	1.6260	1.6365	1.6470	1.6575	31
59	1.6681	1.6787	1.6893	1.6999	1.7106	1.7213	30
60	1.7320	1.7428	1.7536	1.7644	1.7753	1.7862	29
61	1.8013	1.8123	1.8233	1.8343	1.8454	1.8565	28
62	1.8676	1.8788	1.8899	1.9011	1.9123	1.9235	27
63	1.9348	1.9461	1.9574	1.9687	1.9800	1.9914	26
64	2.0028	2.0143	2.0258	2.0373	2.0488	2.0603	25
65	2.0719	2.0835	2.0951	2.1067	2.1183	2.1299	24
66	2.1416	2.1533	2.1650	2.1767	2.1884	2.2001	23
67	2.2119	2.2238	2.2357	2.2476	2.2595	2.2714	22
68	2.2834	2.2954	2.3074	2.3194	2.3314	2.3435	21
69	2.3556	2.3677	2.3798	2.3919	2.4040	2.4161	20
70	2.4283	2.4405	2.4527	2.4649	2.4771	2.4893	19
71	2.5016	2.5139	2.5262	2.5385	2.5508	2.5631	18
72	2.5754	2.5878	2.6002	2.6126	2.6250	2.6374	17
73	2.6498	2.6623	2.6747	2.6871	2.6996	2.7120	16
74	2.7245	2.7370	2.7495	2.7620	2.7745	2.7870	15
75	2.7995	2.8121	2.8246	2.8371	2.8496	2.8621	14
76	2.8747	2.8873	2.8998	2.9123	2.9248	2.9373	13
77	2.9498	2.9624	2.9749	2.9874	2.9999	3.0124	12
78	3.0249	3.0375	3.0500	3.0625	3.0750	3.0875	11
79	3.1000	3.1126	3.1251	3.1376	3.1501	3.1626	10
80	3.1751	3.1877	3.2002	3.2127	3.2252	3.2377	9
81	3.2502	3.2628	3.2753	3.2878	3.3003	3.3128	8
82	3.3253	3.3379	3.3504	3.3629	3.3754	3.3879	7
83	3.4004	3.4130	3.4255	3.4380	3.4505	3.4630	6
84	3.4755	3.4881	3.5006	3.5131	3.5256	3.5381	5
85	3.5506	3.5632	3.5757	3.5882	3.6007	3.6132	4
86	3.6257	3.6383	3.6508	3.6633	3.6758	3.6883	3
87	3.7008	3.7134	3.7259	3.7384	3.7509	3.7634	2
88	3.7759	3.7885	3.8010	3.8135	3.8260	3.8385	1
89	3.8510	3.8636	3.8761	3.8886	3.9011	3.9136	0

NATURAL COLOGIES.

1

22

[illegible]

M	Sin	Log	Sec	Log	M	M	Sin	Log	Sec	Log	M
0	0.0000	0.0000	1.0000	0.0000	0	0	0.0000	0.0000	1.0000	0.0000	0
1	0.0174	0.0007	0.9993	0.0007	1	1	0.0174	0.0007	0.9993	0.0007	1
2	0.0349	0.0014	0.9986	0.0014	2	2	0.0349	0.0014	0.9986	0.0014	2
3	0.0523	0.0021	0.9979	0.0021	3	3	0.0523	0.0021	0.9979	0.0021	3
4	0.0697	0.0028	0.9972	0.0028	4	4	0.0697	0.0028	0.9972	0.0028	4
5	0.0871	0.0035	0.9965	0.0035	5	5	0.0871	0.0035	0.9965	0.0035	5
6	0.1045	0.0042	0.9958	0.0042	6	6	0.1045	0.0042	0.9958	0.0042	6
7	0.1218	0.0049	0.9951	0.0049	7	7	0.1218	0.0049	0.9951	0.0049	7
8	0.1392	0.0056	0.9944	0.0056	8	8	0.1392	0.0056	0.9944	0.0056	8
9	0.1565	0.0063	0.9937	0.0063	9	9	0.1565	0.0063	0.9937	0.0063	9
10	0.1738	0.0070	0.9930	0.0070	10	10	0.1738	0.0070	0.9930	0.0070	10
11	0.1911	0.0077	0.9923	0.0077	11	11	0.1911	0.0077	0.9923	0.0077	11
12	0.2084	0.0084	0.9916	0.0084	12	12	0.2084	0.0084	0.9916	0.0084	12
13	0.2257	0.0091	0.9909	0.0091	13	13	0.2257	0.0091	0.9909	0.0091	13
14	0.2430	0.0098	0.9902	0.0098	14	14	0.2430	0.0098	0.9902	0.0098	14
15	0.2603	0.0105	0.9895	0.0105	15	15	0.2603	0.0105	0.9895	0.0105	15
16	0.2776	0.0112	0.9888	0.0112	16	16	0.2776	0.0112	0.9888	0.0112	16
17	0.2949	0.0119	0.9881	0.0119	17	17	0.2949	0.0119	0.9881	0.0119	17
18	0.3122	0.0126	0.9874	0.0126	18	18	0.3122	0.0126	0.9874	0.0126	18
19	0.3295	0.0133	0.9867	0.0133	19	19	0.3295	0.0133	0.9867	0.0133	19
20	0.3468	0.0140	0.9860	0.0140	20	20	0.3468	0.0140	0.9860	0.0140	20
21	0.3641	0.0147	0.9853	0.0147	21	21	0.3641	0.0147	0.9853	0.0147	21
22	0.3814	0.0154	0.9846	0.0154	22	22	0.3814	0.0154	0.9846	0.0154	22
23	0.3987	0.0161	0.9839	0.0161	23	23	0.3987	0.0161	0.9839	0.0161	23
24	0.4160	0.0168	0.9832	0.0168	24	24	0.4160	0.0168	0.9832	0.0168	24
25	0.4333	0.0175	0.9825	0.0175	25	25	0.4333	0.0175	0.9825	0.0175	25
26	0.4506	0.0182	0.9818	0.0182	26	26	0.4506	0.0182	0.9818	0.0182	26
27	0.4679	0.0189	0.9811	0.0189	27	27	0.4679	0.0189	0.9811	0.0189	27
28	0.4852	0.0196	0.9804	0.0196	28	28	0.4852	0.0196	0.9804	0.0196	28
29	0.5025	0.0203	0.9797	0.0203	29	29	0.5025	0.0203	0.9797	0.0203	29
30	0.5198	0.0210	0.9790	0.0210	30	30	0.5198	0.0210	0.9790	0.0210	30
31	0.5371	0.0217	0.9783	0.0217	31	31	0.5371	0.0217	0.9783	0.0217	31
32	0.5544	0.0224	0.9776	0.0224	32	32	0.5544	0.0224	0.9776	0.0224	32
33	0.5717	0.0231	0.9769	0.0231	33	33	0.5717	0.0231	0.9769	0.0231	33
34	0.5890	0.0238	0.9762	0.0238	34	34	0.5890	0.0238	0.9762	0.0238	34
35	0.6063	0.0245	0.9755	0.0245	35	35	0.6063	0.0245	0.9755	0.0245	35
36	0.6236	0.0252	0.9748	0.0252	36	36	0.6236	0.0252	0.9748	0.0252	36
37	0.6409	0.0259	0.9741	0.0259	37	37	0.6409	0.0259	0.9741	0.0259	37
38	0.6582	0.0266	0.9734	0.0266	38	38	0.6582	0.0266	0.9734	0.0266	38
39	0.6755	0.0273	0.9727	0.0273	39	39	0.6755	0.0273	0.9727	0.0273	39
40	0.6928	0.0280	0.9720	0.0280	40	40	0.6928	0.0280	0.9720	0.0280	40
41	0.7101	0.0287	0.9713	0.0287	41	41	0.7101	0.0287	0.9713	0.0287	41
42	0.7274	0.0294	0.9706	0.0294	42	42	0.7274	0.0294	0.9706	0.0294	42
43	0.7447	0.0301	0.9699	0.0301	43	43	0.7447	0.0301	0.9699	0.0301	43
44	0.7620	0.0308	0.9692	0.0308	44	44	0.7620	0.0308	0.9692	0.0308	44
45	0.7793	0.0315	0.9685	0.0315	45	45	0.7793	0.0315	0.9685	0.0315	45
46	0.7966	0.0322	0.9678	0.0322	46	46	0.7966	0.0322	0.9678	0.0322	46
47	0.8139	0.0329	0.9671	0.0329	47	47	0.8139	0.0329	0.9671	0.0329	47
48	0.8312	0.0336	0.9664	0.0336	48	48	0.8312	0.0336	0.9664	0.0336	48
49	0.8485	0.0343	0.9657	0.0343	49	49	0.8485	0.0343	0.9657	0.0343	49
50	0.8658	0.0350	0.9650	0.0350	50	50	0.8658	0.0350	0.9650	0.0350	50
51	0.8831	0.0357	0.9643	0.0357	51	51	0.8831	0.0357	0.9643	0.0357	51
52	0.9004	0.0364	0.9636	0.0364	52	52	0.9004	0.0364	0.9636	0.0364	52
53	0.9177	0.0371	0.9629	0.0371	53	53	0.9177	0.0371	0.9629	0.0371	53
54	0.9350	0.0378	0.9622	0.0378	54	54	0.9350	0.0378	0.9622	0.0378	54
55	0.9523	0.0385	0.9615	0.0385	55	55	0.9523	0.0385	0.9615	0.0385	55
56	0.9696	0.0392	0.9608	0.0392	56	56	0.9696	0.0392	0.9608	0.0392	56
57	0.9869	0.0399	0.9601	0.0399	57	57	0.9869	0.0399	0.9601	0.0399	57
58	1.0042	0.0406	0.9594	0.0406	58	58	1.0042	0.0406	0.9594	0.0406	58
59	1.0215	0.0413	0.9587	0.0413	59	59	1.0215	0.0413	0.9587	0.0413	59
60	1.0388	0.0420	0.9580	0.0420	60	60	1.0388	0.0420	0.9580	0.0420	60

M	Sine	Diff	Table	Diff	M	M	Sine	Diff	Table	Diff	M
0	0.0000	0.0000	0.0000	0.0000	0	0	0.0000	0.0000	0.0000	0.0000	0
1	0.0174	0.0007	0.0174	0.0007	1	1	0.0174	0.0007	0.0174	0.0007	1
2	0.0349	0.0014	0.0349	0.0014	2	2	0.0349	0.0014	0.0349	0.0014	2
3	0.0523	0.0021	0.0523	0.0021	3	3	0.0523	0.0021	0.0523	0.0021	3
4	0.0697	0.0028	0.0697	0.0028	4	4	0.0697	0.0028	0.0697	0.0028	4
5	0.0871	0.0035	0.0871	0.0035	5	5	0.0871	0.0035	0.0871	0.0035	5
6	0.1045	0.0042	0.1045	0.0042	6	6	0.1045	0.0042	0.1045	0.0042	6
7	0.1218	0.0049	0.1218	0.0049	7	7	0.1218	0.0049	0.1218	0.0049	7
8	0.1392	0.0056	0.1392	0.0056	8	8	0.1392	0.0056	0.1392	0.0056	8
9	0.1565	0.0063	0.1565	0.0063	9	9	0.1565	0.0063	0.1565	0.0063	9
10	0.1738	0.0070	0.1738	0.0070	10	10	0.1738	0.0070	0.1738	0.0070	10
11	0.1911	0.0077	0.1911	0.0077	11	11	0.1911	0.0077	0.1911	0.0077	11
12	0.2084	0.0084	0.2084	0.0084	12	12	0.2084	0.0084	0.2084	0.0084	12
13	0.2257	0.0091	0.2257	0.0091	13	13	0.2257	0.0091	0.2257	0.0091	13
14	0.2430	0.0098	0.2430	0.0098	14	14	0.2430	0.0098	0.2430	0.0098	14
15	0.2603	0.0105	0.2603	0.0105	15	15	0.2603	0.0105	0.2603	0.0105	15
16	0.2776	0.0112	0.2776	0.0112	16	16	0.2776	0.0112	0.2776	0.0112	16
17	0.2949	0.0119	0.2949	0.0119	17	17	0.2949	0.0119	0.2949	0.0119	17
18	0.3122	0.0126	0.3122	0.0126	18	18	0.3122	0.0126	0.3122	0.0126	18
19	0.3295	0.0133	0.3295	0.0133	19	19	0.3295	0.0133	0.3295	0.0133	19
20	0.3468	0.0140	0.3468	0.0140	20	20	0.3468	0.0140	0.3468	0.0140	20
21	0.3641	0.0147	0.3641	0.0147	21	21	0.3641	0.0147	0.3641	0.0147	21
22	0.3814	0.0154	0.3814	0.0154	22	22	0.3814	0.0154	0.3814	0.0154	22
23	0.3987	0.0161	0.3987	0.0161	23	23	0.3987	0.0161	0.3987	0.0161	23
24	0.4160	0.0168	0.4160	0.0168	24	24	0.4160	0.0168	0.4160	0.0168	24
25	0.4333	0.0175	0.4333	0.0175	25	25	0.4333	0.0175	0.4333	0.0175	25
26	0.4506	0.0182	0.4506	0.0182	26	26	0.4506	0.0182	0.4506	0.0182	26
27	0.4679	0.0189	0.4679	0.0189	27	27	0.4679	0.0189	0.4679	0.0189	27
28	0.4852	0.0196	0.4852	0.0196	28	28	0.4852	0.0196	0.4852	0.0196	28
29	0.5025	0.0203	0.5025	0.0203	29	29	0.5025	0.0203	0.5025	0.0203	29
30	0.5198	0.0210	0.5198	0.0210	30	30	0.5198	0.0210	0.5198	0.0210	30
31	0.5371	0.0217	0.5371	0.0217	31	31	0.5371	0.0217	0.5371	0.0217	31
32	0.5544	0.0224	0.5544	0.0224	32	32	0.5544	0.0224	0.5544	0.0224	32
33	0.5717	0.0231	0.5717	0.0231	33	33	0.5717	0.0231	0.5717	0.0231	33
34	0.5890	0.0238	0.5890	0.0238	34	34	0.5890	0.0238	0.5890	0.0238	34
35	0.6063	0.0245	0.6063	0.0245	35	35	0.6063	0.0245	0.6063	0.0245	35
36	0.6236	0.0252	0.6236	0.0252	36	36	0.6236	0.0252	0.6236	0.0252	36
37	0.6409	0.0259	0.6409	0.0259	37	37	0.6409	0.0259	0.6409	0.0259	37
38	0.6582	0.0266	0.6582	0.0266	38	38	0.6582	0.0266	0.6582	0.0266	38
39	0.6755	0.0273	0.6755	0.0273	39	39	0.6755	0.0273	0.6755	0.0273	39
40	0.6928	0.0280	0.6928	0.0280	40	40	0.6928	0.0280	0.6928	0.0280	40
41	0.7101	0.0287	0.7101	0.0287	41	41	0.7101	0.0287	0.7101	0.0287	41
42	0.7274	0.0294	0.7274	0.0294	42	42	0.7274	0.0294	0.7274	0.0294	42
43	0.7447	0.0301	0.7447	0.0301	43	43	0.7447	0.0301	0.7447	0.0301	43
44	0.7620	0.0308	0.7620	0.0308	44	44	0.7620	0.0308	0.7620	0.0308	44
45	0.7793	0.0315	0.7793	0.0315	45	45	0.7793	0.0315	0.7793	0.0315	45
46	0.7966	0.0322	0.7966	0.0322	46	46	0.7966	0.0322	0.7966	0.0322	46
47	0.8139	0.0329	0.8139	0.0329	47	47	0.8139	0.0329	0.8139	0.0329	47
48	0.8312	0.0336	0.8312	0.0336	48	48	0.8312	0.0336	0.8312	0.0336	48
49	0.8485	0.0343	0.8485	0.0343	49	49	0.8485	0.0343	0.8485	0.0343	49
50	0.8658	0.0350	0.8658	0.0350	50	50	0.8658	0.0350	0.8658	0.0350	50
51	0.8831	0.0357	0.8831	0.0357	51	51	0.8831	0.0357	0.8831	0.0357	51
52	0.9004	0.0364	0.9004	0.0364	52	52	0.9004	0.0364	0.9004	0.0364	52
53	0.9177	0.0371	0.9177	0.0371	53	53	0.9177	0.0371	0.9177	0.0371	53
54	0.9350	0.0378	0.9350	0.0378	54	54	0.9350	0.0378	0.9350	0.0378	54
55	0.9523	0.0385	0.9523	0.0385	55	55	0.9523	0.0385	0.9523	0.0385	55
56	0.9696	0.0392	0.9696	0.0392	56	56	0.9696	0.0392	0.9696	0.0392	56
57	0.9869	0.0399	0.9869	0.0399	57	57	0.9869	0.0399	0.9869	0.0399	57
58	1.0042	0.0406	1.0042	0.0406	58	58	1.0042	0.0406	1.0042	0.0406	58
59	1.0215	0.0413	1.0215	0.0413	59	59	1.0215	0.0413	1.0215	0.0413	59
60	1.0388	0.0420	1.0388	0.0420	60	60	1.0388	0.0420	1.0388	0.0420	60
M Sine D. Table D. M											

M	Sine	Di	Tang	Di	M	M	Sine	Di	Tang	Di	M
0	9.1435	1.0	9.14780	1.33	60	0	9.1943	1.31	9.19071	1.36	60
1	1443	1.43	14872	1.32	59	1	19513	1.35	20053	1.36	59
2	1453	1.49	14963	1.32	58	2	19592	1.32	20134	1.36	58
3	14621	1.49	15054	1.32	57	3	19672	1.32	20216	1.35	57
4	14714	1.48	15145	1.31	56	4	19751	1.32	20297	1.35	56
5	14805	1.48	15236	1.31	55	5	19830	1.32	20378	1.35	55
6	14891	1.48	15327	1.31	54	6	19909	1.31	20459	1.35	54
7	14980	1.48	15417	1.31	53	7	19988	1.31	20540	1.35	53
8	15069	1.47	15508	1.30	52	8	20067	1.31	20622	1.35	52
9	15157	1.47	15598	1.30	51	9	20147	1.31	20701	1.34	51
10	15245	1.47	15688	1.30	50	10	20227	1.31	20782	1.34	50
11	15333	1.47	9.15777	1.30	49	11	20307	1.30	20862	1.34	49
12	15421	1.46	1587	1.49	48	12	20387	1.30	20942	1.33	48
13	15508	1.46	15960	1.49	47	13	20467	1.30	21022	1.33	47
14	15596	1.46	16046	1.49	46	14	20547	1.30	21102	1.33	46
15	15683	1.45	16132	1.48	45	15	20627	1.30	21182	1.33	45
16	15770	1.45	16224	1.48	44	16	20707	1.30	21262	1.32	44
17	15857	1.45	16312	1.48	43	17	20787	1.29	21342	1.32	43
18	15944	1.45	16403	1.47	42	18	20867	1.29	21422	1.32	42
19	16030	1.44	16489	1.47	41	19	20947	1.29	21502	1.32	41
20	16116	1.44	16577	1.47	40	20	21027	1.29	21582	1.32	40
21	9.16203	1.43	16668	1.46	39	21	21107	1.29	21662	1.31	39
22	16289	1.43	16754	1.46	38	22	21187	1.29	21742	1.31	38
23	16374	1.43	16841	1.46	37	23	21267	1.29	21822	1.31	37
24	16459	1.42	16928	1.46	36	24	21347	1.29	21902	1.31	36
25	16545	1.42	17016	1.45	35	25	21427	1.29	21982	1.30	35
26	16631	1.42	17103	1.45	34	26	21507	1.29	22062	1.30	34
27	16717	1.42	17190	1.45	33	27	21587	1.28	22142	1.30	33
28	16803	1.41	17277	1.44	32	28	21667	1.28	22222	1.30	32
29	16889	1.41	17363	1.44	31	29	21747	1.28	22302	1.30	31
30	16970	1.41	17450	1.44	30	30	21827	1.28	22382	1.30	30
31	17055	1.41	17536	1.44	29	31	21907	1.28	22462	1.29	29
32	17139	1.40	17622	1.44	28	32	21987	1.28	22542	1.29	28
33	17223	1.40	17708	1.44	27	33	22067	1.28	22622	1.29	27
34	17307	1.40	17794	1.44	26	34	22147	1.28	22702	1.29	26
35	17391	1.40	17880	1.44	25	35	22227	1.28	22782	1.29	25
36	17474	1.39	17966	1.44	24	36	22307	1.28	22862	1.29	24
37	17558	1.39	18051	1.44	23	37	22387	1.28	22942	1.29	23
38	17641	1.39	18137	1.44	22	38	22467	1.28	23022	1.29	22
39	17724	1.38	18223	1.44	21	39	22547	1.28	23102	1.29	21
40	17807	1.38	18309	1.44	20	40	22627	1.28	23182	1.29	20
41	9.17890	1.38	18395	1.44	19	41	22707	1.28	23262	1.29	19
42	17973	1.38	18481	1.44	18	42	22787	1.28	23342	1.29	18
43	18055	1.37	18566	1.44	17	43	22867	1.28	23422	1.29	17
44	18137	1.37	18654	1.44	16	44	22947	1.28	23502	1.29	16
45	18220	1.37	18740	1.44	15	45	23027	1.28	23582	1.29	15
46	18302	1.37	18826	1.44	14	46	23107	1.28	23662	1.29	14
47	18383	1.36	18912	1.44	13	47	23187	1.28	23742	1.29	13
48	18465	1.36	18997	1.44	12	48	23267	1.28	23822	1.29	12
49	18547	1.36	19083	1.44	11	49	23347	1.28	23902	1.29	11
50	18628	1.36	19169	1.44	10	50	23427	1.28	23982	1.29	10
51	9.18709	1.35	19255	1.44	9	51	23507	1.28	24062	1.29	9
52	18790	1.35	19341	1.44	8	52	23587	1.28	24142	1.29	8
53	18871	1.35	19427	1.44	7	53	23667	1.28	24222	1.29	7
54	18952	1.35	19513	1.44	6	54	23747	1.28	24302	1.29	6
55	19033	1.34	19599	1.44	5	55	23827	1.28	24382	1.29	5
56	19113	1.34	19685	1.44	4	56	23907	1.28	24462	1.29	4
57	19193	1.34	19771	1.44	3	57	23987	1.28	24542	1.29	3
58	19274	1.34	19857	1.44	2	58	24067	1.28	24622	1.29	2
59	19354	1.33	19943	1.44	1	59	24147	1.28	24702	1.29	1
60	19434	1.33	20029	1.44	0	60	24227	1.28	24782	1.29	0
M	Logarithm	Di	Cotang	Di	M	M	Logarithm	Di	Cotang	Di	M

M	Sine	Di	Tang	Di	M	M	Sine	Di	Tang	Di	M
0	9.24667	1.19	9.24672	1.23	60	0	9.28060	1.04	9.28060	1.12	60
1	2469	1.19	24706	1.23	59	1	28125	1.08	28125	1.12	59
2	24710	1.19	24719	1.23	58	2	28190	1.08	28190	1.12	58
3	2481	1.19	24811	1.23	57	3	28254	1.08	28254	1.12	57
4	24833	1.18	24832	1.22	56	4	28319	1.08	28319	1.12	56
5	24854	1.18	24850	1.22	55	5	28384	1.07	28384	1.12	55
6	24875	1.18	24873	1.22	54	6	28448	1.07	28448	1.12	54
7	24896	1.18	24894	1.22	53	7	28513	1.07	28513	1.11	53
8	24916	1.18	24915	1.22	52	8	28577	1.07	28577	1.11	52
9	24937	1.17	24936	1.21	51	9	28641	1.07	28641	1.11	51
10	24957	1.17	24956	1.21	50	10	28705	1.07	28705	1.11	50
11	9.24978	1.17	9.24978	1.21	49	11	9.28769	1.06	9.28769	1.11	49
12	24998	1.17	24997	1.21	48	12	28833	1.06	28833	1.11	48
13	24888	1.17	24882	1.21	47	13	28897	1.06	28897	1.11	47
14	24928	1.17	24922	1.20	46	14	28961	1.06	28961	1.11	46
15	25028	1.16	25022	1.20	45	15	29025	1.06	29025	1.11	45
16	25028	1.16	25022	1.20	44	16	29089	1.06	29089	1.11	44
17	25164	1.16	25158	1.20	43	17	29153	1.06	29153	1.11	43
18	252	1.16	25244	1.20	42	18	29217	1.05	29217	1.11	42
19	2527	1.16	25260	1.20	41	19	29277	1.05	29277	1.11	41
20	2537	1.16	25360	1.19	40	20	29340	1.05	29340	1.11	40
21	2544	1.16	25428	1.19	39	21	9.29409	1.05	9.29409	1.11	39
22	25541	1.16	25525	1.19	38	22	29473	1.05	29473	1.11	38
23	2568	1.16	25661	1.19	37	23	29537	1.05	29537	1.11	37
24	25682	1.16	25662	1.19	36	24	29601	1.04	29601	1.11	36
25	2577	1.16	25744	1.19	35	25	29665	1.04	29665	1.11	35
26	25774	1.16	25744	1.18	34	26	29729	1.04	29729	1.11	34
27	258	1.16	25808	1.18	33	27	29793	1.04	29793	1.11	33
28	258	1.16	25808	1.18	32	28	29857	1.04	29857	1.11	32
29	259	1.16	25906	1.18	31	29	29921	1.04	29921	1.11	31
30	259	1.16	25906	1.18	30	30	29985	1.04	29985	1.11	30
31	9.2591	1.16	9.2591	1.17	29	31	9.30049	1.04	9.30049	1.11	29
32	25999	1.16	25993	1.17	28	32	30113	1.04	30113	1.11	28
33	2609	1.16	26083	1.17	27	33	30177	1.04	30177	1.11	27
34	2619	1.16	26183	1.17	26	34	30241	1.04	30241	1.11	26
35	2629	1.16	26283	1.17	25	35	30305	1.04	30305	1.11	25
36	2639	1.16	26383	1.17	24	36	30369	1.04	30369	1.11	24
37	2649	1.16	26483	1.17	23	37	30433	1.04	30433	1.11	23
38	2659	1.16	26583	1.17	22	38	30497	1.04	30497	1.11	22
39	2669	1.16	26683	1.17	21	39	30561	1.04	30561	1.11	21
40	2679	1.16	26783	1.17	20	40	30625	1.04	30625	1.11	20
41	9.2679	1.16	9.2679	1.17	19	41	9.30689	1.04	9.30689	1.11	19
42	2689	1.16	26883	1.17	18	42	30753	1.04	30753	1.11	18
43	2699	1.16	26983	1.17	17	43	30817	1.04	30817	1.11	17
44	2709	1.16	27083	1.17	16	44	30881	1.04	30881	1.11	16
45	2719	1.16	27183	1.17	15	45	30945	1.04	30945	1.11	15
46	2729	1.16	27283	1.17	14	46	31009	1.04	31009	1.11	14
47	2739	1.16	27383	1.17	13	47	31073	1.04	31073	1.11	13
48	2749	1.16	27483	1.17	12	48	31137	1.04	31137	1.11	12
49	2759	1.16	27583	1.17	11	49	31201	1.04	31201	1.11	11
50	2769	1.16	27683	1.17	10	50	31265	1.04	31265	1.11	10
51	9.2769	1.16	9.2769	1.17	9	51	9.31329	1.04	9.31329	1.11	9
52	2779	1.16	27783	1.17	8	52	31393	1.04	31393	1.11	8
53	2789	1.16	27883	1.17	7	53	31457	1.04	31457	1.11	7
54	2799	1.16	27983	1.17	6	54	31521	1.04	31521	1.11	6
55	2809	1.16	28083	1.17	5	55	31585	1.04	31585	1.11	5
56	2819	1.16	28183	1.17	4	56	31649	1.04	31649	1.11	4
57	2829	1.16	28283	1.17	3	57	31713	1.04	31713	1.11	3
58	2839	1.16	28383	1.17	2	58	31777	1.04	31777	1.11	2
59	2849	1.16	28483	1.17	1	59	31841	1.04	31841	1.11	1
60	2859	1.16	28583	1.17	0	60	31905	1.04	31905	1.11	0

M	Sine	D.	Tan.	D.	M	M	Sine	D.	Tan.	D.	M
0	1.188	0.92	12.74	1.0	6	0	2.129	0.91	36.71	0.91	60
1	31847	.92	32810	1.0	59	1	3.1263	.91	36.34	.91	59
2	3190	.92	32872	1.0	58	2	3.1318	.91	36.42	.91	58
3	31960	.92	32933	1.03	57	3	3.1373	.91	36.50	.91	57
4	12.12	.92	32995	1.03	56	4	3.1427	.91	36.58	.91	56
5	32084	.92	33057	1.03	55	5	3.1481	.91	36.67	.91	55
6	32143	.92	33119	1.03	54	6	3.1536	.91	36.75	.91	54
7	32202	.92	33180	1.03	53	7	3.1590	.91	36.83	.91	53
8	32261	.92	33242	1.03	52	8	3.1644	.91	36.91	.91	52
9	32319	.92	33303	1.02	51	9	3.1698	.91	37.00	.91	51
10	32378	.92	33365	1.02	50	10	3.1752	.91	37.08	.91	50
11	32437	.92	33426	1.02	49	11	9.3.1806	.91	37.16	.91	49
12	32495	.92	33487	1.02	48	12	3.1860	.91	37.24	.91	48
13	32554	.92	33548	1.02	47	13	3.1914	.91	37.32	.91	47
14	32612	.92	33609	1.02	46	14	3.1968	.91	37.40	.91	46
15	32670	.92	33670	1.01	45	15	3.2022	.91	37.48	.91	45
16	32728	.92	33731	1.01	44	16	3.2076	.91	37.56	.91	44
17	32786	.92	33792	1.01	43	17	3.2130	.91	37.64	.91	43
18	32844	.92	33853	1.01	42	18	3.2184	.91	37.72	.91	42
19	32902	.92	33914	1.01	41	19	3.2238	.91	37.80	.91	41
20	32960	.92	33974	1.01	40	20	3.2292	.91	37.88	.91	40
21	9.1018	.92	34035	1.01	39	21	9.10.142	.91	37.96	.91	39
22	33077	.92	34095	1.01	38	22	3.2346	.91	38.04	.91	38
23	33135	.92	34156	1.01	37	23	3.2400	.91	38.12	.91	37
24	33193	.92	34217	1.00	36	24	3.2454	.91	38.20	.91	36
25	33251	.92	34278	1.00	35	25	3.2508	.91	38.28	.91	35
26	33309	.92	34339	1.00	34	26	3.2562	.91	38.36	.91	34
27	33367	.92	34400	1.00	33	27	3.2616	.91	38.44	.91	33
28	33425	.92	34461	1.00	32	28	3.2670	.91	38.52	.91	32
29	33483	.92	34522	1.00	31	29	3.2724	.91	38.60	.91	31
30	33541	.92	34583	1.00	30	30	3.2778	.91	38.68	.91	30
31	9.13.571	.92	34644	1.00	29	31	9.13.571	.91	38.76	.91	29
32	33600	.92	34705	.99	28	32	3.2832	.91	38.84	.91	28
33	33658	.92	34766	.99	27	33	3.2886	.91	38.92	.91	27
34	33716	.92	34827	.99	26	34	3.2940	.91	39.00	.91	26
35	33774	.92	34888	.99	25	35	3.2994	.91	39.08	.91	25
36	33832	.92	34949	.99	24	36	3.3048	.91	39.16	.91	24
37	33890	.92	35010	.99	23	37	3.3102	.91	39.24	.91	23
38	33948	.92	35071	.99	22	38	3.3156	.91	39.32	.91	22
39	34006	.92	35132	.99	21	39	3.3210	.91	39.40	.91	21
40	34064	.92	35193	.99	20	40	3.3264	.91	39.48	.91	20
41	9.14.106	.92	35254	.99	19	41	9.14.106	.91	39.56	.91	19
42	34122	.92	35315	.99	18	42	3.3318	.91	39.64	.91	18
43	34180	.92	35376	.99	17	43	3.3372	.91	39.72	.91	17
44	34238	.92	35437	.99	16	44	3.3426	.91	39.80	.91	16
45	34296	.92	35498	.99	15	45	3.3480	.91	39.88	.91	15
46	34354	.92	35559	.99	14	46	3.3534	.91	39.96	.91	14
47	34412	.92	35620	.99	13	47	3.3588	.91	40.04	.91	13
48	34470	.92	35681	.99	12	48	3.3642	.91	40.12	.91	12
49	34528	.92	35742	.99	11	49	3.3696	.91	40.20	.91	11
50	34586	.92	35803	.99	10	50	3.3750	.91	40.28	.91	10
51	9.14.713	.92	35864	.99	9	51	9.14.713	.91	40.36	.91	9
52	34644	.92	35925	.99	8	52	3.3804	.91	40.44	.91	8
53	34702	.92	35986	.99	7	53	3.3858	.91	40.52	.91	7
54	34760	.92	36047	.99	6	54	3.3912	.91	40.60	.91	6
55	34818	.92	36108	.99	5	55	3.3966	.91	40.68	.91	5
56	34876	.92	36169	.99	4	56	3.4020	.91	40.76	.91	4
57	34934	.92	36230	.99	3	57	3.4074	.91	40.84	.91	3
58	34992	.92	36291	.99	2	58	3.4128	.91	40.92	.91	2
59	35050	.92	36352	.99	1	59	3.4182	.91	41.00	.91	1
60	35108	.92	36413	.99	0	60	3.4236	.91	41.08	.91	0

M	Sine	D.	Tan.	D.	M	M	Sine	D.	Tan.	D.	M
0	35166	.92	36474	.99	10	0	4.188	0.92	9.400	0.92	50
1	35224	.92	36535	.99	9	1	4.194	.92	9.406	.92	49
2	35282	.92	36596	.99	8	2	4.200	.92	9.412	.92	48
3	35340	.92	36657	.99	7	3	4.206	.92	9.418	.92	47
4	35398	.92	36718	.99	6	4	4.212	.92	9.424	.92	46
5	35456	.92	36779	.99	5	5	4.218	.92	9.430	.92	45
6	35514	.92	36840	.99	4	6	4.224	.92	9.436	.92	44
7	35572	.92	36901	.99	3	7	4.230	.92	9.442	.92	43
8	35630	.92	36962	.99	2	8	4.236	.92	9.448	.92	42
9	35688	.92	37023	.99	1	9	4.242	.92	9.454	.92	41
10	35746	.92	37084	.99	0	10	4.248	.92	9.460	.92	40
11	35804	.92	37145	.99	59	11	4.254	.92	9.466	.92	39
12	35862	.92	37206	.99	58	12	4.260	.92	9.472	.92	38
13	35920	.92	37267	.99	57	13	4.266	.92	9.478	.92	37
14	35978	.92	37328	.99	56	14	4.272	.92	9.484	.92	36
15	36036	.92	37389	.99	55	15	4.278	.92	9.490	.92	35
16	36094	.92	37450	.99	54	16	4.284	.92	9.496	.92	34
17	36152	.92	37511	.99	53	17	4.290	.92	9.502	.92	33
18	36210	.92	37572	.99	52	18	4.296	.92	9.508	.92	32
19	36268	.92	37633	.99	51	19	4.302	.92	9.514	.92	31
20	36326	.92	37694	.99	50	20	4.308	.92	9.520	.92	30
21	36384	.92	37755	.99	49	21	4.314	.92	9.526	.92	29
22	36442	.92	37816	.99	48	22	4.320	.92	9.532	.92	28
23	36500	.92	37877	.99	47	23	4.326	.92	9.538	.92	27
24	36558	.92	37938	.99	46	24	4.332	.92	9.544	.92	26
25	36616	.92	38000	.99	45	25	4.338	.92	9.550	.92	25
26	36674	.92	38061	.99	44	26	4.344	.92	9.556	.92	24
27	36732	.92	38122	.99	43	27	4.350	.92	9.562	.92	23
28	36790	.92	38183	.99	42	28	4.356	.92	9.568	.92	22
29	36848	.92	38244	.99	41	29	4.362	.92	9.574	.92	21
30	36906	.92	38305	.99	40	30	4.368	.92	9.580	.92	20
31	36964	.92	38366	.99	39	31	4.374	.92	9.586	.92	19
32	37022	.92	38427	.99	38	32	4.380	.92	9.592	.92	18
33	37080	.92	38488	.99	37	33	4.386	.92	9.598	.92	17
34	37138	.92	38549	.99	36	34	4.392	.92	9.604	.92	16
35	37196	.92	38610	.99	35	35	4.398	.92	9.610	.92	15
36	37254	.92	38671	.99	34	36	4.404	.92	9.616	.92	14
37	37312	.92	38732	.99	33	37	4.410	.92	9.622	.92	13
38	37370	.92	38793	.99	32	38	4.416	.92	9.628	.92	12
39	37428	.92	38854	.99	31	39	4.422	.92	9.634	.92	11
40	37486	.92	38915	.99	30	40	4.428	.92	9.640	.92	10
41	37544	.92	38976	.99	29	41	4.434	.92	9.646	.92	9
42	37602	.92	39037	.99	28	42	4.440	.92	9.652	.92	8
43	37660	.92	39098	.99	27	43	4.446	.92	9.658	.92	7
44	37718	.92	39159	.99	26	44	4.452	.92	9.664	.92	6
45	37776	.92	39220	.99	25	45	4.458	.92	9.670	.92	5
46	37834	.92	39281	.99	24	46	4.464	.92	9.676	.92	4
47	37892	.92	39342	.99	23	47	4.470	.92	9.682	.92	3
48	37950	.92	39403	.99	22	48	4.476	.92	9.688	.92	2
49	38008	.92	39464	.99	21	49	4.482	.92	9.694	.92	1
50	38066	.92	39525	.99	20	50	4.488	.92	9.700	.92	0

M	Sine	Diff	Tang	Diff	M	M	Sine	Diff	Tang	Diff	M
0	2410 4	0.73	34 57 00	0.79	60	0	46 10 94	0.63	48 55 51	0.75	60
1	14 58	.73	43 57	.79	59	1	46 33	.69	48 57	.75	59
2	44 12	.73	43 57	.79	58	2	46 56	.69	48 58 24	.75	58
3	44 18	.73	43 57	.79	57	3	46 71	.69	48 58 59	.75	57
4	44 210	.73	43 57	.79	56	4	46 75	.69	48 59 14	.75	56
5	44 233	.73	43 57	.79	55	5	46 80	.68	48 59 59	.75	55
6	44 257	.73	43 57	.79	54	6	46 84	.68	48 60 4	.75	54
7	44 281	.73	43 57	.79	53	7	46 88	.68	48 60 49	.75	53
8	44 303	.73	43 57	.79	52	8	46 92	.68	48 60 91	.75	52
9	44 328	.73	43 57	.79	51	9	46 96	.68	48 60 96	.75	51
10	44 352	.73	43 57	.79	50	10	47 00	.68	48 60 94	.75	50
11	9 44 376	.73	9 46 271	.79	49	11	9 47 04	.68	9 48 629	.75	49
12	44 399	.72	46 319	.79	48	12	47 08	.68	49 07	.75	48
13	44 422	.72	46 366	.79	47	13	47 12	.68	49 1	.75	47
14	44 446	.72	46 413	.79	46	14	47 16	.68	49 1	.75	46
15	44 468	.72	46 46	.79	45	15	47 20	.68	49 1	.75	45
16	44 491	.72	46 507	.79	44	16	47 24	.68	49 1	.75	44
17	44 513	.72	46 554	.79	43	17	47 28	.68	49 1	.75	43
18	44 535	.72	46 601	.79	42	18	47 32	.68	49 1	.75	42
19	44 557	.72	46 648	.79	41	19	47 36	.67	49 1	.75	41
20	44 579	.72	46 694	.79	40	20	47 40	.67	49 1	.75	40
21	9 44 601	.72	9 46 741	.79	39	21	9 47 44	.67	9 49 1	.75	39
22	44 622	.72	46 788	.79	38	22	47 48	.67	49 1	.75	38
23	44 644	.72	46 835	.79	37	23	47 52	.67	49 1	.75	37
24	44 666	.71	46 881	.79	36	24	47 56	.67	49 1	.75	36
25	44 687	.71	46 928	.79	35	25	47 60	.67	49 1	.75	35
26	44 709	.71	46 975	.79	34	26	47 64	.67	49 1	.75	34
27	44 730	.71	47 021	.79	33	27	47 68	.67	49 1	.75	33
28	44 751	.71	47 068	.79	32	28	47 72	.67	49 1	.75	32
29	44 772	.71	47 114	.79	31	29	47 76	.67	49 1	.75	31
30	44 793	.71	47 160	.79	30	30	47 80	.67	49 1	.75	30
31	9 44 814	.71	9 47 207	.79	29	31	9 47 84	.67	9 49 1	.75	29
32	44 835	.71	47 253	.79	28	32	47 88	.67	49 1	.75	28
33	44 856	.71	47 299	.79	27	33	47 92	.67	49 1	.75	27
34	44 877	.71	47 346	.79	26	34	47 96	.67	49 1	.75	26
35	44 898	.71	47 392	.79	25	35	48 00	.67	49 1	.75	25
36	44 919	.71	47 438	.79	24	36	48 04	.67	49 1	.75	24
37	44 940	.71	47 484	.79	23	37	48 08	.67	49 1	.75	23
38	44 961	.71	47 530	.79	22	38	48 12	.67	49 1	.75	22
39	44 982	.71	47 576	.79	21	39	48 16	.67	49 1	.75	21
40	45 003	.71	47 622	.79	20	40	48 20	.67	49 1	.75	20
41	9 45 024	.71	9 47 668	.79	19	41	9 48 24	.67	9 49 1	.75	19
42	45 045	.71	47 714	.79	18	42	48 28	.67	49 1	.75	18
43	45 066	.71	47 760	.79	17	43	48 32	.67	49 1	.75	17
44	45 087	.71	47 806	.79	16	44	48 36	.67	49 1	.75	16
45	45 108	.71	47 852	.79	15	45	48 40	.67	49 1	.75	15
46	45 129	.71	47 898	.79	14	46	48 44	.67	49 1	.75	14
47	45 150	.71	47 944	.79	13	47	48 48	.67	49 1	.75	13
48	45 171	.71	47 990	.79	12	48	48 52	.67	49 1	.75	12
49	45 192	.71	48 036	.79	11	49	48 56	.67	49 1	.75	11
50	45 213	.71	48 082	.79	10	50	48 60	.67	49 1	.75	10
51	9 45 234	.71	9 48 128	.79	9	51	9 48 64	.67	9 49 1	.75	9
52	45 255	.71	48 174	.79	8	52	48 68	.67	49 1	.75	8
53	45 276	.71	48 220	.79	7	53	48 72	.67	49 1	.75	7
54	45 297	.71	48 266	.79	6	54	48 76	.67	49 1	.75	6
55	45 318	.71	48 312	.79	5	55	48 80	.67	49 1	.75	5
56	45 339	.71	48 358	.79	4	56	48 84	.67	49 1	.75	4
57	45 360	.71	48 404	.79	3	57	48 88	.67	49 1	.75	3
58	45 381	.71	48 450	.79	2	58	48 92	.67	49 1	.75	2
59	45 402	.71	48 496	.79	1	59	48 96	.67	49 1	.75	1
60	45 423	.71	48 542	.79	0	60	49 00	.67	49 1	.75	0

M	Sine	Diff	Tang	Diff	M	M	Sine	Diff	Tang	Diff	M
0	245 208		11 17 8		60	0	245 208		11 17 8		60
1	4 40 2	.7	11 20 1	0.7	59	1	245 208	.7	11 20 1	0.7	59
2	49 07	.7	11 22 4	0.7	58	2	245 208	.7	11 22 4	0.7	58
3	49 13	.7	11 24 6	0.7	57	3	245 208	.7	11 24 6	0.7	57
4	49 19	.7	11 26 9	0.7	56	4	245 208	.7	11 26 9	0.7	56
5	49 25	.7	11 29 2	0.7	55	5	245 208	.7	11 29 2	0.7	55
6	49 31	.7	11 31 5	0.7	54	6	245 208	.7	11 31 5	0.7	54
7	49 37	.7	11 33 8	0.7	53	7	245 208	.7	11 33 8	0.7	53
8	49 43	.7	11 36 1	0.7	52	8	245 208	.7	11 36 1	0.7	52
9	49 49	.7	11 38 4	0.7	51	9	245 208	.7	11 38 4	0.7	51
10	49 55	.7	11 40 7	0.7	50	10	245 208	.7	11 40 7	0.7	50
11	49 61	.7	11 43 0	0.7	49	11	245 208	.7	11 43 0	0.7	49
12	49 67	.7	11 45 3	0.7	48	12	245 208	.7	11 45 3	0.7	48
13	49 73	.7	11 47 6	0.7	47	13	245 208	.7	11 47 6	0.7	47
14	49 79	.7	11 49 9	0.7	46	14	245 208	.7	11 49 9	0.7	46
15	49 85	.7	11 52 2	0.7	45	15	245 208	.7	11 52 2	0.7	45
16	49 91	.7	11 54 5	0.7	44	16	245 208	.7	11 54 5	0.7	44
17	49 97	.7	11 56 8	0.7	43	17	245 208	.7	11 56 8	0.7	43
18	49 103	.7	11 59 1	0.7	42	18	245 208	.7	11 59 1	0.7	42
19	49 109	.7	12 01 4	0.7	41	19	245 208	.7	12 01 4	0.7	41
20	49 115	.7	12 03 7	0.7	40	20	245 208	.7	12 03 7	0.7	40
21	49 121	.7	12 06 0	0.7	39	21	245 208	.7	12 06 0	0.7	39
22	49 127	.7	12 08 3	0.7	38	22	245 208	.7	12 08 3	0.7	38
23	49 133	.7	12 10 6	0.7	37	23	245 208	.7	12 10 6	0.7	37
24	49 139	.7	12 12 9	0.7	36	24	245 208	.7	12 12 9	0.7	36
25	49 145	.7	12 15 2	0.7	35	25	245 208	.7	12 15 2	0.7	35
26	49 151	.7	12 17 5	0.7	34	26	245 208	.7	12 17 5	0.7	34
27	49 157	.7	12 19 8	0.7	33	27	245 208	.7	12 19 8	0.7	33
28	49 163	.7	12 22 1	0.7	32	28	245 208	.7	12 22 1	0.7	32
29	49 169	.7	12 24 4	0.7	31	29	245 208	.7	12 24 4	0.7	31
30	49 175	.7	12 26 7	0.7	30	30	245 208	.7	12 26 7	0.7	30
31	9 49 181	.7	9 12 29	0.7	29	31	9 49 181	.7	9 12 29	0.7	29
32	49 187	.7	12 29 0	0.7	28	32	49 187	.7	12 29 0	0.7	28
33	49 193	.7	12 31 3	0.7	27	33	49 193	.7	12 31 3	0.7	27
34	49 199	.7	12 33 6	0.7	26	34	49 199	.7	12 33 6	0.7	26
35	49 205	.7	12 35 9	0.7	25	35	49 205	.7	12 35 9	0.7	25
36	49 211	.7	12 38 2	0.7	24	36	49 211	.7	12 38 2	0.7	24
37	49 217	.7	12 40 5	0.7	23	37	49 217	.7	12 40 5	0.7	23
38	49 223	.7	12 42 8	0.7	22	38	49 223	.7	12 42 8	0.7	22
39	49 229	.7	12 45 1	0.7	21	39	49 229	.7	12 45 1	0.7	21
40	49 235	.7	12 47 4	0.7	20	40	49 235	.7	12 47 4	0.7	20
41	9 49 241	.7	9 12 56	0.7	19	41	9 49 241	.7	9 12 56	0.7	19
42	49 247	.7	12 49 7	0.7	18	42	49 247	.7	12 49 7	0.7	18
43	49 253	.7	12 52 0	0.7	17	43	49 253	.7	12 52 0	0.7	17
44	49 259	.7	12 54 3	0.7	16	44	49 259	.7	12 54 3	0.7	16
45	49 265	.7	12 56 6	0.7	15	45	49 265	.7	12 56 6	0.7	15
46	49 271	.7	12 58 9	0.7	14	46	49 271	.7	12 58 9	0.7	14
47	49 277	.7	13 01 2	0.7	13	47	49 277	.7	13 01 2	0.7	13
48	49 283	.7	13 03 5	0.7	12	48	49 283	.7	13 03 5	0.7	12
49	49 289	.7	13 05 8	0.7	11	49	49 289	.7	13 05 8	0.7	11
50	49 295	.7	13 08 1	0.7	10	50	49 295	.7	13 08 1	0.7	10
51	9 49 301	.7	9 13 13	0.7	9	51	9 49 301	.7	9 13 13	0.7	9
52	49 307	.7	13 10 4	0.7	8	52	49 307	.7	13 10 4	0.7	8
53	49 313	.7	13 12 7	0.7	7	53	49 313	.7	13 12 7	0.7	7
54	49 319	.7	13 15 0	0.7	6	54	49 319	.7	13 15 0	0.7	6
55	49 325	.7	13 17 3	0.7	5	55	49 325	.7	13 17 3	0.7	5
56	49 331	.7	13 19 6	0.7	4	56	49 331	.7	13 19 6	0.7	4
57	49 337	.7	13 21 9	0.7	3	57	49 337	.7	13 21 9	0.7	3
58	49 343	.7	13 24 2	0.7	2	58	49 343	.7	13 24 2	0.7	2
59	49 349	.7	13 26 5	0.7	1	59	49 349	.7	13 26 5	0.7	1
60	49 355	.7	13 28 8	0.7	0	60	49 355	.7	13 28 8	0.7	0

M	Side	D	Lat	Long	M	M	Side	D	Lat	Long	M
0	9.5400	0.58	56107	0.60	60	0	9.54	0.58	56118	0.60	60
1	9.5410	0.58	56116	0.60	59	1	56408	0.58	56118	0.60	59
2	9.5420	0.58	56125	0.60	58	2	56419	0.58	56119	0.60	58
3	9.5430	0.58	56124	0.60	57	3	56432	0.58	56121	0.60	57
4	9.5440	0.58	56124	0.60	56	4	56444	0.58	56122	0.60	56
5	9.5450	0.58	56124	0.60	55	5	56457	0.58	56123	0.60	55
6	9.5460	0.58	56124	0.60	54	6	56470	0.58	56124	0.60	54
7	9.5470	0.58	56124	0.60	53	7	56483	0.58	56125	0.60	53
8	9.5480	0.58	56124	0.60	52	8	56496	0.58	56126	0.60	52
9	9.5490	0.58	56124	0.60	51	9	56509	0.58	56127	0.60	51
10	9.5500	0.58	56124	0.60	50	10	56522	0.58	56128	0.60	50
11	9.5510	0.58	56124	0.60	49	11	9.5510	0.58	56128	0.60	49
12	9.5520	0.58	56124	0.60	48	12	56535	0.58	56129	0.60	48
13	9.5530	0.58	56124	0.60	47	13	56548	0.58	56130	0.60	47
14	9.5540	0.58	56124	0.60	46	14	56561	0.58	56131	0.60	46
15	9.5550	0.58	56124	0.60	45	15	56574	0.58	56132	0.60	45
16	9.5560	0.58	56124	0.60	44	16	56587	0.58	56133	0.60	44
17	9.5570	0.58	56124	0.60	43	17	56600	0.58	56134	0.60	43
18	9.5580	0.58	56124	0.60	42	18	56613	0.58	56135	0.60	42
19	9.5590	0.58	56124	0.60	41	19	56626	0.58	56136	0.60	41
20	9.5600	0.58	56124	0.60	40	20	56639	0.58	56137	0.60	40
21	9.5610	0.58	56124	0.60	39	21	9.5610	0.58	56138	0.60	39
22	9.5620	0.58	56124	0.60	38	22	56652	0.58	56139	0.60	38
23	9.5630	0.58	56124	0.60	37	23	56665	0.58	56140	0.60	37
24	9.5640	0.58	56124	0.60	36	24	56678	0.58	56141	0.60	36
25	9.5650	0.58	56124	0.60	35	25	56691	0.58	56142	0.60	35
26	9.5660	0.58	56124	0.60	34	26	56704	0.58	56143	0.60	34
27	9.5670	0.58	56124	0.60	33	27	56717	0.58	56144	0.60	33
28	9.5680	0.58	56124	0.60	32	28	56730	0.58	56145	0.60	32
29	9.5690	0.58	56124	0.60	31	29	56743	0.58	56146	0.60	31
30	9.5700	0.58	56124	0.60	30	30	56756	0.58	56147	0.60	30
31	9.5710	0.58	56124	0.60	29	31	9.5710	0.58	56148	0.60	29
32	9.5720	0.58	56124	0.60	28	32	56770	0.58	56149	0.60	28
33	9.5730	0.58	56124	0.60	27	33	56783	0.58	56150	0.60	27
34	9.5740	0.58	56124	0.60	26	34	56796	0.58	56151	0.60	26
35	9.5750	0.58	56124	0.60	25	35	56809	0.58	56152	0.60	25
36	9.5760	0.58	56124	0.60	24	36	56822	0.58	56153	0.60	24
37	9.5770	0.58	56124	0.60	23	37	56835	0.58	56154	0.60	23
38	9.5780	0.58	56124	0.60	22	38	56848	0.58	56155	0.60	22
39	9.5790	0.58	56124	0.60	21	39	56861	0.58	56156	0.60	21
40	9.5800	0.58	56124	0.60	20	40	56874	0.58	56157	0.60	20
41	9.5810	0.58	56124	0.60	19	41	9.5810	0.58	56158	0.60	19
42	9.5820	0.58	56124	0.60	18	42	56890	0.58	56159	0.60	18
43	9.5830	0.58	56124	0.60	17	43	56903	0.58	56160	0.60	17
44	9.5840	0.58	56124	0.60	16	44	56916	0.58	56161	0.60	16
45	9.5850	0.58	56124	0.60	15	45	56929	0.58	56162	0.60	15
46	9.5860	0.58	56124	0.60	14	46	56942	0.58	56163	0.60	14
47	9.5870	0.58	56124	0.60	13	47	56955	0.58	56164	0.60	13
48	9.5880	0.58	56124	0.60	12	48	56968	0.58	56165	0.60	12
49	9.5890	0.58	56124	0.60	11	49	56981	0.58	56166	0.60	11
50	9.5900	0.58	56124	0.60	10	50	56994	0.58	56167	0.60	10
51	9.5910	0.58	56124	0.60	9	51	9.5910	0.58	56168	0.60	9
52	9.5920	0.58	56124	0.60	8	52	57011	0.58	56169	0.60	8
53	9.5930	0.58	56124	0.60	7	53	57024	0.58	56170	0.60	7
54	9.5940	0.58	56124	0.60	6	54	57037	0.58	56171	0.60	6
55	9.5950	0.58	56124	0.60	5	55	57050	0.58	56172	0.60	5
56	9.5960	0.58	56124	0.60	4	56	57063	0.58	56173	0.60	4
57	9.5970	0.58	56124	0.60	3	57	57076	0.58	56174	0.60	3
58	9.5980	0.58	56124	0.60	2	58	57089	0.58	56175	0.60	2
59	9.5990	0.58	56124	0.60	1	59	57102	0.58	56176	0.60	1
60	9.6000	0.58	56124	0.60	0	60	57115	0.58	56177	0.60	0
M	Side	D	Lat	Long	M	M	Side	D	Lat	Long	M

M	Sec	Dist	Time	Dist	M	M	Sec	Dist	Time	Dist	M
0	57.17	0.2	60.41	0.61	60	0	57.17	0.50	60.41	0.61	60
1	57.18	0.2	60.42	0.61	61	1	57.18	0.50	60.42	0.61	61
2	57.19	0.2	60.43	0.61	62	2	57.19	0.50	60.43	0.61	62
3	57.20	0.2	60.44	0.61	63	3	57.20	0.50	60.44	0.61	63
4	57.21	0.2	60.45	0.61	64	4	57.21	0.50	60.45	0.61	64
5	57.22	0.2	60.46	0.61	65	5	57.22	0.50	60.46	0.61	65
6	57.23	0.2	60.47	0.61	66	6	57.23	0.50	60.47	0.61	66
7	57.24	0.2	60.48	0.61	67	7	57.24	0.50	60.48	0.61	67
8	57.25	0.2	60.49	0.61	68	8	57.25	0.50	60.49	0.61	68
9	57.26	0.2	60.50	0.61	69	9	57.26	0.50	60.50	0.61	69
10	57.27	0.2	60.51	0.61	70	10	57.27	0.50	60.51	0.61	70
11	57.28	0.2	60.52	0.61	71	11	57.28	0.50	60.52	0.61	71
12	57.29	0.2	60.53	0.61	72	12	57.29	0.50	60.53	0.61	72
13	57.30	0.2	60.54	0.61	73	13	57.30	0.50	60.54	0.61	73
14	57.31	0.2	60.55	0.61	74	14	57.31	0.50	60.55	0.61	74
15	57.32	0.2	60.56	0.61	75	15	57.32	0.50	60.56	0.61	75
16	57.33	0.2	60.57	0.61	76	16	57.33	0.50	60.57	0.61	76
17	57.34	0.2	60.58	0.61	77	17	57.34	0.50	60.58	0.61	77
18	57.35	0.2	60.59	0.61	78	18	57.35	0.50	60.59	0.61	78
19	57.36	0.2	61.00	0.61	79	19	57.36	0.50	61.00	0.61	79
20	57.37	0.2	61.01	0.61	80	20	57.37	0.50	61.01	0.61	80
21	57.38	0.2	61.02	0.61	81	21	57.38	0.50	61.02	0.61	81
22	57.39	0.2	61.03	0.61	82	22	57.39	0.50	61.03	0.61	82
23	57.40	0.2	61.04	0.61	83	23	57.40	0.50	61.04	0.61	83
24	57.41	0.2	61.05	0.61	84	24	57.41	0.50	61.05	0.61	84
25	57.42	0.2	61.06	0.61	85	25	57.42	0.50	61.06	0.61	85
26	57.43	0.2	61.07	0.61	86	26	57.43	0.50	61.07	0.61	86
27	57.44	0.2	61.08	0.61	87	27	57.44	0.50	61.08	0.61	87
28	57.45	0.2	61.09	0.61	88	28	57.45	0.50	61.09	0.61	88
29	57.46	0.2	61.10	0.61	89	29	57.46	0.50	61.10	0.61	89
30	57.47	0.2	61.11	0.61	90	30	57.47	0.50	61.11	0.61	90
31	57.48	0.2	61.12	0.61	91	31	57.48	0.50	61.12	0.61	91
32	57.49	0.2	61.13	0.61	92	32	57.49	0.50	61.13	0.61	92
33	57.50	0.2	61.14	0.61	93	33	57.50	0.50	61.14	0.61	93
34	57.51	0.2	61.15	0.61	94	34	57.51	0.50	61.15	0.61	94
35	57.52	0.2	61.16	0.61	95	35	57.52	0.50	61.16	0.61	95
36	57.53	0.2	61.17	0.61	96	36	57.53	0.50	61.17	0.61	96
37	57.54	0.2	61.18	0.61	97	37	57.54	0.50	61.18	0.61	97
38	57.55	0.2	61.19	0.61	98	38	57.55	0.50	61.19	0.61	98
39	57.56	0.2	61.20	0.61	99	39	57.56	0.50	61.20	0.61	99
40	57.57	0.2	61.21	0.61	100	40	57.57	0.50	61.21	0.61	100
41	57.58	0.2	61.22	0.61	101	41	57.58	0.50	61.22	0.61	101
42	57.59	0.2	61.23	0.61	102	42	57.59	0.50	61.23	0.61	102
43	57.60	0.2	61.24	0.61	103	43	57.60	0.50	61.24	0.61	103
44	57.61	0.2	61.25	0.61	104	44	57.61	0.50	61.25	0.61	104
45	57.62	0.2	61.26	0.61	105	45	57.62	0.50	61.26	0.61	105
46	57.63	0.2	61.27	0.61	106	46	57.63	0.50	61.27	0.61	106
47	57.64	0.2	61.28	0.61	107	47	57.64	0.50	61.28	0.61	107
48	57.65	0.2	61.29	0.61	108	48	57.65	0.50	61.29	0.61	108
49	57.66	0.2	61.30	0.61	109	49	57.66	0.50	61.30	0.61	109
50	57.67	0.2	61.31	0.61	110	50	57.67	0.50	61.31	0.61	110
51	57.68	0.2	61.32	0.61	111	51	57.68	0.50	61.32	0.61	111
52	57.69	0.2	61.33	0.61	112	52	57.69	0.50	61.33	0.61	112
53	57.70	0.2	61.34	0.61	113	53	57.70	0.50	61.34	0.61	113
54	57.71	0.2	61.35	0.61	114	54	57.71	0.50	61.35	0.61	114
55	57.72	0.2	61.36	0.61	115	55	57.72	0.50	61.36	0.61	115
56	57.73	0.2	61.37	0.61	116	56	57.73	0.50	61.37	0.61	116
57	57.74	0.2	61.38	0.61	117	57	57.74	0.50	61.38	0.61	117
58	57.75	0.2	61.39	0.61	118	58	57.75	0.50	61.39	0.61	118
59	57.76	0.2	61.40	0.61	119	59	57.76	0.50	61.40	0.61	119
60	57.77	0.2	61.41	0.61	120	60	57.77	0.50	61.41	0.61	120
61	57.78	0.2	61.42	0.61	121	61	57.78	0.50	61.42	0.61	121
62	57.79	0.2	61.43	0.61	122	62	57.79	0.50	61.43	0.61	122
63	57.80	0.2	61.44	0.61	123	63	57.80	0.50	61.44	0.61	123
64	57.81	0.2	61.45	0.61	124	64	57.81	0.50	61.45	0.61	124
65	57.82	0.2	61.46	0.61	125	65	57.82	0.50	61.46	0.61	125
66	57.83	0.2	61.47	0.61	126	66	57.83	0.50	61.47	0.61	126
67	57.84	0.2	61.48	0.61	127	67	57.84	0.50	61.48	0.61	127
68	57.85	0.2	61.49	0.61	128	68	57.85	0.50	61.49	0.61	128
69	57.86	0.2	61.50	0.61	129	69	57.86	0.50	61.50	0.61	129
70	57.87	0.2	61.51	0.61	130	70	57.87	0.50	61.51	0.61	130
71	57.88	0.2	61.52	0.61	131	71	57.88	0.50	61.52	0.61	131
72	57.89	0.2	61.53	0.61	132	72	57.89	0.50	61.53	0.61	132
73	57.90	0.2	61.54	0.61	133	73	57.90	0.50	61.54	0.61	133
74	57.91	0.2	61.55	0.61	134	74	57.91	0.50	61.55	0.61	134
75	57.92	0.2	61.56	0.61	135	75	57.92	0.50	61.56	0.61	135
76	57.93	0.2	61.57	0.61	136	76	57.93	0.50	61.57	0.61	136
77	57.94	0.2	61.58	0.61	137	77	57.94	0.50	61.58	0.61	137
78	57.95	0.2	61.59	0.61	138	78	57.95	0.50	61.59	0.61	138
79	57.96	0.2	61.60	0.61	139	79	57.96	0.50	61.60	0.61	139
80	57.97	0.2	61.61	0.61	140	80	57.97	0.50	61.61	0.61	140
81	57.98	0.2	61.62	0.61	141	81	57.98	0.50	61.62	0.61	141
82	57.99	0.2	61.63	0.61	142	82	57.99	0.50	61.63	0.61	142
83	58.00	0.2	61.64	0.61	143	83	58.00	0.50	61.64	0.61	143
84	58.01	0.2	61.65	0.61	144	84	58.01	0.50	61.65	0.61	144
85	58.02	0.2	61.66	0.61	145	85	58.02	0.50	61.66	0.61	145
86	58.03	0.2	61.67	0.61	146	86	58.03	0.50	61.67	0.61	146
87	58.04	0.2	61.68	0.61	147	87	58.04	0.50	61.68	0.61	147
88	58.05	0.2	61.69	0.61	148	88	58.05	0.50	61.69	0.61	148
89	58.06	0.2	61.70	0.61	149	89	58.06	0.50	61.70	0.61	149
90	58.07	0.2	61.71	0.61	150	90	58.07	0.50	61.71	0.61	150
91	58.08	0.2	61.72	0.61	151	91	58.08	0.50	61.72	0.61	151
92	58.09	0.2	61.73	0.61	152	92	58.09	0.50	61.73	0.61	152
93	58.10	0.2	61.74	0.61	153	93	58.10	0.50	61.74	0.61	153
94	58.11	0.2	61.75	0.61	154	94	58.11	0.50	61.75	0.61	154
95	58.12	0.2	61.76	0.61	155	95	58.12	0.50	61.76	0.61	155
96	58.13	0.2	61.77	0.61	156	96	58.13	0.50	61.77	0.61	156
97	58.14	0.2	61.78	0.61	157	97	58.14	0.50	61.78	0.61	157
98	58.15	0.2	61.79	0.61	158	98	58.15	0.50	61.79	0.61	158
99	58.16	0.2	61.80	0.61	159	99	58.16	0.50	61.80	0.61	159
100	58.17	0.2	61.81	0.61	160	100	58.17	0.50	61.81	0.61	160

M.	Sine	Diff.	Tang.	Diff.	M.	M.	Sine	Diff.	Tang.	Diff.	M.
0	0.0000	0.0000	0.0000	0.0000	0	0	0.0000	0.0000	0.0000	0.0000	0
1	0.0175	0.0175	0.0175	0.0175	1	1	0.0350	0.0350	0.0350	0.0350	1
2	0.0350	0.0350	0.0350	0.0350	2	2	0.0525	0.0525	0.0525	0.0525	2
3	0.0525	0.0525	0.0525	0.0525	3	3	0.0700	0.0700	0.0700	0.0700	3
4	0.0675	0.0675	0.0675	0.0675	4	4	0.0850	0.0850	0.0850	0.0850	4
5	0.0850	0.0850	0.0850	0.0850	5	5	0.1025	0.1025	0.1025	0.1025	5
6	0.1025	0.1025	0.1025	0.1025	6	6	0.1200	0.1200	0.1200	0.1200	6
7	0.1175	0.1175	0.1175	0.1175	7	7	0.1350	0.1350	0.1350	0.1350	7
8	0.1350	0.1350	0.1350	0.1350	8	8	0.1525	0.1525	0.1525	0.1525	8
9	0.1525	0.1525	0.1525	0.1525	9	9	0.1700	0.1700	0.1700	0.1700	9
10	0.1675	0.1675	0.1675	0.1675	10	10	0.1850	0.1850	0.1850	0.1850	10
11	0.1850	0.1850	0.1850	0.1850	11	11	0.2025	0.2025	0.2025	0.2025	11
12	0.2025	0.2025	0.2025	0.2025	12	12	0.2200	0.2200	0.2200	0.2200	12
13	0.2175	0.2175	0.2175	0.2175	13	13	0.2350	0.2350	0.2350	0.2350	13
14	0.2350	0.2350	0.2350	0.2350	14	14	0.2525	0.2525	0.2525	0.2525	14
15	0.2525	0.2525	0.2525	0.2525	15	15	0.2700	0.2700	0.2700	0.2700	15
16	0.2675	0.2675	0.2675	0.2675	16	16	0.2850	0.2850	0.2850	0.2850	16
17	0.2850	0.2850	0.2850	0.2850	17	17	0.3025	0.3025	0.3025	0.3025	17
18	0.3025	0.3025	0.3025	0.3025	18	18	0.3200	0.3200	0.3200	0.3200	18
19	0.3175	0.3175	0.3175	0.3175	19	19	0.3350	0.3350	0.3350	0.3350	19
20	0.3350	0.3350	0.3350	0.3350	20	20	0.3525	0.3525	0.3525	0.3525	20
21	0.3525	0.3525	0.3525	0.3525	21	21	0.3700	0.3700	0.3700	0.3700	21
22	0.3675	0.3675	0.3675	0.3675	22	22	0.3850	0.3850	0.3850	0.3850	22
23	0.3850	0.3850	0.3850	0.3850	23	23	0.4025	0.4025	0.4025	0.4025	23
24	0.4025	0.4025	0.4025	0.4025	24	24	0.4200	0.4200	0.4200	0.4200	24
25	0.4175	0.4175	0.4175	0.4175	25	25	0.4350	0.4350	0.4350	0.4350	25
26	0.4350	0.4350	0.4350	0.4350	26	26	0.4525	0.4525	0.4525	0.4525	26
27	0.4525	0.4525	0.4525	0.4525	27	27	0.4700	0.4700	0.4700	0.4700	27
28	0.4675	0.4675	0.4675	0.4675	28	28	0.4850	0.4850	0.4850	0.4850	28
29	0.4850	0.4850	0.4850	0.4850	29	29	0.5025	0.5025	0.5025	0.5025	29
30	0.5025	0.5025	0.5025	0.5025	30	30	0.5200	0.5200	0.5200	0.5200	30
31	0.5175	0.5175	0.5175	0.5175	31	31	0.5350	0.5350	0.5350	0.5350	31
32	0.5350	0.5350	0.5350	0.5350	32	32	0.5525	0.5525	0.5525	0.5525	32
33	0.5525	0.5525	0.5525	0.5525	33	33	0.5700	0.5700	0.5700	0.5700	33
34	0.5675	0.5675	0.5675	0.5675	34	34	0.5850	0.5850	0.5850	0.5850	34
35	0.5850	0.5850	0.5850	0.5850	35	35	0.6025	0.6025	0.6025	0.6025	35
36	0.6025	0.6025	0.6025	0.6025	36	36	0.6200	0.6200	0.6200	0.6200	36
37	0.6175	0.6175	0.6175	0.6175	37	37	0.6350	0.6350	0.6350	0.6350	37
38	0.6350	0.6350	0.6350	0.6350	38	38	0.6525	0.6525	0.6525	0.6525	38
39	0.6525	0.6525	0.6525	0.6525	39	39	0.6700	0.6700	0.6700	0.6700	39
40	0.6675	0.6675	0.6675	0.6675	40	40	0.6850	0.6850	0.6850	0.6850	40
41	0.6850	0.6850	0.6850	0.6850	41	41	0.7025	0.7025	0.7025	0.7025	41
42	0.7025	0.7025	0.7025	0.7025	42	42	0.7200	0.7200	0.7200	0.7200	42
43	0.7175	0.7175	0.7175	0.7175	43	43	0.7350	0.7350	0.7350	0.7350	43
44	0.7350	0.7350	0.7350	0.7350	44	44	0.7525	0.7525	0.7525	0.7525	44
45	0.7525	0.7525	0.7525	0.7525	45	45	0.7700	0.7700	0.7700	0.7700	45
46	0.7675	0.7675	0.7675	0.7675	46	46	0.7850	0.7850	0.7850	0.7850	46
47	0.7850	0.7850	0.7850	0.7850	47	47	0.8025	0.8025	0.8025	0.8025	47
48	0.8025	0.8025	0.8025	0.8025	48	48	0.8200	0.8200	0.8200	0.8200	48
49	0.8175	0.8175	0.8175	0.8175	49	49	0.8350	0.8350	0.8350	0.8350	49
50	0.8350	0.8350	0.8350	0.8350	50	50	0.8525	0.8525	0.8525	0.8525	50
51	0.8525	0.8525	0.8525	0.8525	51	51	0.8700	0.8700	0.8700	0.8700	51
52	0.8675	0.8675	0.8675	0.8675	52	52	0.8850	0.8850	0.8850	0.8850	52
53	0.8850	0.8850	0.8850	0.8850	53	53	0.9025	0.9025	0.9025	0.9025	53
54	0.9025	0.9025	0.9025	0.9025	54	54	0.9200	0.9200	0.9200	0.9200	54
55	0.9175	0.9175	0.9175	0.9175	55	55	0.9350	0.9350	0.9350	0.9350	55
56	0.9350	0.9350	0.9350	0.9350	56	56	0.9525	0.9525	0.9525	0.9525	56
57	0.9525	0.9525	0.9525	0.9525	57	57	0.9700	0.9700	0.9700	0.9700	57
58	0.9675	0.9675	0.9675	0.9675	58	58	0.9850	0.9850	0.9850	0.9850	58
59	0.9850	0.9850	0.9850	0.9850	59	59	0.9925	0.9925	0.9925	0.9925	59
60	0.9925	0.9925	0.9925	0.9925	60	60	1.0000	1.0000	1.0000	1.0000	60

M.	Sine	Diff.	Tang.	Diff.	M.	M.	Sine	Diff.	Tang.	Diff.	M.
0	9.64184		2.68818		60	0	9.67005		2.71017		60
1	64210	0.4	68836	0.2	61	1	67029	0.4	71047	0.2	61
2	64236	0.4	68862	0.2	62	2	67054	0.4	71072	0.2	62
3	64262	0.4	68888	0.2	63	3	67079	0.4	71097	0.2	63
4	64288	0.4	68914	0.2	64	4	67104	0.4	71122	0.2	64
5	64313	0.4	68940	0.2	65	5	67129	0.4	71147	0.2	65
6	64339	0.4	68966	0.2	66	6	67154	0.4	71172	0.2	66
7	64365	0.4	68992	0.2	67	7	67179	0.4	71197	0.2	67
8	64391	0.4	69018	0.2	68	8	67204	0.4	71222	0.2	68
9	64417	0.4	69044	0.2	69	9	67229	0.4	71247	0.2	69
10	64442	0.4	69070	0.2	70	10	67254	0.4	71272	0.2	70
11	9.64468		2.69100		71	11	9.67279		2.71302		71
12	64494	0.4	69126	0.2	72	12	67304	0.4	71327	0.2	72
13	64519	0.4	69152	0.2	73	13	67329	0.4	71352	0.2	73
14	64545	0.4	69178	0.2	74	14	67354	0.4	71377	0.2	74
15	64571	0.4	69204	0.2	75	15	67379	0.4	71402	0.2	75
16	64596	0.4	69230	0.2	76	16	67404	0.4	71427	0.2	76
17	64622	0.4	69256	0.2	77	17	67429	0.4	71452	0.2	77
18	64648	0.4	69282	0.2	78	18	67454	0.4	71477	0.2	78
19	64673	0.4	69308	0.2	79	19	67479	0.4	71502	0.2	79
20	64699	0.4	69334	0.2	80	20	67504	0.4	71527	0.2	80
21	64725	0.4	69360	0.2	81	21	9.67529		9.71552		81
22	64750	0.4	69386	0.2	82	22	67554	0.4	71577	0.2	82
23	64776	0.4	69412	0.2	83	23	67579	0.4	71602	0.2	83
24	64802	0.4	69438	0.2	84	24	67604	0.4	71627	0.2	84
25	64827	0.4	69464	0.2	85	25	67629	0.4	71652	0.2	85
26	64853	0.4	69490	0.2	86	26	67654	0.4	71677	0.2	86
27	64879	0.4	69516	0.2	87	27	67679	0.4	71702	0.2	87
28	64904	0.4	69542	0.2	88	28	67704	0.4	71727	0.2	88
29	64930	0.4	69568	0.2	89	29	67729	0.4	71752	0.2	89
30	64956	0.4	69594	0.2	90	30	67754	0.4	71777	0.2	90
31	9.64978		9.69603		91	31	9.67779		9.71802		91
32	64997	0.4	69620	0.2	92	32	67804	0.4	71827	0.2	92
33	65023	0.4	69646	0.2	93	33	67829	0.4	71852	0.2	93
34	65049	0.4	69672	0.2	94	34	67854	0.4	71877	0.2	94
35	65075	0.4	69698	0.2	95	35	67879	0.4	71902	0.2	95
36	65101	0.4	69724	0.2	96	36	67904	0.4	71927	0.2	96
37	65127	0.4	69750	0.2	97	37	67929	0.4	71952	0.2	97
38	65153	0.4	69776	0.2	98	38	67954	0.4	71977	0.2	98
39	65179	0.4	69802	0.2	99	39	67979	0.4	72002	0.2	99
40	65205	0.4	69828	0.2	100	40	68004	0.4	72027	0.2	100
41	65231	0.4	69854	0.2	101	41	68029	0.4	72052	0.2	101
42	65257	0.4	69880	0.2	102	42	68054	0.4	72077	0.2	102
43	65283	0.4	69906	0.2	103	43	68079	0.4	72102	0.2	103
44	65309	0.4	69932	0.2	104	44	68104	0.4	72127	0.2	104
45	65335	0.4	69958	0.2	105	45	68129	0.4	72152	0.2	105
46	65361	0.4	69984	0.2	106	46	68154	0.4	72177	0.2	106
47	65387	0.4	70010	0.2	107	47	68179	0.4	72202	0.2	107
48	65413	0.4	70036	0.2	108	48	68204	0.4	72227	0.2	108
49	65439	0.4	70062	0.2	109	49	68229	0.4	72252	0.2	109
50	65465	0.4	70088	0.2	110	50	68254	0.4	72277	0.2	110
51	9.65481		7.00113		111	51	9.68279		7.22302		111
52	65497	0.4	70114	0.2	112	52	68304	0.4	72302	0.2	112
53	65523	0.4	70140	0.2	113	53	68329	0.4	72327	0.2	113
54	65549	0.4	70166	0.2	114	54	68354	0.4	72352	0.2	114
55	65575	0.4	70192	0.2	115	55	68379	0.4	72377	0.2	115
56	65601	0.4	70218	0.2	116	56	68404	0.4	72402	0.2	116
57	65627	0.4	70244	0.2	117	57	68429	0.4	72427	0.2	117
58	65653	0.4	70270	0.2	118	58	68454	0.4	72452	0.2	118
59	65679	0.4	70296	0.2	119	59	68479	0.4	72477	0.2	119
60	65705	0.4	70322	0.2	120	60	68504	0.4	72502	0.2	120

M	Sine	Log	1°	M	M	Sine	Log	1°	M
0	9 67 1	0 10	9 72567	0 51	60	0 68 1	0 38	9 74375	0 50
1	67 18	40	72578	51	59	1 68 180	38	74405	50
2	67 20	40	72628	51	58	2 68 403	38	74435	50
3	67 22	40	72679	51	57	3 68 625	38	74465	50
4	67 24	40	72730	51	56	4 68 848	38	74494	50
5	67 26	40	72780	51	55	5 68 171	38	74524	50
6	67 28	40	72830	51	54	6 68 394	38	74554	50
7	67 30	40	72881	51	53	7 68 617	38	74584	50
8	67 32	40	72931	51	52	8 68 840	38	74614	50
9	67 34	40	72981	51	51	9 68 1063	38	74644	50
10	67 36	40	73031	51	50	10 68 326	38	74674	50
11	9 67 38	40	73081	51	49	11 68 549	38	74704	50
12	6 11	39	73131	51	48	12 68 772	38	74734	50
13	67 40	39	73181	51	47	13 68 995	38	74764	50
14	67 42	39	73231	51	46	14 69 218	38	74794	50
15	67 44	39	73281	51	45	15 69 441	38	74824	50
16	67 46	39	73331	51	44	16 69 664	38	74854	50
17	67 48	39	73381	51	43	17 69 887	38	74884	50
18	67 50	39	73431	51	42	18 70 110	38	74914	50
19	67 52	39	73481	51	41	19 70 333	38	74944	50
20	67 54	39	73531	51	40	20 70 556	38	74974	50
21	9 67 56	39	73581	51	39	21 70 779	38	75004	50
22	67 58	39	73631	51	38	22 70 1002	38	75034	50
23	67 60	39	73681	51	37	23 70 325	38	75064	50
24	67 62	39	73731	51	36	24 70 548	38	75094	50
25	67 64	39	73781	51	35	25 70 771	38	75124	50
26	67 66	39	73831	51	34	26 70 994	38	75154	50
27	67 68	39	73881	51	33	27 71 217	38	75184	50
28	67 70	39	73931	51	32	28 71 440	38	75214	50
29	67 72	39	73981	51	31	29 71 663	38	75244	50
30	67 74	39	74031	51	30	30 71 886	38	75274	50
31	9 67 76	39	74081	51	29	31 72 109	38	75304	50
32	67 78	39	74131	51	28	32 72 332	38	75334	50
33	6 78	39	74181	51	27	33 72 555	38	75364	50
34	67 80	39	74231	51	26	34 72 778	38	75394	50
35	67 82	39	74281	51	25	35 72 1001	38	75424	50
36	67 84	39	74331	51	24	36 72 324	38	75454	50
37	67 86	39	74381	51	23	37 72 547	38	75484	50
38	67 88	39	74431	51	22	38 72 770	38	75514	50
39	67 90	39	74481	51	21	39 72 993	38	75544	50
40	67 92	39	74531	51	20	40 73 216	38	75574	50
41	9 67 94	39	74581	51	19	41 73 439	38	75604	50
42	67 96	39	74631	51	18	42 73 662	38	75634	50
43	67 98	39	74681	51	17	43 73 885	38	75664	50
44	68 00	39	74731	51	16	44 74 108	38	75694	50
45	68 02	39	74781	51	15	45 74 331	38	75724	50
46	68 04	39	74831	51	14	46 74 554	38	75754	50
47	68 06	39	74881	51	13	47 74 777	38	75784	50
48	68 08	39	74931	51	12	48 74 1000	38	75814	50
49	68 10	39	74981	51	11	49 74 323	38	75844	50
50	68 12	39	75031	51	10	50 74 546	38	75874	50
51	9 68 14	39	75081	51	9	51 74 769	38	75904	50
52	68 16	39	75131	51	8	52 74 992	38	75934	50
53	68 18	39	75181	51	7	53 75 215	38	75964	50
54	68 20	39	75231	51	6	54 75 438	38	75994	50
55	68 22	39	75281	51	5	55 75 661	38	76024	50
56	68 24	39	75331	51	4	56 75 884	38	76054	50
57	68 26	39	75381	51	3	57 76 107	38	76084	50
58	68 28	39	75431	51	2	58 76 330	38	76114	50
59	68 30	39	75481	51	1	59 76 553	38	76144	50
60	68 32	39	75531	51	0	60 76 776	38	76174	50

M	Sine	Log	1°	M	M	Sine	Log	1°	M
0	2 68 34	0 36	76114	0 49	61	0 71 1	0 35	76114	0 48
1	68 36	36	76144	49	60	1 71 2	35	76144	48
2	68 38	36	76174	49	59	2 71 3	35	76174	48
3	68 40	36	76204	49	58	3 71 4	35	76204	48
4	68 42	36	76234	49	57	4 71 5	35	76234	48
5	68 44	36	76264	49	56	5 71 6	35	76264	48
6	68 46	36	76294	49	55	6 71 7	35	76294	48
7	68 48	36	76324	49	54	7 71 8	35	76324	48
8	68 50	36	76354	49	53	8 71 9	35	76354	48
9	68 52	36	76384	49	52	9 71 10	35	76384	48
10	68 54	36	76414	49	51	10 71 11	35	76414	48
11	68 56	36	76444	49	50	11 71 12	35	76444	48
12	68 58	36	76474	49	49	12 71 13	35	76474	48
13	68 60	36	76504	49	48	13 71 14	35	76504	48
14	68 62	36	76534	49	47	14 71 15	35	76534	48
15	68 64	36	76564	49	46	15 71 16	35	76564	48
16	68 66	36	76594	49	45	16 71 17	35	76594	48
17	68 68	36	76624	49	44	17 71 18	35	76624	48
18	68 70	36	76654	49	43	18 71 19	35	76654	48
19	68 72	36	76684	49	42	19 71 20	35	76684	48
20	68 74	36	76714	49	41	20 71 21	35	76714	48
21	9 68 76	36	76744	49	40	21 71 22	35	76744	48
22	68 78	36	76774	49	39	22 71 23	35	76774	48
23	68 80	36	76804	49	38	23 71 24	35	76804	48
24	68 82	36	76834	49	37	24 71 25	35	76834	48
25	68 84	36	76864	49	36	25 71 26	35	76864	48
26	68 86	36	76894	49	35	26 71 27	35	76894	48
27	68 88	36	76924	49	34	27 71 28	35	76924	48
28	68 90	36	76954	49	33	28 71 29	35	76954	48
29	68 92	36	76984	49	32	29 71 30	35	76984	48
30	68 94	36	77014	49	31	30 71 31	35	77014	48
31	9 68 96	36	77044	49	30	31 71 32	35	77044	48
32	68 98	36	77074	49	29	32 71 33	35	77074	48
33	69 00	36	77104	49	28	33 71 34	35	77104	48
34	69 02	36	77134	49	27	34 71 35	35	77134	48
35	69 04	36	77164	49	26	35 71 36	35	77164	48
36	69 06	36	77194	49	25	36 71 37	35	77194	48
37	69 08	36	77224	49	24	37 71 38	35	77224	48
38	69 10	36	77254	49	23	38 71 39	35	77254	48
39	69 12	36	77284	49	22	39 71 40	35	77284	48
40	69 14	36	77314	49	21	40 71 41	35	77314	48
41	9 69 16	36	77344	49	20	41 71 42	35	77344	48
42	69 18	36	77374	49	19	42 71 43	35	77374	48
43	69 20	36	77404	49	18	43 71 44	35	77404	48
44	69 22	36	77434	49	17	44 71 45	35	77434	48
45	69 24	36	77464	49	16	45 71 46	35	77464	48
46	69 26	36	77494	49	15	46 71 47	35	77494	48
47	69 28	36	77524	49	14	47 71 48	35	77524	48
48	69 30	36	77554	49	13	48 71 49	35	77554	48
49	69 32	36	77584	49	12	49 71 50	35	77584	48
50	69 34	36	77614	49	11	50 71 51	35	77614	48
51	9 69 36	36	77644	49	10	51 71 52	35	77644	48
52	69 38	36	77674	49	9	52 71 53	35	77674	48
53	69 40	36	77704	49	8	53 71 54	35	77704	48
54	69 42	36	77734	49	7	54 71 55	35	77734	48
55	69 44	36	77764	49	6	55 71 56	35	77764	48
56	69 46	36	77794	49	5	56 71 57	35	77794	48
57	69 48	36	77824	49	4	57 71 58	35	77824	48
58	69 50	36	77854	49	3	58 71 59	35	77854	48
59	69 52	36	77884	49	2	59 71 60	35	77884	48
60	69 54	36	77914	49	1	60 71 61	35	77914	48

M	Sine	Diff	Sec	Diff	M	M	Sine	Diff	Tang	Diff	M
0	7121	14	79607	47	10	0	73611	12	81272	46	60
1	7141	14	79607	47	19	1	73630	12	81279	46	59
2	7160	14	79607	47	58	2	73651	12	81287	46	58
3	7179	14	79607	47	57	3	73669	12	81295	46	57
4	7198	14	79607	47	56	4	73689	12	81302	46	56
5	7217	14	79607	47	55	5	73708	12	81309	46	55
6	7236	14	79607	47	54	6	73727	12	81318	46	54
7	7255	14	79607	47	53	7	73747	12	81325	46	53
8	7274	14	79607	47	52	8	73766	12	81333	46	52
9	7293	14	79607	47	51	9	73785	12	81340	46	51
10	7312	14	79607	47	50	10	73805	12	81348	46	50
11	7331	14	79607	47	49	11	73824	12	81355	46	49
12	7350	14	79607	47	48	12	73843	12	81363	46	48
13	7369	14	79607	47	47	13	73863	12	81371	46	47
14	7388	14	79607	47	46	14	73882	12	81378	46	46
15	7407	14	80000	47	45	15	73901	12	81386	46	45
16	7426	14	80028	47	44	16	73921	12	81394	46	44
17	7445	14	80056	47	43	17	73940	12	81402	46	43
18	7464	14	80084	47	42	18	73959	12	81410	46	42
19	7483	14	80112	47	41	19	73978	12	81418	46	41
20	7502	14	80140	47	40	20	73997	12	81426	46	40
21	7521	14	80168	47	39	21	74017	12	81434	46	39
22	7540	14	80195	47	38	22	74036	12	81442	46	38
23	7559	14	80223	47	37	23	74055	12	81450	46	37
24	7578	14	80251	47	36	24	74074	12	81458	46	36
25	7597	14	80279	47	35	25	74093	12	81466	46	35
26	7616	14	80307	47	34	26	74113	12	81474	46	34
27	7635	14	80335	47	33	27	74132	12	81482	46	33
28	7654	14	80363	47	32	28	74151	12	81490	46	32
29	7673	14	80391	47	31	29	74170	12	81498	46	31
30	7692	14	80419	47	30	30	74189	12	81506	46	30
31	7711	14	80447	47	29	31	74208	12	81514	46	29
32	7730	14	80475	47	28	32	74227	12	81522	46	28
33	7749	14	80503	47	27	33	74246	12	81530	46	27
34	7768	14	80531	47	26	34	74265	12	81538	46	26
35	7787	14	80559	47	25	35	74284	12	81546	46	25
36	7806	14	80587	47	24	36	74303	12	81554	46	24
37	7825	14	80615	47	23	37	74322	12	81562	46	23
38	7844	14	80643	47	22	38	74341	12	81570	46	22
39	7863	14	80671	47	21	39	74360	12	81578	46	21
40	7882	14	80699	47	20	40	74379	12	81586	46	20
41	7901	14	80727	47	19	41	74398	12	81594	46	19
42	7920	14	80755	47	18	42	74417	12	81602	46	18
43	7939	14	80783	47	17	43	74436	12	81610	46	17
44	7958	14	80811	47	16	44	74455	12	81618	46	16
45	7977	14	80839	47	15	45	74474	12	81626	46	15
46	7996	14	80867	47	14	46	74493	12	81634	46	14
47	8015	14	80895	47	13	47	74512	12	81642	46	13
48	8034	14	80923	47	12	48	74531	12	81650	46	12
49	8053	14	80951	47	11	49	74550	12	81658	46	11
50	8072	14	80979	47	10	50	74569	12	81666	46	10
51	8091	14	81007	47	9	51	74588	12	81674	46	9
52	8110	14	81035	47	8	52	74607	12	81682	46	8
53	8129	14	81063	47	7	53	74626	12	81690	46	7
54	8148	14	81091	47	6	54	74645	12	81698	46	6
55	8167	14	81119	47	5	55	74664	12	81706	46	5
56	8186	14	81147	47	4	56	74683	12	81714	46	4
57	8205	14	81175	47	3	57	74702	12	81722	46	3
58	8224	14	81203	47	2	58	74721	12	81730	46	2
59	8243	14	81231	47	1	59	74740	12	81738	46	1
60	8262	14	81259	47	0	60	74759	12	81746	46	0

M	Sine	Diff	Tang	Diff	M	Sine	Diff	Tang	Diff	M
0	9711.56	0.31	98222	0.4	60	84708	0.3	84708	0.4	60
1	9717.2	.31	98226	.4	59	84717	.3	84717	.4	59
2	9722.94	.31	98233	.4	58	84726	.3	84726	.4	58
3	9728.72	.31	98240	.4	57	84735	.3	84735	.4	57
4	9734.51	.31	98248	.4	56	84744	.3	84744	.4	56
5	9740.30	.31	98255	.4	55	84753	.3	84753	.4	55
6	9746.08	.31	98262	.4	54	84762	.3	84762	.4	54
7	9751.87	.31	98269	.4	53	84771	.3	84771	.4	53
8	9757.66	.31	98277	.4	52	84780	.3	84780	.4	52
9	9763.44	.31	98284	.4	51	84789	.3	84789	.4	51
10	9769.23	.31	98291	.4	50	84798	.3	84798	.4	50
11	9775.01	.31	98298	.4	49	84807	.3	84807	.4	49
12	9780.80	.31	98305	.4	48	84816	.3	84816	.4	48
13	9786.58	.31	98312	.4	47	84825	.3	84825	.4	47
14	9792.37	.31	98320	.4	46	84834	.3	84834	.4	46
15	9798.15	.31	98327	.4	45	84843	.3	84843	.4	45
16	9803.94	.31	98334	.4	44	84852	.3	84852	.4	44
17	9809.72	.31	98341	.4	43	84861	.3	84861	.4	43
18	9815.51	.31	98348	.4	42	84870	.3	84870	.4	42
19	9821.29	.31	98355	.4	41	84879	.3	84879	.4	41
20	9827.08	.31	98362	.4	40	84888	.3	84888	.4	40
21	9832.86	.31	98369	.4	39	84897	.3	84897	.4	39
22	9838.65	.31	98376	.4	38	84906	.3	84906	.4	38
23	9844.43	.31	98383	.4	37	84915	.3	84915	.4	37
24	9850.22	.31	98390	.4	36	84924	.3	84924	.4	36
25	9856.00	.31	98397	.4	35	84933	.3	84933	.4	35
26	9861.79	.31	98404	.4	34	84942	.3	84942	.4	34
27	9867.57	.31	98411	.4	33	84951	.3	84951	.4	33
28	9873.36	.31	98418	.4	32	84960	.3	84960	.4	32
29	9879.14	.31	98425	.4	31	84969	.3	84969	.4	31
30	9884.93	.31	98432	.4	30	84978	.3	84978	.4	30
31	9890.71	.31	98439	.4	29	84987	.3	84987	.4	29
32	9896.50	.31	98446	.4	28	84996	.3	84996	.4	28
33	9902.28	.31	98453	.4	27	85005	.3	85005	.4	27
34	9908.07	.31	98460	.4	26	85014	.3	85014	.4	26
35	9913.85	.31	98467	.4	25	85023	.3	85023	.4	25
36	9919.64	.31	98474	.4	24	85032	.3	85032	.4	24
37	9925.42	.31	98481	.4	23	85041	.3	85041	.4	23
38	9931.21	.31	98488	.4	22	85050	.3	85050	.4	22
39	9936.99	.31	98495	.4	21	85059	.3	85059	.4	21
40	9942.78	.31	98502	.4	20	85068	.3	85068	.4	20
41	9948.56	.31	98509	.4	19	85077	.3	85077	.4	19
42	9954.35	.31	98516	.4	18	85086	.3	85086	.4	18
43	9960.13	.31	98523	.4	17	85095	.3	85095	.4	17
44	9965.92	.31	98530	.4	16	85104	.3	85104	.4	16
45	9971.70	.31	98537	.4	15	85113	.3	85113	.4	15
46	9977.49	.31	98544	.4	14	85122	.3	85122	.4	14
47	9983.27	.31	98551	.4	13	85131	.3	85131	.4	13
48	9989.06	.31	98558	.4	12	85140	.3	85140	.4	12
49	9994.84	.31	98565	.4	11	85149	.3	85149	.4	11
50	10000.63	.31	98572	.4	10	85158	.3	85158	.4	10
51	10006.41	.31	98579	.4	9	85167	.3	85167	.4	9
52	10012.20	.31	98586	.4	8	85176	.3	85176	.4	8
53	10017.98	.31	98593	.4	7	85185	.3	85185	.4	7
54	10023.77	.31	98600	.4	6	85194	.3	85194	.4	6
55	10029.55	.31	98607	.4	5	85203	.3	85203	.4	5
56	10035.34	.31	98614	.4	4	85212	.3	85212	.4	4
57	10041.12	.31	98621	.4	3	85221	.3	85221	.4	3
58	10046.91	.31	98628	.4	2	85230	.3	85230	.4	2
59	10052.69	.31	98635	.4	1	85239	.3	85239	.4	1
60	10058.48	.31	98642	.4	0	85248	.3	85248	.4	0
M					M					M

M	Sine	D'	Log	D'	M	M	Sine	D'	Log	D'	M
0	77000	0.14	86100	0.14	60	0	77000	0.14	86100	0.14	60
1	77001	0.14	86101	0.14	59	1	77001	0.14	86101	0.14	59
2	77002	0.14	86102	0.14	58	2	77002	0.14	86102	0.14	58
3	77003	0.14	86103	0.14	57	3	77003	0.14	86103	0.14	57
4	77004	0.14	86104	0.14	56	4	77004	0.14	86104	0.14	56
5	77005	0.14	86105	0.14	55	5	77005	0.14	86105	0.14	55
6	77006	0.14	86106	0.14	54	6	77006	0.14	86106	0.14	54
7	77007	0.14	86107	0.14	53	7	77007	0.14	86107	0.14	53
8	77008	0.14	86108	0.14	52	8	77008	0.14	86108	0.14	52
9	77009	0.14	86109	0.14	51	9	77009	0.14	86109	0.14	51
10	77010	0.14	86110	0.14	50	10	77010	0.14	86110	0.14	50
11	77011	0.14	86111	0.14	49	11	77011	0.14	86111	0.14	49
12	77012	0.14	86112	0.14	48	12	77012	0.14	86112	0.14	48
13	77013	0.14	86113	0.14	47	13	77013	0.14	86113	0.14	47
14	77014	0.14	86114	0.14	46	14	77014	0.14	86114	0.14	46
15	77015	0.14	86115	0.14	45	15	77015	0.14	86115	0.14	45
16	77016	0.14	86116	0.14	44	16	77016	0.14	86116	0.14	44
17	77017	0.14	86117	0.14	43	17	77017	0.14	86117	0.14	43
18	77018	0.14	86118	0.14	42	18	77018	0.14	86118	0.14	42
19	77019	0.14	86119	0.14	41	19	77019	0.14	86119	0.14	41
20	77020	0.14	86120	0.14	40	20	77020	0.14	86120	0.14	40
21	77021	0.14	86121	0.14	39	21	77021	0.14	86121	0.14	39
22	77022	0.14	86122	0.14	38	22	77022	0.14	86122	0.14	38
23	77023	0.14	86123	0.14	37	23	77023	0.14	86123	0.14	37
24	77024	0.14	86124	0.14	36	24	77024	0.14	86124	0.14	36
25	77025	0.14	86125	0.14	35	25	77025	0.14	86125	0.14	35
26	77026	0.14	86126	0.14	34	26	77026	0.14	86126	0.14	34
27	77027	0.14	86127	0.14	33	27	77027	0.14	86127	0.14	33
28	77028	0.14	86128	0.14	32	28	77028	0.14	86128	0.14	32
29	77029	0.14	86129	0.14	31	29	77029	0.14	86129	0.14	31
30	77030	0.14	86130	0.14	30	30	77030	0.14	86130	0.14	30
31	77031	0.14	86131	0.14	29	31	77031	0.14	86131	0.14	29
32	77032	0.14	86132	0.14	28	32	77032	0.14	86132	0.14	28
33	77033	0.14	86133	0.14	27	33	77033	0.14	86133	0.14	27
34	77034	0.14	86134	0.14	26	34	77034	0.14	86134	0.14	26
35	77035	0.14	86135	0.14	25	35	77035	0.14	86135	0.14	25
36	77036	0.14	86136	0.14	24	36	77036	0.14	86136	0.14	24
37	77037	0.14	86137	0.14	23	37	77037	0.14	86137	0.14	23
38	77038	0.14	86138	0.14	22	38	77038	0.14	86138	0.14	22
39	77039	0.14	86139	0.14	21	39	77039	0.14	86139	0.14	21
40	77040	0.14	86140	0.14	20	40	77040	0.14	86140	0.14	20
41	77041	0.14	86141	0.14	19	41	77041	0.14	86141	0.14	19
42	77042	0.14	86142	0.14	18	42	77042	0.14	86142	0.14	18
43	77043	0.14	86143	0.14	17	43	77043	0.14	86143	0.14	17
44	77044	0.14	86144	0.14	16	44	77044	0.14	86144	0.14	16
45	77045	0.14	86145	0.14	15	45	77045	0.14	86145	0.14	15
46	77046	0.14	86146	0.14	14	46	77046	0.14	86146	0.14	14
47	77047	0.14	86147	0.14	13	47	77047	0.14	86147	0.14	13
48	77048	0.14	86148	0.14	12	48	77048	0.14	86148	0.14	12
49	77049	0.14	86149	0.14	11	49	77049	0.14	86149	0.14	11
50	77050	0.14	86150	0.14	10	50	77050	0.14	86150	0.14	10
51	77051	0.14	86151	0.14	9	51	77051	0.14	86151	0.14	9
52	77052	0.14	86152	0.14	8	52	77052	0.14	86152	0.14	8
53	77053	0.14	86153	0.14	7	53	77053	0.14	86153	0.14	7
54	77054	0.14	86154	0.14	6	54	77054	0.14	86154	0.14	6
55	77055	0.14	86155	0.14	5	55	77055	0.14	86155	0.14	5
56	77056	0.14	86156	0.14	4	56	77056	0.14	86156	0.14	4
57	77057	0.14	86157	0.14	3	57	77057	0.14	86157	0.14	3
58	77058	0.14	86158	0.14	2	58	77058	0.14	86158	0.14	2
59	77059	0.14	86159	0.14	1	59	77059	0.14	86159	0.14	1
60	77060	0.14	86160	0.14	0	60	77060	0.14	86160	0.14	0
M	Cosine	D'	Log	D'	M	M	Cosine	D'	Log	D'	M

M	Sine	D'	Tang	D'	M	M	Sine	D'	Tang	D'	M
0	974081	0 27	974081	0 45	60	0	974081	0 27	974081	0 45	60
1	974083	0 27	974083	0 45	59	1	974083	0 27	974083	0 45	59
2	974085	0 27	974085	0 45	58	2	974085	0 27	974085	0 45	58
3	974087	0 27	974087	0 45	57	3	974087	0 27	974087	0 45	57
4	974089	0 27	974089	0 45	56	4	974089	0 27	974089	0 45	56
5	974091	0 27	974091	0 45	55	5	974091	0 27	974091	0 45	55
6	974093	0 27	974093	0 45	54	6	974093	0 27	974093	0 45	54
7	974095	0 27	974095	0 45	53	7	974095	0 27	974095	0 45	53
8	974097	0 27	974097	0 45	52	8	974097	0 27	974097	0 45	52
9	974099	0 27	974099	0 45	51	9	974099	0 27	974099	0 45	51
10	974101	0 27	974101	0 45	50	10	974101	0 27	974101	0 45	50
11	974103	0 27	974103	0 45	49	11	974103	0 27	974103	0 45	49
12	974105	0 27	974105	0 45	48	12	974105	0 27	974105	0 45	48
13	974107	0 27	974107	0 45	47	13	974107	0 27	974107	0 45	47
14	974109	0 27	974109	0 45	46	14	974109	0 27	974109	0 45	46
15	974111	0 27	974111	0 45	45	15	974111	0 27	974111	0 45	45
16	974113	0 27	974113	0 45	44	16	974113	0 27	974113	0 45	44
17	974115	0 27	974115	0 45	43	17	974115	0 27	974115	0 45	43
18	974117	0 27	974117	0 45	42	18	974117	0 27	974117	0 45	42
19	974119	0 27	974119	0 45	41	19	974119	0 27	974119	0 45	41
20	974121	0 27	974121	0 45	40	20	974121	0 27	974121	0 45	40
21	974123	0 27	974123	0 45	39	21	974123	0 27	974123	0 45	39
22	974125	0 27	974125	0 45	38	22	974125	0 27	974125	0 45	38
23	974127	0 27	974127	0 45	37	23	974127	0 27	974127	0 45	37
24	974129	0 27	974129	0 45	36	24	974129	0 27	974129	0 45	36
25	974131	0 27	974131	0 45	35	25	974131	0 27	974131	0 45	35
26	974133	0 27	974133	0 45	34	26	974133	0 27	974133	0 45	34
27	974135	0 27	974135	0 45	33	27	974135	0 27	974135	0 45	33
28	974137	0 27	974137	0 45	32	28	974137	0 27	974137	0 45	32
29	974139	0 27	974139	0 45	31	29	974139	0 27	974139	0 45	31
30	974141	0 27	974141	0 45	30	30	974141	0 27	974141	0 45	30
31	974143	0 27	974143	0 45	29	31	974143	0 27	974143	0 45	29
32	974145	0 27	974145	0 45	28	32	974145	0 27	974145	0 45	28
33	974147	0 27	974147	0 45	27	33	974147	0 27	974147	0 45	27
34	974149	0 27	974149	0 45	26	34	974149	0 27	974149	0 45	26
35	974151	0 27	974151	0 45	25	35	974151	0 27	974151	0 45	25
36	974153	0 27	974153	0 45	24	36	974153	0 27	974153	0 45	24
37	974155	0 27	974155	0 45	23	37	974155	0 27	974155	0 45	23
38	974157	0 27	974157	0 45	22	38	974157	0 27	974157	0 45	22
39	974159	0 27	974159	0 45	21	39	974159	0 27	974159	0 45	21
40	974161	0 27	974161	0 45	20	40	974161	0 27	974161	0 45	20
41	974163	0 27	974163	0 45	19	41	974163	0 27	974163	0 45	19
42	974165	0 27	974165	0 45	18	42	974165	0 27	974165	0 45	18
43	974167	0 27	974167	0 45	17	43	974167	0 27	974167	0 45	17
44	974169	0 27	974169	0 45	16	44	974169	0 27	974169	0 45	16
45	974171	0 27	974171	0 45	15	45	974171	0 27	974171	0 45	15
46	974173	0 27	974173	0 45	14	46	974173	0 27	974173	0 45	14
47	974175	0 27	974175	0 45	13	47	974175	0 27	974175	0 45	13
48	974177	0 27	974177	0 45	12	48	974177	0 27	974177	0 45	12
49	974179	0 27	974179	0 45	11	49	974179	0 27	974179	0 45	11
50	974181	0 27	974181	0 45	10	50	974181	0 27	974181	0 45	10
51	974183	0 27	974183	0 45	9	51	974183	0 27	974183	0 45	9
52	974185	0 27	974185	0 45	8	52	974185	0 27	974185	0 45	8
53	974187	0 27	974187	0 45	7	53	974187	0 27	974187	0 45	7
54	974189	0 27	974189	0 45	6	54	974189	0 27	974189	0 45	6
55	974191	0 27	974191	0 45	5	55	974191	0 27	974191	0 45	5
56	974193	0 27	974193	0 45	4	56	974193	0 27	974193	0 45	4
57	974195	0 27	974195	0 45	3	57	974195	0 27	974195	0 45	3
58	974197	0 27	974197	0 45	2	58	974197	0 27	974197	0 45	2
59	974199	0 27	974199	0 45	1	59	974199	0 27	974199	0 45	1
60	974201	0 27	974201	0 45	0	60	974201	0 27	974201	0 45	0
M	Cosine	D'	Cosine	D'	M	M	Cosine	D'	Cosine	D'	M

M	Sine	Diff	Tang	Diff	M	M	Sine	Diff	Tang	Diff	M
0	80807	0.2	92281	0.4	50	0	9.81694	6.24	9.93910	0.41	00
1	80817	0.2	92100	0.4	59	1	81709	.24	93942	.43	59
2	80827	0.2	92113	0.4	55	2	81723	.24	93967	.43	55
3	80837	0.2	92126	0.4	57	3	81738	.24	93993	.43	57
4	80847	0.2	92139	0.4	56	4	81752	.24	94018	.43	56
5	80857	0.2	92150	0.4	55	5	81767	.24	94044	.43	55
6	80867	0.2	92163	0.4	54	6	81781	.24	94069	.43	54
7	80877	0.2	92176	0.4	53	7	81796	.24	94095	.43	53
8	80887	0.2	92189	0.4	52	8	81810	.24	94120	.43	52
9	80897	0.2	92202	0.4	51	9	81825	.24	94146	.43	51
10	80907	0.2	92215	0.4	50	10	81839	.24	94171	.43	50
11	80917	0.2	92228	0.4	49	11	81854	.24	94197	.43	49
12	80927	0.2	92241	0.4	48	12	81868	.24	94222	.43	48
13	81002	0.2	92715	0.4	47	13	81882	.24	94248	.43	47
14	81017	0.2	92740	0.4	46	14	81897	.24	94273	.43	46
15	81032	0.2	92766	0.4	45	15	81911	.24	94299	.43	45
16	81047	0.2	92792	0.4	44	16	81926	.24	94324	.43	44
17	81061	0.2	92817	0.4	43	17	81940	.24	94350	.43	43
18	81076	0.2	92843	0.4	42	18	81955	.24	94375	.43	42
19	81091	0.2	92868	0.4	41	19	81969	.24	94401	.43	41
20	81106	0.2	92894	0.4	40	20	81984	.24	94426	.43	40
21	81121	0.2	92920	0.4	39	21	82000	.24	94451	.43	39
22	81136	0.2	92945	0.4	38	22	82015	.24	94477	.43	38
23	81151	0.2	92971	0.4	37	23	82030	.24	94502	.43	37
24	81166	0.2	92996	0.4	36	24	82045	.24	94528	.43	36
25	81180	0.2	93022	0.4	35	25	82060	.24	94553	.43	35
26	81195	0.2	93048	0.4	34	26	82075	.24	94579	.43	34
27	81210	0.2	93073	0.4	33	27	82090	.24	94604	.43	33
28	81225	0.2	93099	0.4	32	28	82105	.24	94630	.43	32
29	81240	0.2	93124	0.4	31	29	82120	.24	94655	.43	31
30	81254	0.2	93150	0.4	30	30	82135	.24	94681	.43	30
31	81269	0.2	93175	0.4	29	31	82150	.24	94706	.43	29
32	81284	0.2	93201	0.4	28	32	82165	.24	94732	.43	28
33	81299	0.2	93227	0.4	27	33	82180	.24	94757	.43	27
34	81314	0.2	93252	0.4	26	34	82195	.24	94783	.43	26
35	81328	0.2	93278	0.4	25	35	82210	.24	94808	.43	25
36	81343	0.2	93303	0.4	24	36	82225	.24	94834	.43	24
37	81358	0.2	93329	0.4	23	37	82240	.24	94859	.43	23
38	81372	0.2	93354	0.4	22	38	82255	.24	94885	.43	22
39	81387	0.2	93380	0.4	21	39	82270	.24	94910	.43	21
40	81402	0.2	93405	0.4	20	40	82285	.24	94936	.43	20
41	81417	0.2	93431	0.4	19	41	82300	.24	94961	.43	19
42	81431	0.2	93457	0.4	18	42	82315	.24	94987	.43	18
43	81446	0.2	93482	0.4	17	43	82330	.24	95012	.43	17
44	81461	0.2	93508	0.4	16	44	82345	.24	95038	.43	16
45	81475	0.2	93533	0.4	15	45	82360	.24	95063	.43	15
46	81490	0.2	93559	0.4	14	46	82375	.24	95089	.43	14
47	81505	0.2	93584	0.4	13	47	82390	.24	95114	.43	13
48	81519	0.2	93610	0.4	12	48	82405	.24	95140	.43	12
49	81534	0.2	93635	0.4	11	49	82420	.24	95165	.43	11
50	81549	0.2	93661	0.4	10	50	82435	.24	95191	.43	10
51	81563	0.2	93687	0.4	9	51	82450	.24	95216	.43	9
52	81578	0.2	93712	0.4	8	52	82465	.24	95242	.43	8
53	81592	0.2	93738	0.4	7	53	82480	.24	95267	.43	7
54	81607	0.2	93763	0.4	6	54	82495	.24	95293	.43	6
55	81622	0.2	93789	0.4	5	55	82510	.24	95318	.43	5
56	81636	0.2	93814	0.4	4	56	82525	.24	95344	.43	4
57	81651	0.2	93840	0.4	3	57	82540	.24	95369	.43	3
58	81665	0.2	93865	0.4	2	58	82555	.24	95395	.43	2
59	81680	0.2	93891	0.4	1	59	82570	.24	95420	.43	1
60	81694	0.2	93916	0.4	0	60	82585	.24	95446	.43	0

M	Sine	Diff	Tang	Diff	M	M	Sine	Diff	Tang	Diff	M
0	82599	0.2	95444	0.42	60	0	82599	0.2	95444	0.42	60
1	82614	0.2	95469	0.42	59	1	82614	0.2	95469	0.42	59
2	82629	0.2	95495	0.42	58	2	82629	0.2	95495	0.42	58
3	82643	0.2	95520	0.42	57	3	82643	0.2	95520	0.42	57
4	82658	0.2	95545	0.42	56	4	82658	0.2	95545	0.42	56
5	82672	0.2	95571	0.42	55	5	82672	0.2	95571	0.42	55
6	82687	0.2	95596	0.42	54	6	82687	0.2	95596	0.42	54
7	82701	0.2	95622	0.42	53	7	82701	0.2	95622	0.42	53
8	82716	0.2	95647	0.42	52	8	82716	0.2	95647	0.42	52
9	82730	0.2	95672	0.42	51	9	82730	0.2	95672	0.42	51
10	82745	0.2	95698	0.42	50	10	82745	0.2	95698	0.42	50
11	82759	0.2	95723	0.42	49	11	82759	0.2	95723	0.42	49
12	82774	0.2	95748	0.42	48	12	82774	0.2	95748	0.42	48
13	82788	0.2	95774	0.42	47	13	82788	0.2	95774	0.42	47
14	82803	0.2	95799	0.42	46	14	82803	0.2	95799	0.42	46
15	82817	0.2	95825	0.42	45	15	82817	0.2	95825	0.42	45
16	82832	0.2	95850	0.42	44	16	82832	0.2	95850	0.42	44
17	82846	0.2	95875	0.42	43	17	82846	0.2	95875	0.42	43
18	82861	0.2	95901	0.42	42	18	82861	0.2	95901	0.42	42
19	82875	0.2	95926	0.42	41	19	82875	0.2	95926	0.42	41
20	82890	0.2	95951	0.42	40	20	82890	0.2	95951	0.42	40
21	82904	0.2	95977	0.42	39	21	82904	0.2	95977	0.42	39
22	82919	0.2	96002	0.42	38	22	82919	0.2	96002	0.42	38
23	82933	0.2	96028	0.42	37	23	82933	0.2	96028	0.42	37
24	82948	0.2	96053	0.42	36	24	82948	0.2	96053	0.42	36
25	82962	0.2	96079	0.42	35	25	82962	0.2	96079	0.42	35
26	82977	0.2	96104	0.42	34	26	82977	0.2	96104	0.42	34
27	82991	0.2	96130	0.42	33	27	82991	0.2	96130	0.42	33
28	83006	0.2	96155	0.42	32	28	83006	0.2	96155	0.42	32
29	83020	0.2	96181	0.42	31	29	83020	0.2	96181	0.42	31
30	83035	0.2	96206	0.42	30	30	83035	0.2	96206	0.42	30
31	83049	0.2	96232	0.42	29	31	83049	0.2	96232	0.42	29
32	83064	0.2	96257	0.42	28	32	83064	0.2	96257	0.42	28
33	83078	0.2	96283	0.42	27	33	83078	0.2	96283	0.42	27
34	83093	0.2	96308	0.42	26	34	83093	0.2	96308	0.42	26
35	83107	0.2	96334	0.42	25	35	83107	0.2	96334	0.42	25
36	83122	0.2	96359	0.42	24	36	83122	0.2	96359	0.42	24
37	83136	0.2	96385	0.42	23	37	83136	0.2	96385	0.42	23
38	83151	0.2	96410	0.42	22	38	83151	0.2	96410	0.42	22
39	83165	0.2	96436	0.42	21	39	83165	0.2	96436	0.42	21
40	83180	0.2	96461	0.42	20	40	83180	0.2	96461	0.42	20
41	83194	0.2	96487	0.42	19	41	83194	0.2	96487	0.42	19
42	83209	0.2	96512	0.42	18	42	83209	0.2	96512	0.42	18
43	83223	0.2	96538	0.42	17	43	83223	0.2	96538	0.42	17
44	83238	0.2	96563	0.42	16	44	83238	0.2	96563	0.42	16
45	83252	0.2	96589	0.42	15	45	83252	0.2	96589	0.42	15
46	83267	0.2	96614	0.42	14	46	83267	0.2	96614	0.42	14
47	83281	0.2	96640	0.42	13	47	83281	0.2	96640	0.42	13
48	83296	0.2	96665	0.42	12	48	83296	0.2	96665	0.42	12
49	83310	0.2	96691	0.42	11	49	83310	0.2	96691	0.42	11
50	83325	0.2	96716	0.42	10	50	83325	0.2	96716	0.42	10
51	83339	0.2	96742	0.42	9	51	83339	0.2	96742	0.42	9
52	83354	0.2	96767	0.42	8	52	83354	0.2	96767	0.42	8
53	83368	0.2	96793	0.42	7	53	83368	0.2	96793	0.42	7
54	83383	0.2	96818	0.42	6	54	83383	0.2	96818	0.42	6
55	83397	0.2	96844	0.42	5	55	83397	0.2	96844	0.42	5
56	83412	0.2	96869	0.42	4	56	83412	0.2	96869	0.42	4
57	83426	0.2	96895	0.42	3	57	83426	0.2	96895	0.42	3
58	83441	0.2	96920	0.42	2	58	83441	0.2	96920	0.42	2
59	83455	0.2	96946	0.42	1	59	83455	0.2	96946	0.42	1
60	83470	0.2	96971	0.42	0	60	83470	0.2	96971	0.42	0
M	Sine	Diff	Tang	Diff	M	M	Sine	Diff	Tang	Diff	M

N	Sine	D"	Tang	D"	N	N	Sine	D"	Tang	D"	N
0	9 8117	0 22	9 8117	0 42	60	0	9 84949	0 21	10 00000	0 42	60
1	81 90	0 22	9 8119	0 42	59	1	84961	0 21	00023	0 42	59
2	81 03	0 22	9 81 1	0 42	58	2	84974	0 21	00051	0 42	58
3	81 16	0 22	9 81 60	0 42	57	3	84986	0 21	00078	0 42	57
4	81 29	0 22	9 81 8	0 42	56	4	84992	0 21	00101	0 42	56
5	81 42	0 22	9 81 60	0 42	55	5	85012	0 21	00126	0 42	55
6	81 55	0 22	9 81 60	0 42	54	6	85024	0 21	00152	0 42	54
7	81 68	0 22	9 81 60	0 42	53	7	85037	0 21	00177	0 42	53
8	81 81	0 22	9 81 60	0 42	52	8	85049	0 21	00202	0 42	52
9	81 94	0 22	9 81 60	0 42	51	9	85062	0 21	00227	0 42	51
10	81 108	0 22	9 81 60	0 42	50	10	85074	0 21	00252	0 42	50
11	81 121	0 22	9 81 60	0 42	49	11	85087	0 21	00278	0 42	49
12	81 134	0 22	9 81 60	0 42	48	12	85100	0 21	00303	0 42	48
13	81 147	0 22	9 81 60	0 42	47	13	85112	0 21	00328	0 42	47
14	81 160	0 22	9 81 60	0 42	46	14	85125	0 21	00353	0 42	46
15	81 173	0 22	9 81 60	0 42	45	15	85137	0 21	00379	0 42	45
16	81 186	0 22	9 81 60	0 42	44	16	85150	0 21	00404	0 42	44
17	81 199	0 22	9 81 60	0 42	43	17	85162	0 21	00430	0 42	43
18	81 211	0 22	9 81 60	0 42	42	18	85175	0 21	00455	0 42	42
19	81 224	0 22	9 81 60	0 42	41	19	85187	0 21	00480	0 42	41
20	81 237	0 22	9 81 60	0 42	40	20	85200	0 21	00506	0 42	40
21	81 250	0 22	9 81 60	0 42	39	21	85212	0 21	00531	0 42	39
22	81 263	0 22	9 81 60	0 42	38	22	85225	0 21	00556	0 42	38
23	81 276	0 22	9 81 60	0 42	37	23	85237	0 21	00581	0 42	37
24	81 289	0 22	9 81 60	0 42	36	24	85250	0 21	00606	0 42	36
25	81 302	0 22	9 81 60	0 42	35	25	85262	0 21	00631	0 42	35
26	81 315	0 22	9 81 60	0 42	34	26	85275	0 21	00656	0 42	34
27	81 328	0 22	9 81 60	0 42	33	27	85287	0 21	00681	0 42	33
28	81 341	0 22	9 81 60	0 42	32	28	85300	0 21	00706	0 42	32
29	81 354	0 22	9 81 60	0 42	31	29	85312	0 21	00731	0 42	31
30	81 367	0 22	9 81 60	0 42	30	30	85325	0 21	00756	0 42	30
31	81 380	0 22	9 81 60	0 42	29	31	85337	0 21	00781	0 42	29
32	81 393	0 22	9 81 60	0 42	28	32	85350	0 21	00806	0 42	28
33	81 406	0 22	9 81 60	0 42	27	33	85362	0 21	00831	0 42	27
34	81 419	0 22	9 81 60	0 42	26	34	85375	0 21	00856	0 42	26
35	81 432	0 22	9 81 60	0 42	25	35	85387	0 21	00881	0 42	25
36	81 445	0 22	9 81 60	0 42	24	36	85400	0 21	00906	0 42	24
37	81 458	0 22	9 81 60	0 42	23	37	85412	0 21	00931	0 42	23
38	81 471	0 22	9 81 60	0 42	22	38	85425	0 21	00956	0 42	22
39	81 484	0 22	9 81 60	0 42	21	39	85437	0 21	00981	0 42	21
40	81 497	0 22	9 81 60	0 42	20	40	85450	0 21	01006	0 42	20
41	81 510	0 22	9 81 60	0 42	19	41	85462	0 21	01031	0 42	19
42	81 523	0 22	9 81 60	0 42	18	42	85475	0 21	01056	0 42	18
43	81 536	0 22	9 81 60	0 42	17	43	85487	0 21	01081	0 42	17
44	81 549	0 22	9 81 60	0 42	16	44	85500	0 21	01106	0 42	16
45	81 562	0 22	9 81 60	0 42	15	45	85512	0 21	01131	0 42	15
46	81 575	0 22	9 81 60	0 42	14	46	85525	0 21	01156	0 42	14
47	81 588	0 22	9 81 60	0 42	13	47	85537	0 21	01181	0 42	13
48	81 601	0 22	9 81 60	0 42	12	48	85550	0 21	01206	0 42	12
49	81 614	0 22	9 81 60	0 42	11	49	85562	0 21	01231	0 42	11
50	81 627	0 22	9 81 60	0 42	10	50	85575	0 21	01256	0 42	10
51	81 640	0 22	9 81 60	0 42	9	51	85587	0 21	01281	0 42	9
52	81 653	0 22	9 81 60	0 42	8	52	85600	0 21	01306	0 42	8
53	81 666	0 22	9 81 60	0 42	7	53	85612	0 21	01331	0 42	7
54	81 679	0 22	9 81 60	0 42	6	54	85625	0 21	01356	0 42	6
55	81 692	0 22	9 81 60	0 42	5	55	85637	0 21	01381	0 42	5
56	81 705	0 22	9 81 60	0 42	4	56	85650	0 21	01406	0 42	4
57	81 718	0 22	9 81 60	0 42	3	57	85662	0 21	01431	0 42	3
58	81 731	0 22	9 81 60	0 42	2	58	85675	0 21	01456	0 42	2
59	81 744	0 22	9 81 60	0 42	1	59	85687	0 21	01481	0 42	1
60	81 757	0 22	10 00000	0 42	0	60	85700	0 21	01506	0 42	0

N	Sine	D"	Tang	D"	N	N	Sine	D"	Tang	D"	N
0	9 8117	0 22	9 8117	0 42	60	0	9 84949	0 21	10 00000	0 42	60
1	81 90	0 22	9 8119	0 42	59	1	84961	0 21	00023	0 42	59
2	81 03	0 22	9 81 1	0 42	58	2	84974	0 21	00051	0 42	58
3	81 16	0 22	9 81 60	0 42	57	3	84986	0 21	00078	0 42	57
4	81 29	0 22	9 81 8	0 42	56	4	84992	0 21	00101	0 42	56
5	81 42	0 22	9 81 60	0 42	55	5	85012	0 21	00126	0 42	55
6	81 55	0 22	9 81 60	0 42	54	6	85024	0 21	00152	0 42	54
7	81 68	0 22	9 81 60	0 42	53	7	85037	0 21	00177	0 42	53
8	81 81	0 22	9 81 60	0 42	52	8	85049	0 21	00202	0 42	52
9	81 94	0 22	9 81 60	0 42	51	9	85062	0 21	00227	0 42	51
10	81 108	0 22	9 81 60	0 42	50	10	85074	0 21	00252	0 42	50
11	81 121	0 22	9 81 60	0 42	49	11	85087	0 21	00278	0 42	49
12	81 134	0 22	9 81 60	0 42	48	12	85100	0 21	00303	0 42	48
13	81 147	0 22	9 81 60	0 42	47	13	85112	0 21	00328	0 42	47
14	81 160	0 22	9 81 60	0 42	46	14	85125	0 21	00353	0 42	46
15	81 173	0 22	9 81 60	0 42	45	15	85137	0 21	00379	0 42	45
16	81 186	0 22	9 81 60	0 42	44	16	85150	0 21	00404	0 42	44
17	81 199	0 22	9 81 60	0 42	43	17	85162	0 21	00430	0 42	43
18	81 211	0 22	9 81 60	0 42	42	18	85175	0 21	00455	0 42	42
19	81 224	0 22	9 81 60	0 42	41	19	85187	0 21	00480	0 42	41
20	81 237	0 22	9 81 60	0 42	40	20	85200	0 21	00506	0 42	40
21	81 250	0 22	9 81 60	0 42	39	21	85212	0 21	00531	0 42	39
22	81 263	0 22	9 81 60	0 42	38	22	85225	0 21	00556	0 42	38
23	81 276	0 22	9 81 60	0 42	37	23	85237	0 21	00581	0 42	37
24	81 289	0 22	9 81 60	0 42	36	24	85250	0 21	00606	0 42	36
25	81 302	0 22	9 81 60	0 42	35	25	85262	0 21	00631	0 42	35
26	81 315	0 22	9 81 60	0 42	34	26	85275	0 21	00656	0 42	34
27	81 328	0 22	9 81 60	0 42	33	27	85287	0 21	00681	0 42	33
28	81 341	0 22	9 81 60	0 42	32	28	85300	0 21	00706	0 42	32
29	81 354	0 22	9 81 60	0 42	31	29	85312	0 21	00731	0 42	31
30	81 367	0 22	9 81 60	0 42	30	30	85325	0 21	00756	0 42	30
31	81 380	0 22	9 81 60	0 42	29	31	85337	0 21	00781	0 42	29
32	81 393	0 22	9 81 60	0 42	28	32	85350	0 21	00806	0 42	28
33	81 406	0 22	9 81 60	0 42	27	33	85362	0 21	00831	0 42	27
34	81 419	0 22	9 81 60	0 42	26	34	85375	0 21	00856	0 42	26
35	81 432	0 22	9 81 60	0 42	25	35	85387	0 21	00881	0 42	25
36	81 445	0 22	9 81 60	0 42	24	36	85400	0 21	00906	0 42	24
37	81 458	0 22	9 81 60	0 42	23	37	85412	0 21	00931	0 42	23
38	81 471	0 22	9 81 60	0 42	22	38	85425	0 21	00956	0 42	22
39	81 484	0 22	9 81 60	0 42	21	39	85437	0 21	00981	0 42	21
40	81 497	0 22	9 81 60	0 42	20	40	85450	0 21	01006	0 42	20
41	81 510	0 22	9 81 60	0 42	19	41	85462	0 21	01031	0 42	19
42	81 523	0 22	9 81 60	0 42	18	42	85475	0 21	01056	0 42	18
43	81 536	0 22	9 81 60	0 42	17	43	85487	0 21	01081	0 42	17
44	81 549	0 22	9 81 60	0 42	16	44	85500	0 21	01106	0 42	16
45	81 562	0 22	9 81 60	0 42	15	45	85512	0 21	01131	0 42	15
46	81 575	0 22	9 81 60	0 42	14	46	85525	0 21	01156	0 42	14
47	81 588	0 22	9 81 60	0 42	13	47	85537	0 21	01181	0 42	13
48	81 601	0 22	9 81 60	0 42	12	48	85550	0 21	01206	0 42	12
49	81 614	0 22	9 81 60	0 42	11	49	85562	0 21	01231	0 42	11
50	81 627	0 22	9 81 60	0 42	10	50	85575	0 21	01256	0 42	10
51	81 640	0 22	9 81 60	0 42	9	51	85587	0 21	01281	0 42	9
52	81 653	0 22	9 81 60	0 42	8	52	85600	0 21	01306	0 42	8
53	81 666	0 22	9 81 60	0 42	7	53	85612	0 21	01331	0 42	7
54	81 679	0 22	9 81 60	0 42	6	54	85625	0 21	01356	0 42	6
55	81 692	0 22	9 81 60	0 42	5	55	85637	0 21	01381	0 42	5
56	81 705	0 22	9 81 60	0 42	4	56	85650	0 21	01406	0 42	4
57	81 718	0 22	9 81 60	0 42	3	57	85662	0 21	01431	0 42	3
58	81 731	0 22	9 81 60	0 42	2	58	85675	0 21	01456	0 42	2
59	81 744	0 22	9 81 60	0 42	1	59	85687	0 21	01481	0 42	1
60	81 757	0 22	9 81 60	0 42	0	60	85700	0 21	01506	0 42	0

M	Sine	Diff.	Cotang.	Sec.	M	Sine	Diff.	Cotang.	Sec.	M	Sine	Diff.	Cotang.	Sec.
0	87100	0.18	10.06084	0.43	0	87778	0.18	10.06084	0.43	0	87100	0.18	10.06084	0.43
1	87113	.19	0458	42	1	87789	.18	06109	43	1	87113	.19	0458	42
2	87126	.19	04607	42	2	87800	.18	06135	43	2	87126	.19	04607	42
3	87139	.19	04632	42	3	87811	.18	06160	43	3	87139	.19	04632	42
4	87152	.19	04658	42	4	87822	.18	06186	43	4	87152	.19	04658	42
5	87164	.19	04683	42	5	87833	.18	06211	43	5	87164	.19	04683	42
6	87177	.19	04709	42	6	87844	.18	06237	43	6	87177	.19	04709	42
7	87189	.19	04734	42	7	87855	.18	06262	43	7	87189	.19	04734	42
8	87202	.19	04760	42	8	87866	.18	06288	43	8	87202	.19	04760	42
9	87215	.19	04785	42	9	87877	.18	06313	43	9	87215	.19	04785	42
10	87228	.19	04810	42	10	87888	.18	06339	43	10	87228	.19	04810	42
11	87241	.19	10.04836	42	11	87899	.18	10.06364	43	11	87241	.19	10.04836	42
12	87254	.19	04861	42	12	87910	.18	06390	43	12	87254	.19	04861	42
13	87267	.19	04887	42	13	87921	.18	06415	43	13	87267	.19	04887	42
14	87280	.19	04912	42	14	87932	.18	06441	43	14	87280	.19	04912	42
15	87293	.19	04938	42	15	87943	.18	06466	43	15	87293	.19	04938	42
16	87306	.19	04963	42	16	87954	.18	06492	43	16	87306	.19	04963	42
17	87319	.19	04989	42	17	87965	.18	06517	43	17	87319	.19	04989	42
18	87332	.19	05014	42	18	87976	.18	06543	43	18	87332	.19	05014	42
19	87345	.19	05040	42	19	87987	.18	06568	43	19	87345	.19	05040	42
20	87358	.19	05065	42	20	87998	.18	06594	43	20	87358	.19	05065	42
21	87371	.19	10.05090	42	21	88009	.18	10.06619	43	21	87371	.19	10.05090	42
22	87384	.19	05116	42	22	88020	.18	06645	43	22	87384	.19	05116	42
23	87397	.19	05141	42	23	88031	.18	06670	43	23	87397	.19	05141	42
24	87410	.19	05166	42	24	88042	.18	06696	43	24	87410	.19	05166	42
25	87423	.19	05192	42	25	88053	.18	06721	43	25	87423	.19	05192	42
26	87436	.19	05217	42	26	88064	.18	06747	43	26	87436	.19	05217	42
27	87449	.19	05243	42	27	88075	.18	06772	43	27	87449	.19	05243	42
28	87462	.19	05268	42	28	88086	.18	06798	43	28	87462	.19	05268	42
29	87475	.19	05294	42	29	88097	.18	06823	43	29	87475	.19	05294	42
30	87488	.19	05319	42	30	88108	.18	06849	43	30	87488	.19	05319	42
31	87501	.19	10.05345	42	31	88119	.18	10.06874	43	31	87501	.19	10.05345	42
32	87514	.19	05370	42	32	88130	.18	06900	43	32	87514	.19	05370	42
33	87527	.19	05396	42	33	88141	.18	06925	43	33	87527	.19	05396	42
34	87540	.19	05421	42	34	88152	.18	06951	43	34	87540	.19	05421	42
35	87553	.19	05447	42	35	88163	.18	06976	43	35	87553	.19	05447	42
36	87566	.19	05472	42	36	88174	.18	07002	43	36	87566	.19	05472	42
37	87579	.19	05498	42	37	88185	.18	07027	43	37	87579	.19	05498	42
38	87592	.19	05523	42	38	88196	.18	07053	43	38	87592	.19	05523	42
39	87605	.19	05549	42	39	88207	.18	07078	43	39	87605	.19	05549	42
40	87618	.19	05574	42	40	88218	.18	07104	43	40	87618	.19	05574	42
41	87631	.19	10.05599	42	41	88229	.18	10.07129	43	41	87631	.19	10.05599	42
42	87644	.19	05625	42	42	88240	.18	07155	43	42	87644	.19	05625	42
43	87657	.19	05650	42	43	88251	.18	07180	43	43	87657	.19	05650	42
44	87670	.19	05676	42	44	88262	.18	07206	43	44	87670	.19	05676	42
45	87683	.19	05701	42	45	88273	.18	07231	43	45	87683	.19	05701	42
46	87696	.19	05727	42	46	88284	.18	07257	43	46	87696	.19	05727	42
47	87709	.19	05752	42	47	88295	.18	07282	43	47	87709	.19	05752	42
48	87722	.19	05778	42	48	88306	.18	07308	43	48	87722	.19	05778	42
49	87735	.19	05803	42	49	88317	.18	07333	43	49	87735	.19	05803	42
50	87748	.19	05829	42	50	88328	.18	07359	43	50	87748	.19	05829	42
51	87761	.19	10.05854	42	51	88339	.18	10.07384	43	51	87761	.19	10.05854	42
52	87774	.19	05880	42	52	88350	.18	07410	43	52	87774	.19	05880	42
53	87787	.19	05905	42	53	88361	.18	07435	43	53	87787	.19	05905	42
54	87800	.19	05931	42	54	88372	.18	07461	43	54	87800	.19	05931	42
55	87813	.19	05956	42	55	88383	.18	07486	43	55	87813	.19	05956	42
56	87826	.19	05982	42	56	88394	.18	07512	43	56	87826	.19	05982	42
57	87839	.19	06007	42	57	88405	.18	07537	43	57	87839	.19	06007	42
58	87852	.19	06033	42	58	88416	.18	07563	43	58	87852	.19	06033	42
59	87865	.19	06058	42	59	88427	.18	07588	43	59	87865	.19	06058	42
60	87878	.19	06084	42	60	88438	.18	07614	43	60	87878	.19	06084	42

M	Sine	Diff.	Cotang.	Sec.	M	Sine	Diff.	Cotang.	Sec.	M	Sine	Diff.	Cotang.	Sec.
0	87100	0.18	10.06084	0.43	0	87778	0.17	10.06084	0.43	0	87100	0.18	10.06084	0.43
1	87113	.18	0458	42	1	87789	.17	06109	43	1	87113	.18	0458	42
2	87126	.18	04607	42	2	87800	.17	06135	43	2	87126	.18	04607	42
3	87139	.18	04632	42	3	87811	.17	06160	43	3	87139	.18	04632	42
4	87152	.18	04658	42	4	87822	.17	06186	43	4	87152	.18	04658	42
5	87164	.18	04683	42	5	87833	.17	06211	43	5	87164	.18	04683	42
6	87177	.18	04709	42	6	87844	.17	06237	43	6	87177	.18	04709	42
7	87189	.18	04734	42	7	87855	.17	06262	43	7	87189	.18	04734	42
8	87202	.18	04760	42	8	87866	.17	06288	43	8	87202	.18	04760	42
9	87215	.18	04785	42	9	87877	.17	06313	43	9	87215	.18	04785	42
10	87228	.18	04810	42	10	87888	.17	06339	43	10	87228	.18	04810	42
11	87241	.18	10.04836	42	11	87899	.17	10.06364	43	11	87241	.18	10.04836	42
12	87254	.18	04861	42	12	87910	.17	06390	43	12	87254	.18	04861	42
13	87267	.18	04887	42	13	87921	.17	06415	43	13	87267	.18	04887	42
14	87280	.18	04912	42	14	87932	.17	06441	43	14	87280	.18	04912	42
15	87293	.18	04938	42	15	87943	.17	06466	43	15	87293	.18	04938	42
16	87306	.18	04963	42	16	87954	.17	06492	43	16	87306	.18	04963	42
17	87319	.18	04989	42	17	87965	.17	06517	43	17	87319	.18	04989	42
18	87332	.18	05014	42	18	87976	.17	06543	43	18	87332	.18	05014	42
19	87345	.18	05040	42	19	87987	.17	06568	43	19	87345	.18	05040	42
20	87358	.18	05065	42	20	87998	.17	06594	43	20	87358	.18	05065	42
21	87371	.18	10.05090	42	21	88009	.17	10.06619	43	21	87371	.18	10.05090	42
22	87384	.18	05116	42	22	88020	.17	06645	43	22	87384	.18	05116	42
23	87397	.18	05141	42	23	88031	.17	06670	43	23	87397	.18	05141	42
24	87410	.18	05166	42	24	88042	.17	06696	43	24	87410	.18	05166	42
25	87423	.18	05192	42	25	88053	.17	06721	43	25	87423	.18	05192	42
26	87436	.18	05217	42	26	88064	.17	06747	43	26	87436	.18	05217	42
27	87449	.18	05243	42	27	88075	.17	06772	43	27	87449	.18	05243	42
28	87462	.18	05268	42	28	88086	.17	06798	43	28	87462	.18	05268	42
29	87475	.18	05294	42	29	88097	.17	06823	43	29	87475	.18	05294	42
30	87488	.18	05319	42	30	88108	.17	06849	43	30	87488	.18	05319	42
31	87501	.18	10.05345	42	31	88119	.17	10.06874	43	31	87501	.18	10.05345	42

M	Sec	D	Tab	D	M	M	Sec	D	Tab	D	M
0	89800	0	10.10718	0.44	60	0	9.90245	0.16	10.13259	0.44	60
1	89801	1	10743	.44	59	1	90244	.16	12315	.44	59
2	89802	2	10773	.44	58	2	90243	.16	12341	.44	58
3	89803	3	10803	.44	57	3	90242	.16	12367	.44	57
4	89804	4	10832	.44	56	4	90241	.16	12394	.44	56
5	89805	5	10862	.44	55	5	90240	.16	12420	.44	55
6	89806	6	10892	.44	54	6	90239	.16	12446	.44	54
7	89807	7	10922	.44	53	7	90238	.16	12473	.44	53
8	89808	8	10952	.44	52	8	90237	.16	12500	.44	52
9	89809	9	10982	.44	51	9	90236	.16	12527	.44	51
10	89810	10	10980	.44	50	10	90235	.16	12553	.44	50
11	89811	11	10.11006	.44	49	11	90234	.16	10.12580	.44	49
12	89812	12	11032	.44	48	12	90233	.16	12606	.44	48
13	89813	13	11058	.44	47	13	90232	.16	12632	.44	47
14	89814	14	11084	.44	46	14	90231	.16	12658	.44	46
15	89815	15	11110	.44	45	15	90230	.16	12684	.44	45
16	89816	16	11136	.44	44	16	90229	.16	12710	.44	44
17	89817	17	11162	.44	43	17	90228	.16	12736	.44	43
18	89818	18	11188	.44	42	18	90227	.16	12762	.44	42
19	89819	19	11214	.44	41	19	90226	.16	12788	.44	41
20	89820	20	11240	.44	40	20	90225	.16	12814	.44	40
21	89821	21	11266	.44	39	21	90224	.16	12840	.44	39
22	89822	22	11292	.44	38	22	90223	.16	12866	.44	38
23	89823	23	11318	.44	37	23	90222	.16	12892	.44	37
24	89824	24	11344	.44	36	24	90221	.16	12918	.44	36
25	89825	25	11370	.44	35	25	90220	.16	12944	.44	35
26	89826	26	11396	.44	34	26	90219	.16	12970	.44	34
27	89827	27	11422	.44	33	27	90218	.16	12996	.44	33
28	89828	28	11448	.44	32	28	90217	.16	13022	.44	32
29	89829	29	11474	.44	31	29	90216	.16	13048	.44	31
30	89830	30	11500	.44	30	30	90215	.16	13074	.44	30
31	89831	31	11526	.44	29	31	90214	.16	13100	.44	29
32	89832	32	11552	.44	28	32	90213	.16	13126	.44	28
33	89833	33	11578	.44	27	33	90212	.16	13152	.44	27
34	89834	34	11604	.44	26	34	90211	.16	13178	.44	26
35	89835	35	11630	.44	25	35	90210	.16	13204	.44	25
36	89836	36	11656	.44	24	36	90209	.16	13230	.44	24
37	89837	37	11682	.44	23	37	90208	.16	13256	.44	23
38	89838	38	11708	.44	22	38	90207	.16	13282	.44	22
39	89839	39	11734	.44	21	39	90206	.16	13308	.44	21
40	89840	40	11760	.44	20	40	90205	.16	13334	.44	20
41	89841	41	11786	.44	19	41	90204	.16	13360	.44	19
42	89842	42	11812	.44	18	42	90203	.16	13386	.44	18
43	89843	43	11838	.44	17	43	90202	.16	13412	.44	17
44	89844	44	11864	.44	16	44	90201	.16	13438	.44	16
45	89845	45	11890	.44	15	45	90200	.16	13464	.44	15
46	89846	46	11916	.44	14	46	90199	.16	13490	.44	14
47	89847	47	11942	.44	13	47	90198	.16	13516	.44	13
48	89848	48	11968	.44	12	48	90197	.16	13542	.44	12
49	89849	49	11994	.44	11	49	90196	.16	13568	.44	11
50	89850	50	12020	.44	10	50	90195	.16	13594	.44	10
51	89851	51	12046	.44	9	51	90194	.16	13620	.44	9
52	89852	52	12072	.44	8	52	90193	.16	13646	.44	8
53	89853	53	12098	.44	7	53	90192	.16	13672	.44	7
54	89854	54	12124	.44	6	54	90191	.16	13698	.44	6
55	89855	55	12150	.44	5	55	90190	.16	13724	.44	5
56	89856	56	12176	.44	4	56	90189	.16	13750	.44	4
57	89857	57	12202	.44	3	57	90188	.16	13776	.44	3
58	89858	58	12228	.44	2	58	90187	.16	13802	.44	2
59	89859	59	12254	.44	1	59	90186	.16	13828	.44	1
60	89860	60	12280	.44	0	60	90185	.16	13854	.44	0

M	Sec	D	Tab	D	M	M	Sec	D	Tab	D	M
0	89800	0	10.13874	0.44	60	0	9.90245	0.16	10.13259	0.44	60
1	89801	1	13900	.44	59	1	90244	.16	12315	.44	59
2	89802	2	13927	.44	58	2	90243	.16	12341	.44	58
3	89803	3	13954	.44	57	3	90242	.16	12367	.44	57
4	89804	4	13980	.44	56	4	90241	.16	12394	.44	56
5	89805	5	14007	.44	55	5	90240	.16	12420	.44	55
6	89806	6	14033	.44	54	6	90239	.16	12446	.44	54
7	89807	7	14060	.44	53	7	90238	.16	12473	.44	53
8	89808	8	14087	.44	52	8	90237	.16	12500	.44	52
9	89809	9	14113	.44	51	9	90236	.16	12527	.44	51
10	89810	10	14140	.44	50	10	90235	.16	12553	.44	50
11	89811	11	14166	.44	49	11	90234	.16	10.12580	.44	49
12	89812	12	14193	.44	48	12	90233	.16	12606	.44	48
13	89813	13	14220	.44	47	13	90232	.16	12632	.44	47
14	89814	14	14246	.44	46	14	90231	.16	12658	.44	46
15	89815	15	14273	.44	45	15	90230	.16	12684	.44	45
16	89816	16	14300	.44	44	16	90229	.16	12710	.44	44
17	89817	17	14326	.44	43	17	90228	.16	12736	.44	43
18	89818	18	14353	.44	42	18	90227	.16	12762	.44	42
19	89819	19	14380	.44	41	19	90226	.16	12788	.44	41
20	89820	20	14406	.44	40	20	90225	.16	12814	.44	40
21	89821	21	14433	.44	39	21	90224	.16	12840	.44	39
22	89822	22	14460	.44	38	22	90223	.16	12866	.44	38
23	89823	23	14486	.44	37	23	90222	.16	12892	.44	37
24	89824	24	14513	.44	36	24	90221	.16	12918	.44	36
25	89825	25	14540	.44	35	25	90220	.16	12944	.44	35
26	89826	26	14566	.44	34	26	90219	.16	12970	.44	34
27	89827	27	14593	.44	33	27	90218	.16	12996	.44	33
28	89828	28	14620	.44	32	28	90217	.16	13022	.44	32
29	89829	29	14646	.44	31	29	90216	.16	13048	.44	31
30	89830	30	14673	.44	30	30	90215	.16	13074	.44	30
31	89831	31	14700	.44	29	31	90214	.16	13100	.44	29
32	89832	32	14726	.44	28	32	90213	.16	13126	.44	28
33	89833	33	14753	.44	27	33	90212	.16	13152	.44	27
34	89834	34	14780	.44	26	34	90211	.16	13178	.44	26
35	89835	35	14806	.44	25	35	90210	.16	13204	.44	25
36	89836	36	14833	.44	24	36	90209	.16	13230	.44	24
37	89837	37	14860	.44	23	37	90208	.16	13256	.44	23
38	89838	38	14886	.44	22	38	90207	.16	13282	.44	22
39	89839	39	14913	.44	21	39	90206	.16	13308	.44	21
40	89840	40	14940	.44	20	40	90205	.16	13334	.44	20
41	89841	41	14966	.44	19	41	90204	.16	13360	.44	19
42	89842	42	14993	.44	18	42	90203	.16	13386	.44	18
43	89843	43	15020	.44	17	43	90202	.16	13412	.44	17
44	89844	44	15046	.44	16	44	90201	.16	13438	.44	16
45	89845	45	15073	.44	15	45	90200	.16	13464	.44	15
46	89846	46	15100	.44	14	46	90199	.16	13490	.44	14
47	89847	47	15126	.44	13	47	90198	.16	13516	.44	13
48	89848	48	15153	.44	12	48	90197	.16	13542	.44	12
49	89849	49	15180	.44	11	49	90196	.16	13568	.44	11
50	89850	50	15206	.44	10	50	90195	.16	13594	.44	10
51	89851	51	15233	.44	9	51	90194	.16	13620	.44	9
52	89852	52	15260	.44	8	52	90193	.16	13646	.44	8
53	89853	53	15286	.44	7	53	90192	.16	13672	.44	7
54	89854	54	15313	.44	6	54	90191	.16	13698	.44	6
55	89855	55	15340	.44	5	55	90190	.16	13724	.44	5
56	89856	56	15366	.44	4	56	90189	.16	13750	.44	4
57	89857	57	15393	.44	3	57	90188	.16	13776	.44	3
58	89858	58	15420	.44	2	58	90187	.16	13802	.44	2
59	89859	59	15446	.44	1	59	90186	.16	13828	.44	1
60	89860	60	15473	.44	0	60	90185	.16	13854	.44	0
61	89861	61	15500	.44	59	61	90184	.16	13880	.44	59

M	Sec	Dist	Lat	M	Sec	Dist	Lat	M	Sec	Dist	Lat
0	0.02339	10.17101	0.45	60	0.02339	10.17101	0.45	60	0.02339	10.17101	0.45
1	0.02339	17121	45	59	0.02339	17121	45	59	0.02339	17121	45
2	0.02339	17131	45	58	0.02339	17131	45	58	0.02339	17131	45
3	0.02339	17141	45	57	0.02339	17141	45	57	0.02339	17141	45
4	0.02339	17151	45	56	0.02339	17151	45	56	0.02339	17151	45
5	0.02339	17161	45	55	0.02339	17161	45	55	0.02339	17161	45
6	0.02339	17171	45	54	0.02339	17171	45	54	0.02339	17171	45
7	0.02339	17181	45	53	0.02339	17181	45	53	0.02339	17181	45
8	0.02339	17191	45	52	0.02339	17191	45	52	0.02339	17191	45
9	0.02339	17201	45	51	0.02339	17201	45	51	0.02339	17201	45
10	0.02339	17211	45	50	0.02339	17211	45	50	0.02339	17211	45
11	0.02339	17221	45	49	0.02339	17221	45	49	0.02339	17221	45
12	0.02339	17231	45	48	0.02339	17231	45	48	0.02339	17231	45
13	0.02339	17241	45	47	0.02339	17241	45	47	0.02339	17241	45
14	0.02339	17251	45	46	0.02339	17251	45	46	0.02339	17251	45
15	0.02339	17261	45	45	0.02339	17261	45	45	0.02339	17261	45
16	0.02339	17271	45	44	0.02339	17271	45	44	0.02339	17271	45
17	0.02339	17281	45	43	0.02339	17281	45	43	0.02339	17281	45
18	0.02339	17291	45	42	0.02339	17291	45	42	0.02339	17291	45
19	0.02339	17301	45	41	0.02339	17301	45	41	0.02339	17301	45
20	0.02339	17311	45	40	0.02339	17311	45	40	0.02339	17311	45
21	0.02339	17321	45	39	0.02339	17321	45	39	0.02339	17321	45
22	0.02339	17331	45	38	0.02339	17331	45	38	0.02339	17331	45
23	0.02339	17341	45	37	0.02339	17341	45	37	0.02339	17341	45
24	0.02339	17351	45	36	0.02339	17351	45	36	0.02339	17351	45
25	0.02339	17361	45	35	0.02339	17361	45	35	0.02339	17361	45
26	0.02339	17371	45	34	0.02339	17371	45	34	0.02339	17371	45
27	0.02339	17381	45	33	0.02339	17381	45	33	0.02339	17381	45
28	0.02339	17391	45	32	0.02339	17391	45	32	0.02339	17391	45
29	0.02339	17401	45	31	0.02339	17401	45	31	0.02339	17401	45
30	0.02339	17411	45	30	0.02339	17411	45	30	0.02339	17411	45
31	0.02339	17421	45	29	0.02339	17421	45	29	0.02339	17421	45
32	0.02339	17431	45	28	0.02339	17431	45	28	0.02339	17431	45
33	0.02339	17441	45	27	0.02339	17441	45	27	0.02339	17441	45
34	0.02339	17451	45	26	0.02339	17451	45	26	0.02339	17451	45
35	0.02339	17461	45	25	0.02339	17461	45	25	0.02339	17461	45
36	0.02339	17471	45	24	0.02339	17471	45	24	0.02339	17471	45
37	0.02339	17481	45	23	0.02339	17481	45	23	0.02339	17481	45
38	0.02339	17491	45	22	0.02339	17491	45	22	0.02339	17491	45
39	0.02339	17501	45	21	0.02339	17501	45	21	0.02339	17501	45
40	0.02339	17511	45	20	0.02339	17511	45	20	0.02339	17511	45
41	0.02339	17521	45	19	0.02339	17521	45	19	0.02339	17521	45
42	0.02339	17531	45	18	0.02339	17531	45	18	0.02339	17531	45
43	0.02339	17541	45	17	0.02339	17541	45	17	0.02339	17541	45
44	0.02339	17551	45	16	0.02339	17551	45	16	0.02339	17551	45
45	0.02339	17561	45	15	0.02339	17561	45	15	0.02339	17561	45
46	0.02339	17571	45	14	0.02339	17571	45	14	0.02339	17571	45
47	0.02339	17581	45	13	0.02339	17581	45	13	0.02339	17581	45
48	0.02339	17591	45	12	0.02339	17591	45	12	0.02339	17591	45
49	0.02339	17601	45	11	0.02339	17601	45	11	0.02339	17601	45
50	0.02339	17611	45	10	0.02339	17611	45	10	0.02339	17611	45
51	0.02339	17621	45	9	0.02339	17621	45	9	0.02339	17621	45
52	0.02339	17631	45	8	0.02339	17631	45	8	0.02339	17631	45
53	0.02339	17641	45	7	0.02339	17641	45	7	0.02339	17641	45
54	0.02339	17651	45	6	0.02339	17651	45	6	0.02339	17651	45
55	0.02339	17661	45	5	0.02339	17661	45	5	0.02339	17661	45
56	0.02339	17671	45	4	0.02339	17671	45	4	0.02339	17671	45
57	0.02339	17681	45	3	0.02339	17681	45	3	0.02339	17681	45
58	0.02339	17691	45	2	0.02339	17691	45	2	0.02339	17691	45
59	0.02339	17701	45	1	0.02339	17701	45	1	0.02339	17701	45
60	0.02339	17711	45	0	0.02339	17711	45	0	0.02339	17711	45

M	Sec	Dist	Lat	M	Sec	Dist	Lat
0	9.2254	10.2421	0.13	0	9.2254	10.2421	0.13
1	9.2255	2449	0.13	1	9.2255	2449	0.13
2	9.2256	2447	0.13	2	9.2256	2447	0.13
3	9.2257	2453	0.13	3	9.2257	2453	0.13
4	9.2258	2459	0.13	4	9.2258	2459	0.13
5	9.2259	2465	0.13	5	9.2259	2465	0.13
6	9.2260	2471	0.13	6	9.2260	2471	0.13
7	9.2261	2477	0.13	7	9.2261	2477	0.13
8	9.2262	2483	0.13	8	9.2262	2483	0.13
9	9.2263	2489	0.13	9	9.2263	2489	0.13
10	9.2264	2495	0.13	10	9.2264	2495	0.13
11	9.2265	2501	0.13	11	9.2265	2501	0.13
12	9.2266	2507	0.13	12	9.2266	2507	0.13
13	9.2267	2513	0.13	13	9.2267	2513	0.13
14	9.2268	2519	0.13	14	9.2268	2519	0.13
15	9.2269	2525	0.13	15	9.2269	2525	0.13
16	9.2270	2531	0.13	16	9.2270	2531	0.13
17	9.2271	2537	0.13	17	9.2271	2537	0.13
18	9.2272	2543	0.13	18	9.2272	2543	0.13
19	9.2273	2549	0.13	19	9.2273	2549	0.13
20	9.2274	2555	0.13	20	9.2274	2555	0.13
21	9.2275	2561	0.13	21	9.2275	2561	0.13
22	9.2276	2567	0.13	22	9.2276	2567	0.13
23	9.2277	2573	0.13	23	9.2277	2573	0.13
24	9.2278	2579	0.13	24	9.2278	2579	0.13
25	9.2279	2585	0.13	25	9.2279	2585	0.13
26	9.2280	2591	0.13	26	9.2280	2591	0.13
27	9.2281	2597	0.13	27	9.2281	2597	0.13
28	9.2282	2603	0.13	28	9.2282	2603	0.13
29	9.2283	2609	0.13	29	9.2283	2609	0.13
30	9.2284	2615	0.13	30	9.2284	2615	0.13
31	9.2285	2621	0.13	31	9.2285	2621	0.13
32	9.2286	2627	0.13	32	9.2286	2627	0.13
33	9.2287	2633	0.13	33	9.2287	2633	0.13
34	9.2288	2639	0.13	34	9.2288	2639	0.13
35	9.2289	2645	0.13	35	9.2289	2645	0.13
36	9.2290	2651	0.13	36	9.2290	2651	0.13
37	9.2291	2657	0.13	37	9.2291	2657	0.13
38	9.2292	2663	0.13	38	9.2292	2663	0.13
39	9.2293	2669	0.13	39	9.2293	2669	0.13
40	9.2294	2675	0.13	40	9.2294	2675	0.13
41	9.2295	2681	0.13	41	9.2295	2681	0.13
42	9.2296	2687	0.13	42	9.2296	2687	0.13
43	9.2297	2693	0.13	43	9.2297	2693	0.13
44	9.2298	2699	0.13	44	9.2298	2699	0.13
45	9.2299	2705	0.13	45	9.2299	2705	0.13
46	9.2300	2711	0.13	46	9.2300	2711	0.13
47	9.2301	2717	0.13	47	9.2301	2717	0.13
48	9.2302	2723	0.13	48	9.2302	2723	0.13
49	9.2303	2729	0.13	49	9.2303	2729	0.13
50	9.2304	2735	0.13	50	9.2304	2735	0.13
51	9.2305	2741	0.13	51	9.2305	2741	0.13
52	9.2306	2747	0.13	52	9.2306	2747	0.13
53	9.2307	2753	0.13	53	9.2307	2753	0.13
54	9.2308	2759	0.13	54	9.2308	2759	0.13
55	9.2309	2765	0.13	55	9.2309	2765	0.13
56	9.2310	2771	0.13	56	9.2310	2771	0.13
57	9.2311	2777	0.13	57	9.2311	2777	0.13
58	9.2312	2783	0.13	58	9.2312	2783	0.13
59	9.2313	2789	0.13	59	9.2313	2789	0.13
60	9.2314	2795	0.13	60	9.2314	2795	0.13

N	Sine	Log	Sec	Tang.	Cot	M	N	Sine	Log	Sec	Tang.	Cot	M
0	9.94182	0.12	10.23625	0.50	60	0	9.94182	0.12	10.23625	0.50	60	60	0
1	9.94189	.12	2.655	.50	59	1	9.94189	.12	2.655	.50	59	59	1
2	9.94196	.12	2.684	.50	58	2	9.94196	.12	2.684	.50	58	58	2
3	9.94203	.12	25714	.50	57	3	9.94203	.12	25714	.50	57	57	3
4	9.94210	.12	25714	.50	56	4	9.94210	.12	25714	.50	56	56	4
5	9.94217	.12	2.774	.50	55	5	9.94217	.12	2.774	.50	55	55	5
6	9.94224	.12	2.801	.50	54	6	9.94224	.12	2.801	.50	54	54	6
7	9.94231	.12	2.851	.50	53	7	9.94231	.12	2.851	.50	53	53	7
8	9.94238	.12	2.86	.50	52	8	9.94238	.12	2.86	.50	52	52	8
9	9.94245	.12	2.89	.50	51	9	9.94245	.12	2.89	.50	51	51	9
10	9.94252	.12	2.902	.50	50	10	9.94252	.12	2.902	.50	50	50	10
11	9.94259	.12	10.23625	.50	49	11	9.94259	.12	10.23625	.50	49	49	11
12	9.94266	.12	2.91	.50	48	12	9.94266	.12	2.91	.50	48	48	12
13	9.94273	.12	2.91	.50	47	13	9.94273	.12	2.91	.50	47	47	13
14	9.94279	.12	2.91	.50	46	14	9.94279	.12	2.91	.50	46	46	14
15	9.94286	.12	2.91	.50	45	15	9.94286	.12	2.91	.50	45	45	15
16	9.94293	.12	2.91	.50	44	16	9.94293	.12	2.91	.50	44	44	16
17	9.94300	.12	2.91	.50	43	17	9.94300	.12	2.91	.50	43	43	17
18	9.94307	.12	2.91	.50	42	18	9.94307	.12	2.91	.50	42	42	18
19	9.94314	.12	2.91	.50	41	19	9.94314	.12	2.91	.50	41	41	19
20	9.94321	.12	2.91	.50	40	20	9.94321	.12	2.91	.50	40	40	20
21	9.94328	.12	2.91	.50	39	21	9.94328	.12	2.91	.50	39	39	21
22	9.94335	.12	2.91	.50	38	22	9.94335	.12	2.91	.50	38	38	22
23	9.94342	.12	2.91	.50	37	23	9.94342	.12	2.91	.50	37	37	23
24	9.94349	.12	2.91	.50	36	24	9.94349	.12	2.91	.50	36	36	24
25	9.94356	.12	2.91	.50	35	25	9.94356	.12	2.91	.50	35	35	25
26	9.94363	.12	2.91	.50	34	26	9.94363	.12	2.91	.50	34	34	26
27	9.94370	.12	2.91	.50	33	27	9.94370	.12	2.91	.50	33	33	27
28	9.94377	.12	2.91	.50	32	28	9.94377	.12	2.91	.50	32	32	28
29	9.94384	.12	2.91	.50	31	29	9.94384	.12	2.91	.50	31	31	29
30	9.94391	.12	2.91	.50	30	30	9.94391	.12	2.91	.50	30	30	30
31	9.94398	.12	2.91	.50	29	31	9.94398	.12	2.91	.50	29	29	31
32	9.94405	.12	2.91	.50	28	32	9.94405	.12	2.91	.50	28	28	32
33	9.94412	.12	2.91	.50	27	33	9.94412	.12	2.91	.50	27	27	33
34	9.94419	.12	2.91	.50	26	34	9.94419	.12	2.91	.50	26	26	34
35	9.94426	.12	2.91	.50	25	35	9.94426	.12	2.91	.50	25	25	35
36	9.94433	.12	2.91	.50	24	36	9.94433	.12	2.91	.50	24	24	36
37	9.94440	.12	2.91	.50	23	37	9.94440	.12	2.91	.50	23	23	37
38	9.94447	.12	2.91	.50	22	38	9.94447	.12	2.91	.50	22	22	38
39	9.94454	.12	2.91	.50	21	39	9.94454	.12	2.91	.50	21	21	39
40	9.94461	.12	2.91	.50	20	40	9.94461	.12	2.91	.50	20	20	40
41	9.94468	.12	2.91	.50	19	41	9.94468	.12	2.91	.50	19	19	41
42	9.94475	.12	2.91	.50	18	42	9.94475	.12	2.91	.50	18	18	42
43	9.94482	.12	2.91	.50	17	43	9.94482	.12	2.91	.50	17	17	43
44	9.94489	.12	2.91	.50	16	44	9.94489	.12	2.91	.50	16	16	44
45	9.94496	.12	2.91	.50	15	45	9.94496	.12	2.91	.50	15	15	45
46	9.94503	.12	2.91	.50	14	46	9.94503	.12	2.91	.50	14	14	46
47	9.94510	.12	2.91	.50	13	47	9.94510	.12	2.91	.50	13	13	47
48	9.94517	.12	2.91	.50	12	48	9.94517	.12	2.91	.50	12	12	48
49	9.94524	.12	2.91	.50	11	49	9.94524	.12	2.91	.50	11	11	49
50	9.94531	.12	2.91	.50	10	50	9.94531	.12	2.91	.50	10	10	50
51	9.94538	.12	2.91	.50	9	51	9.94538	.12	2.91	.50	9	9	51
52	9.94545	.12	2.91	.50	8	52	9.94545	.12	2.91	.50	8	8	52
53	9.94552	.12	2.91	.50	7	53	9.94552	.12	2.91	.50	7	7	53
54	9.94559	.12	2.91	.50	6	54	9.94559	.12	2.91	.50	6	6	54
55	9.94566	.12	2.91	.50	5	55	9.94566	.12	2.91	.50	5	5	55
56	9.94573	.12	2.91	.50	4	56	9.94573	.12	2.91	.50	4	4	56
57	9.94580	.12	2.91	.50	3	57	9.94580	.12	2.91	.50	3	3	57
58	9.94587	.12	2.91	.50	2	58	9.94587	.12	2.91	.50	2	2	58
59	9.94594	.12	2.91	.50	1	59	9.94594	.12	2.91	.50	1	1	59
60	9.94601	.12	2.91	.50	0	60	9.94601	.12	2.91	.50	0	0	60
M	Cosine	D	C	Tang	D	M	M	Cosine	D	C	Tang	D	M

M	S	T	Tang	Sec	M	M	S	T	Tang	Sec	M
0	9.94593	0.11	10.27433	0.51	60	0	9.94593	0.11	10.27433	0.51	60
1	9.94600	.11	2746	.51	59	1	9.94600	.11	2746	.51	59
2	9.94607	.11	27494	.51	58	2	9.94607	.11	27494	.51	58
3	9.94614	.11	27524	.51	57	3	9.94614	.11	27527	.51	57
4	9.94621	.11	27555	.51	56	4	9.94614	.11	27548	.51	56
5	9.94627	.11	27585	.51	55	5	9.94621	.11	27580	.51	55
6	9.94634	.11	27616	.51	54	6	9.94627	.11	27617	.51	54
7	9.94640	.11	27646	.51	53	7	9.94634	.11	27652	.51	53
8	9.94647	.11	2.677	.51	52	8	9.94640	.11	2.674	.51	52
9	9.94654	.11	27707	.51	51	9	9.94647	.11	27695	.51	51
10	9.94660	.11	27738	.51	50	10	9.94654	.11	27726	.51	50
11	9.94667	.11	10.27763	.51	49	11	9.94660	.11	27758	.51	49
12	9.94674	.11	27799	.51	48	12	9.94667	.11	27792	.51	48
13	9.94681	.11	27830	.51	47	13	9.94674	.11	27823	.51	47
14	9.94688	.11	27861	.51	46	14	9.94681	.11	27854	.51	46
15	9.94695	.11	27891	.51	45	15	9.94688	.11	27885	.51	45
16	9.94702	.11	27922	.51	44	16	9.94695	.11	27916	.51	44
17	9.94709	.11	27953	.51	43	17	9.94702	.11	27946	.51	43
18	9.94716	.11	27984	.51	42	18	9.94709	.11	27978	.51	42
19	9.94723	.11	28014	.51	41	19	9.94716	.11	28009	.51	41
20	9.94730	.11	28045	.51	40	20	9.94723	.11	28041	.51	40
21	9.94737	.11	10.28075	.51	39	21	9.94730	.11	28072	.51	39
22	9.94744	.11	28106	.51	38	22	9.94737	.11	28103	.51	38
23	9.94751	.11	28137	.51	37	23	9.94744	.11	28134	.51	37
24	9.94758	.11	28168	.51	36	24	9.94751	.11	28165	.51	36
25	9.94765	.11	28199	.51	35	25	9.94758	.11	28196	.51	35
26	9.94772	.11	28230	.51	34	26	9.94765	.11	28227	.51	34
27	9.94779	.11	28260	.51	33	27	9.94772	.11	28258	.51	33
28	9.94786	.11	28291	.51	32	28	9.94779	.11	28289	.51	32
29	9.94793	.11	28322	.51	31	29	9.94786	.11	28320	.51	31
30	9.94800	.11	10.28353	.51	30	30	9.94793	.11	28351	.51	30
31	9.94807	.11	28384	.51	29	31	9.94800	.11	28382	.51	29
32	9.94814	.11	28415	.51	28	32	9.94807	.11	28413	.51	28
33	9.94821	.11	28446	.51	27	33	9.94814	.11	28444	.51	27
34	9.94828	.11	28477	.51	26	34	9.94821	.11	28475	.51	26
35	9.94835	.11	28508	.51	25	35	9.94828	.11	28506	.51	25
36	9.94842	.11	28539	.51	24	36	9.94835	.11	28537	.51	24
37	9.94849	.11	28570	.51	23	37	9.94842	.11	28568	.51	23
38	9.94856	.11	28601	.51	22	38	9.94849	.11	28599	.51	22
39	9.94863	.11	28632	.51	21	39	9.94856	.11	28630	.51	21
40	9.94870	.11	10.28663	.51	20	40	9.94863	.11	28661	.51	20
41	9.94877	.11	28694	.51	19	41	9.94870	.11	28692	.51	19
42	9.94884	.11	28725	.51	18	42	9.94877	.11	28723	.51	18
43	9.94891	.11	28756	.51	17	43	9.94884	.11	28754	.51	17
44	9.94898	.11	28787	.51	16	44	9.94891	.11	28785	.51	16
45	9.94905	.11	28818	.51	15	45	9.94898	.11	28816	.51	15
46	9.94912	.11	28849	.51	14	46	9.94905	.11	28847	.51	14
47	9.94919	.11	28880	.51	13	47	9.94912	.11	28878	.51	13
48	9.94926	.11	28911	.51	12	48	9.94919	.11	28909	.51	12
49	9.94933	.11	28942	.51	11	49	9.94926	.11	28940	.51	11
50	9.94940	.11	10.28973	.51	10	50	9.94933	.11	28971	.51	10
51	9.94947	.11	28974	.51	9	51	9.94940	.11	29002	.51	9
52	9.94954	.11	29005	.51	8	52	9.94947	.11	29033	.51	8
53	9.94961	.11	29036	.51	7	53	9.94954	.11	29064	.51	7
54	9.94968	.11	29067	.51	6	54	9.94961	.11	29095	.51	6
55	9.94975	.11	29098	.51	5	55	9.94968	.11	29126	.51	5
56	9.94982	.11	29129	.51	4	56	9.94975	.11	29157	.51	4
57	9.94989	.11	29160	.51	3	57	9.94982	.11	29188	.51	3
58	9.94996	.11	29191	.51	2	58	9.94989	.11	29219	.51	2
59	9.95003	.11	29222	.51	1	59	9.94996	.11	29250	.51	1
60	9.95010	.11	29253	.51	0	60	9.95003	.11	29281	.51	0
M	C	C	C	D	M	M	C	C	C	D	M

M	Sec	Log	Diff	M	M	Sec	Log	Diff	M	M	Sec	Log	Diff	M
0		0.10		0	0	9.95728	10.38133	0.55	60	0	9.95728	10.38133	0.55	60
1	0.10	0.10		1	1	9.95733	10.38136	0.55	59	1	9.95733	10.38136	0.55	59
2	0.10	0.10		2	2	9.95737	10.38139	0.55	58	2	9.95737	10.38139	0.55	58
3	0.10	0.10		3	3	9.95743	10.38142	0.55	57	3	9.95743	10.38142	0.55	57
4	0.10	0.10		4	4	9.95751	10.38145	0.55	56	4	9.95751	10.38145	0.55	56
5	0.10	0.10		5	5	9.95757	10.38148	0.55	55	5	9.95757	10.38148	0.55	55
6	0.10	0.10		6	6	9.95763	10.38151	0.55	54	6	9.95763	10.38151	0.55	54
7	0.10	0.10		7	7	9.95770	10.38154	0.55	53	7	9.95770	10.38154	0.55	53
8	0.10	0.10		8	8	9.95775	10.38157	0.55	52	8	9.95775	10.38157	0.55	52
9	0.10	0.10		9	9	9.95780	10.38160	0.55	51	9	9.95780	10.38160	0.55	51
10	0.10	0.10		10	10	9.95786	10.38163	0.55	50	10	9.95786	10.38163	0.55	50
11	0.10	0.10		11	11	9.95792	10.38166	0.55	49	11	9.95792	10.38166	0.55	49
12	0.10	0.10		12	12	9.95798	10.38169	0.55	48	12	9.95798	10.38169	0.55	48
13	0.10	0.10		13	13	9.95804	10.38172	0.55	47	13	9.95804	10.38172	0.55	47
14	0.10	0.10		14	14	9.95810	10.38175	0.55	46	14	9.95810	10.38175	0.55	46
15	0.10	0.10		15	15	9.95815	10.38178	0.55	45	15	9.95815	10.38178	0.55	45
16	0.10	0.10		16	16	9.95821	10.38181	0.55	44	16	9.95821	10.38181	0.55	44
17	0.10	0.10		17	17	9.95827	10.38184	0.55	43	17	9.95827	10.38184	0.55	43
18	0.10	0.10		18	18	9.95833	10.38187	0.55	42	18	9.95833	10.38187	0.55	42
19	0.10	0.10		19	19	9.95839	10.38190	0.55	41	19	9.95839	10.38190	0.55	41
20	0.10	0.10		20	20	9.95844	10.38193	0.55	40	20	9.95844	10.38193	0.55	40
21	0.10	0.10		21	21	9.95850	10.38196	0.55	39	21	9.95850	10.38196	0.55	39
22	0.10	0.10		22	22	9.95856	10.38199	0.55	38	22	9.95856	10.38199	0.55	38
23	0.10	0.10		23	23	9.95861	10.38202	0.55	37	23	9.95861	10.38202	0.55	37
24	0.10	0.10		24	24	9.95867	10.38205	0.55	36	24	9.95867	10.38205	0.55	36
25	0.10	0.10		25	25	9.95873	10.38208	0.55	35	25	9.95873	10.38208	0.55	35
26	0.10	0.10		26	26	9.95879	10.38211	0.55	34	26	9.95879	10.38211	0.55	34
27	0.10	0.10		27	27	9.95885	10.38214	0.55	33	27	9.95885	10.38214	0.55	33
28	0.10	0.10		28	28	9.95891	10.38217	0.55	32	28	9.95891	10.38217	0.55	32
29	0.10	0.10		29	29	9.95897	10.38220	0.55	31	29	9.95897	10.38220	0.55	31
30	0.10	0.10		30	30	9.95902	10.38223	0.55	30	30	9.95902	10.38223	0.55	30
31	0.10	0.10		31	31	9.95908	10.38226	0.55	29	31	9.95908	10.38226	0.55	29
32	0.10	0.10		32	32	9.95914	10.38229	0.55	28	32	9.95914	10.38229	0.55	28
33	0.10	0.10		33	33	9.95920	10.38232	0.55	27	33	9.95920	10.38232	0.55	27
34	0.10	0.10		34	34	9.95925	10.38235	0.55	26	34	9.95925	10.38235	0.55	26
35	0.10	0.10		35	35	9.95931	10.38238	0.55	25	35	9.95931	10.38238	0.55	25
36	0.10	0.10		36	36	9.95937	10.38241	0.55	24	36	9.95937	10.38241	0.55	24
37	0.10	0.10		37	37	9.95942	10.38244	0.55	23	37	9.95942	10.38244	0.55	23
38	0.10	0.10		38	38	9.95948	10.38247	0.55	22	38	9.95948	10.38247	0.55	22
39	0.10	0.10		39	39	9.95954	10.38250	0.55	21	39	9.95954	10.38250	0.55	21
40	0.10	0.10		40	40	9.95960	10.38253	0.55	20	40	9.95960	10.38253	0.55	20
41	0.10	0.10		41	41	9.95966	10.38256	0.55	19	41	9.95966	10.38256	0.55	19
42	0.10	0.10		42	42	9.95971	10.38259	0.55	18	42	9.95971	10.38259	0.55	18
43	0.10	0.10		43	43	9.95977	10.38262	0.55	17	43	9.95977	10.38262	0.55	17
44	0.10	0.10		44	44	9.95982	10.38265	0.55	16	44	9.95982	10.38265	0.55	16
45	0.10	0.10		45	45	9.95988	10.38268	0.55	15	45	9.95988	10.38268	0.55	15
46	0.10	0.10		46	46	9.95994	10.38271	0.55	14	46	9.95994	10.38271	0.55	14
47	0.10	0.10		47	47	9.95999	10.38274	0.55	13	47	9.95999	10.38274	0.55	13
48	0.10	0.10		48	48	9.96005	10.38277	0.55	12	48	9.96005	10.38277	0.55	12
49	0.10	0.10		49	49	9.96011	10.38280	0.55	11	49	9.96011	10.38280	0.55	11
50	0.10	0.10		50	50	9.96016	10.38283	0.55	10	50	9.96016	10.38283	0.55	10
51	0.10	0.10		51	51	9.96022	10.38286	0.55	9	51	9.96022	10.38286	0.55	9
52	0.10	0.10		52	52	9.96028	10.38289	0.55	8	52	9.96028	10.38289	0.55	8
53	0.10	0.10		53	53	9.96033	10.38292	0.55	7	53	9.96033	10.38292	0.55	7
54	0.10	0.10		54	54	9.96039	10.38295	0.55	6	54	9.96039	10.38295	0.55	6
55	0.10	0.10		55	55	9.96045	10.38298	0.55	5	55	9.96045	10.38298	0.55	5
56	0.10	0.10		56	56	9.96050	10.38301	0.55	4	56	9.96050	10.38301	0.55	4
57	0.10	0.10		57	57	9.96056	10.38304	0.55	3	57	9.96056	10.38304	0.55	3
58	0.10	0.10		58	58	9.96062	10.38307	0.55	2	58	9.96062	10.38307	0.55	2
59	0.10	0.10		59	59	9.96067	10.38310	0.55	1	59	9.96067	10.38310	0.55	1
60	0.10	0.10		60	60	9.96073	10.38313	0.55	0	60	9.96073	10.38313	0.55	0

M	Sec	Log	Diff	M	M	Sec	Log	Diff	M	M	Sec	Log	Diff	M
0	9.96103	0.09	10.38316	0.57	60	0	9.96103	0.09	10.38316	0.57	60	0	9.96103	0.09
1	9.96108	.09	3.210	.57	59	1	9.96108	.09	3.210	.57	59	1	9.96108	.09
2	9.96114	.09	3.214	.57	58	2	9.96114	.09	3.214	.57	58	2	9.96114	.09
3	9.96119	.09	3.218	.57	57	3	9.96119	.09	3.218	.57	57	3	9.96119	.09
4	9.96124	.09	3.222	.57	56	4	9.96124	.09	3.222	.57	56	4	9.96124	.09
5	9.96129	.09	3.226	.57	55	5	9.96129	.09	3.226	.57	55	5	9.96129	.09
6	9.96135	.09	3.230	.57	54	6	9.96135	.09	3.230	.57	54	6	9.96135	.09
7	9.96140	.09	3.234	.57	53	7	9.96140	.09	3.234	.57	53	7	9.96140	.09
8	9.96145	.09	3.238	.57	52	8	9.96145	.09	3.238	.57	52	8	9.96145	.09
9	9.96150	.09	3.242	.57	51	9	9.96150	.09	3.242	.57	51	9	9.96150	.09
10	9.96156	.09	3.246	.57	50	10	9.96156	.09	3.246	.57	50	10	9.96156	.09
11	9.96161	.09	3.250	.57	49	11	9.96161	.09	3.250	.57	49	11	9.96161	.09
12	9.96166	.09	3.254	.57	48	12	9.96166	.09	3.254	.57	48	12	9.96166	.09
13	9.96172	.09	3.258	.57	47	13	9.96172	.09	3.258	.57	47	13	9.96172	.09
14	9.96177	.09	3.262	.57	46	14	9.96177	.09	3.262	.57	46	14	9.96177	.09
15	9.96183	.09	3.266	.57	45	15	9.96183	.09	3.266	.57	45	15	9.96183	.09
16	9.96188	.09	3.270	.57	44	16	9.96188	.09	3.270	.57	44	16	9.96188	.09
17	9.96193	.09	3.274	.57	43	17	9.96193	.09	3.274	.57	43	17	9.96193	.09
18	9.96198	.09	3.278	.57	42	18	9.96198	.09	3.278	.57	42	18	9.96198	.09
19	9.96204	.09	3.282	.57	41	19	9.96204	.09	3.282	.57	41	19	9.96204	.09
20	9.96209	.09	3.286	.57	40	20	9.96209	.09	3.286	.57	40	20	9.96209	.09
21	9.96214	.09	3.290	.57	39	21	9.96214	.09	3.290	.57	39	21	9.96214	.09
22	9.96220	.09	3.294	.57	38	22	9.96220	.09	3.294	.57	38	22	9.96220	.09
23	9.96225	.09	3.298	.57	37	23	9.96225	.09	3.298	.57	37	23	9.96225	.09
24	9.96230	.09	3.302	.57	36	24	9.96230	.09	3.302	.57	36	24	9.96230	.09
25	9.96236	.09	3.306	.57	35	25	9.96236	.09	3.306	.57	35	25	9.96236	.09
26	9.96241	.09	3.310	.57	34	26	9.96241	.09	3.310	.57	34	26	9.96241	.09
27	9.96246	.09	3.314	.57	33	27	9.96246	.09	3.314	.57	33	27	9.96246	.09
28	9.96251	.09	3.318	.57	32	28	9.96251	.09	3.318	.57	32	28	9.96251	.09
29	9.96256	.09	3.322	.57	31	29	9.96256	.09	3.322	.57	31	29	9.96256	.09
30	9.96261	.09	3.326	.57	30	30	9.96261	.09	3.326	.57	30	30	9.96261	.09
31	9.96266	.09	3.330	.57	29	31	9.96266	.09	3.330	.57	29	31	9.96266	.09
32	9.96271	.09	3.334	.57	28	32	9.96271	.09	3.334	.57	28	32	9.96271	.09
33	9.96276	.09	3.338	.57	27	33	9.96276	.09	3.338	.57	27	33	9.96276	.09
34	9.96281	.09	3.342	.57	26	34	9.96281	.09	3.342	.57	26	34	9.96281	.09
35	9.96286	.09	3.346	.57	25	35	9.96286	.09	3.346	.57	25	35	9.96286	.09
36	9.96291	.09	3.350	.57	24	36	9.96291	.09	3.350	.57	24	36	9.96291	.09
37	9.96296	.09	3.354	.57	23	37	9.96296	.09	3.354	.57	23	37	9.96296	.09
38	9.96301	.09	3.358	.57	22	38	9.96301	.09	3.358	.57	22	38	9.96301	.09
39	9.96306	.09	3.362	.57	21	39	9.96306	.09	3.362	.57	21	39	9.96306	.09
40	9.96311	.09	3.366	.57	20	40	9.96311	.09	3.366	.57	20	40	9.96311	.09
41	9.96316	.09	3.370	.57	19	41	9.96316	.09	3.370	.57	19	41	9.96316	.09
42	9.96321	.09	3.374	.57	18	42	9.96321	.09	3.374	.57	18	42	9.96321	.09
43	9.96326	.09	3.378	.57	17	43	9.96326	.09	3.378	.57	17	43	9.96326	.09
44	9.96331	.09	3.382	.57	16	44	9.96331	.09	3.382	.57	16	44	9.96331	.09
45	9.96336	.09	3.386	.57	15	45	9.96336	.09	3.386	.57	15	45	9.96336	.09
46	9.96341	.09	3.390	.57	14	46	9.96341	.09	3.390	.57	14	46	9.96341	.09
47	9.96346	.09	3.394	.57	13	47	9.96346	.09	3.394	.57	13	47	9.96346	.09
48	9.96351	.09	3.398	.57	12	48	9.96351	.09	3.398	.57	12	48	9.96351	.09
49	9.96356	.09	3.402	.57	11	49	9.96356	.09	3.402	.57	11	49	9.96356	.09
50	9.96361	.09	3.406	.57	10	50	9.96361	.09	3.406	.57	10	50	9.96361	.09
51	9.96366	.09	3.410	.57	9	51	9.96366	.09	3.410	.57	9	51	9.96366	.09
52	9.96371	.09	3.414	.57	8	52	9.96371	.09	3.414	.57	8	52	9.96371	.09
53	9.96376	.09	3.418	.57	7	53	9.96376	.09	3.418	.57	7	53	9.96376	.09
54	9.96381	.09	3.422	.57	6	54	9.96381	.09	3.422	.57	6	54	9.96381	.09
55	9.96386	.09	3.426	.57	5	55	9.96386	.09	3.426	.57	5	55	9.96386	.09
56	9.96391	.09	3.430	.57	4	56	9.96391	.09	3.430	.57	4	56	9.96391	.09
57	9.96396	.09	3.434	.57	3	57	9.96396	.09	3.434	.57	3	57	9.96396	.09
58	9.96401	.09	3.438	.57	2	58	9.96401	.09	3.438	.57	2	58	9.96401	.09
59	9.96406	.09	3.442	.57	1	59	9.96406	.09	3.442	.57	1	59	9.96406	.09
60	9.96411	.09	3.446	.57	0	60	9.96411	.09	3.446	.57	0	60	9.96411	.09

[illegible]

0	1	2	3	4	5	6	7	8	9	0	1	2	3	4	5	6	7	8	9	0	1	2	3	4	5	6	7	8	9
0	8.97	2.22	10.4	2.22	10.4	2.22	10.4	2.22	10.4	0	8.97	2.22	10.4	2.22	10.4	2.22	10.4	2.22	10.4	0	8.97	2.22	10.4	2.22	10.4	2.22	10.4	2.22	10.4
1	9.00	2.23	10.4	2.23	10.4	2.23	10.4	2.23	10.4	1	9.00	2.23	10.4	2.23	10.4	2.23	10.4	2.23	10.4	1	9.00	2.23	10.4	2.23	10.4	2.23	10.4	2.23	10.4
2	9.03	2.24	10.4	2.24	10.4	2.24	10.4	2.24	10.4	2	9.03	2.24	10.4	2.24	10.4	2.24	10.4	2.24	10.4	2	9.03	2.24	10.4	2.24	10.4	2.24	10.4	2.24	10.4
3	9.06	2.25	10.4	2.25	10.4	2.25	10.4	2.25	10.4	3	9.06	2.25	10.4	2.25	10.4	2.25	10.4	2.25	10.4	3	9.06	2.25	10.4	2.25	10.4	2.25	10.4	2.25	10.4
4	9.09	2.26	10.4	2.26	10.4	2.26	10.4	2.26	10.4	4	9.09	2.26	10.4	2.26	10.4	2.26	10.4	2.26	10.4	4	9.09	2.26	10.4	2.26	10.4	2.26	10.4	2.26	10.4
5	9.12	2.27	10.4	2.27	10.4	2.27	10.4	2.27	10.4	5	9.12	2.27	10.4	2.27	10.4	2.27	10.4	2.27	10.4	5	9.12	2.27	10.4	2.27	10.4	2.27	10.4	2.27	10.4
6	9.15	2.28	10.4	2.28	10.4	2.28	10.4	2.28	10.4	6	9.15	2.28	10.4	2.28	10.4	2.28	10.4	2.28	10.4	6	9.15	2.28	10.4	2.28	10.4	2.28	10.4	2.28	10.4
7	9.18	2.29	10.4	2.29	10.4	2.29	10.4	2.29	10.4	7	9.18	2.29	10.4	2.29	10.4	2.29	10.4	2.29	10.4	7	9.18	2.29	10.4	2.29	10.4	2.29	10.4	2.29	10.4
8	9.21	2.30	10.4	2.30	10.4	2.30	10.4	2.30	10.4	8	9.21	2.30	10.4	2.30	10.4	2.30	10.4	2.30	10.4	8	9.21	2.30	10.4	2.30	10.4	2.30	10.4	2.30	10.4
9	9.24	2.31	10.4	2.31	10.4	2.31	10.4	2.31	10.4	9	9.24	2.31	10.4	2.31	10.4	2.31	10.4	2.31	10.4	9	9.24	2.31	10.4	2.31	10.4	2.31	10.4	2.31	10.4
10	9.27	2.32	10.4	2.32	10.4	2.32	10.4	2.32	10.4	10	9.27	2.32	10.4	2.32	10.4	2.32	10.4	2.32	10.4	10	9.27	2.32	10.4	2.32	10.4	2.32	10.4	2.32	10.4
11	9.30	2.33	10.4	2.33	10.4	2.33	10.4	2.33	10.4	11	9.30	2.33	10.4	2.33	10.4	2.33	10.4	2.33	10.4	11	9.30	2.33	10.4	2.33	10.4	2.33	10.4	2.33	10.4
12	9.33	2.34	10.4	2.34	10.4	2.34	10.4	2.34	10.4	12	9.33	2.34	10.4	2.34	10.4	2.34	10.4	2.34	10.4	12	9.33	2.34	10.4	2.34	10.4	2.34	10.4	2.34	10.4
13	9.36	2.35	10.4	2.35	10.4	2.35	10.4	2.35	10.4	13	9.36	2.35	10.4	2.35	10.4	2.35	10.4	2.35	10.4	13	9.36	2.35	10.4	2.35	10.4	2.35	10.4	2.35	10.4
14	9.39	2.36	10.4	2.36	10.4	2.36	10.4	2.36	10.4	14	9.39	2.36	10.4	2.36	10.4	2.36	10.												

[illegible]

31	800	100	1000	1000	31	800	100	1000	1000	31
0	98284	00	105120	00	0	98284	00	105120	00	0
1	98285	00	54298	00	1	98285	00	54298	00	1
2	98291	00	54348	00	2	98291	00	54348	00	2
3	98295	00	54394	00	3	98295	00	54394	00	3
4	98299	00	54441	00	4	98299	00	54497	00	4
5	98302	00	54489	00	5	98311	00	57448	00	5
6	98306	00	54537	00	6	98313	00	57509	00	6
7	98310	00	54585	00	7	98318	00	57550	00	7
8	98313	00	54633	00	8	98321	00	57601	00	8
9	98317	00	54681	00	9	98322	00	57652	00	9
10	98320	00	54729	00	10	98328	00	57702	00	10
11	98324	00	1054778	00	11	98333	00	1057701	00	11
12	98327	00	54826	00	12	98335	00	57803	00	12
13	98331	00	54874	00	13	98338	00	57856	00	13
14	98334	00	54922	00	14	98341	00	57907	00	14
15	98338	00	54970	00	15	98343	00	57959	00	15
16	98342	00	55018	00	16	98348	00	58010	00	16
17	98345	00	55067	00	17	98351	00	58061	00	17
18	98349	00	55115	00	18	98353	00	58112	00	18
19	98352	00	55164	00	19	98358	00	58164	00	19
20	98356	00	55213	00	20	98361	00	58216	00	20
21	98359	00	1055262	00	21	98362	00	1058262	00	21
22	98363	00	55310	00	22	98368	00	58319	00	22
23	98367	00	55359	00	23	98371	00	58371	00	23
24	98370	00	55408	00	24	98374	00	58422	00	24
25	98374	00	55456	00	25	98378	00	58474	00	25
26	98377	00	55505	00	26	98381	00	58526	00	26
27	98381	00	55554	00	27	98384	00	58578	00	27
28	98384	00	55603	00	28	98388	00	58630	00	28
29	98388	00	55652	00	29	98391	00	58682	00	29
30	98391	00	55701	00	30	98394	00	58734	00	30
31	98395	00	1055753	00	31	98397	00	1058786	00	31
32	98398	00	55799	00	32	98401	00	58839	00	32
33	98402	00	55849	00	33	98401	00	58891	00	33
34	98405	00	55898	00	34	98407	00	58943	00	34
35	98409	00	55947	00	35	98416	00	58995	00	35
36	98412	00	55996	00	36	98414	00	59048	00	36
37	98416	00	56046	00	37	98417	00	59100	00	37
38	98419	00	56095	00	38	98425	00	59153	00	38
39	98423	00	56145	00	39	98423	00	59205	00	39
40	98426	00	56194	00	40	98427	00	59258	00	40
41	98429	00	1056244	00	41	98430	00	1059311	00	41
42	98433	00	56293	00	42	98433	00	59364	00	42
43	98436	00	56343	00	43	98438	00	59416	00	43
44	98440	00	56393	00	44	98440	00	59469	00	44
45	98443	00	56442	00	45	98443	00	59522	00	45
46	98447	00	56492	00	46	98448	00	59574	00	46
47	98450	00	56542	00	47	98449	00	59628	00	47
48	98453	00	56592	00	48	98452	00	59681	00	48
49	98457	00	56642	00	49	98456	00	59734	00	49
50	98460	00	56692	00	50	98459	00	59788	00	50
51	98464	00	1056713	00	51	98462	00	1059841	00	51
52	98467	00	56742	00	52	98465	00	59834	00	52
53	98471	00	56792	00	53	98468	00	59888	00	53
54	98474	00	56842	00	54	98471	00	59941	00	54
55	98477	00	56892	00	55	98474	00	60000	00	55
56	98481	00	56942	00	56	98478	00	60058	00	56
57	98484	00	57043	00	57	98481	00	60162	00	57
58	98488	00	57094	00	58	98484	00	60215	00	58
59	98491	00	57144	00	59	98487	00	60269	00	59
60	98494	00	57195	00	60	98490	00	60323	00	60

[illegible]

M	Sec	Lat	Long	Alt	M	Sec	Lat	Long	Alt
0	9 20 10	0.01	10 87 2 3	1.04	0	9 20 10	0.04	10 7 1 3	1.13
1	9 20 11	0.01	87 31 1	1.04	1	9 20 11	0.04	7 12 2	1.13
2	9 20 12	0.01	87 37 7	1.04	2	9 20 12	0.01	7 12 0	1.13
3	9 20 13	0.01	87 43 9	1.04	3	9 20 13	0.01	7 13 8	1.13
4	9 20 14	0.01	87 49 2	1.04	4	9 20 14	0.01	7 14 0	1.13
5	9 20 15	0.01	87 55 4	1.04	5	9 20 15	0.01	7 14 3	1.13
6	9 20 16	0.01	87 52 7	1.04	6	9 20 16	0.01	7 15 4	1.13
7	9 20 17	0.01	87 58 9	1.04	7	9 20 17	0.01	7 16 1	1.13
8	9 20 18	0.01	87 55 2	1.05	8	9 20 18	0.01	7 16 7	1.14
9	9 20 19	0.01	87 51 5	1.05	9	9 20 19	0.01	7 17 10	1.14
10	9 20 20	0.01	87 47 8	1.05	10	9 20 20	0.01	7 18 4	1.14
11	9 20 21	0.01	87 44 1	1.05	11	9 20 21	0.01	7 18 8	1.14
12	9 20 22	0.01	87 40 4	1.05	12	9 20 22	0.01	7 19 1	1.14
13	9 20 23	0.01	87 36 7	1.05	13	9 20 23	0.01	7 20 20	1.15
14	9 20 24	0.01	87 33 0	1.06	14	9 20 24	0.01	7 20 8	1.15
15	9 20 25	0.01	87 29 3	1.06	15	9 20 25	0.01	7 21 58	1.15
16	9 20 26	0.01	87 25 6	1.06	16	9 20 26	0.01	7 22 27	1.15
17	9 20 27	0.01	87 21 9	1.06	17	9 20 27	0.01	7 22 57	1.15
18	9 20 28	0.01	87 18 2	1.06	18	9 20 28	0.01	7 23 26	1.15
19	9 20 29	0.01	87 14 5	1.06	19	9 20 29	0.01	7 23 55	1.16
20	9 20 30	0.01	87 10 8	1.06	20	9 20 30	0.01	7 24 24	1.16
21	9 20 31	0.01	10 86 5 3	1.07	21	9 20 31	0.01	10 7 2 3	1.16
22	9 20 32	0.01	86 7 0	1.07	22	9 20 32	0.01	7 24 53	1.16
23	9 20 33	0.01	86 7 03	1.07	23	9 20 33	0.01	7 25 12	1.16
24	9 20 34	0.01	86 7 07	1.07	24	9 20 34	0.01	7 25 42	1.17
25	9 20 35	0.01	86 6 12	1.07	25	9 20 35	0.01	7 26 12	1.17
26	9 20 36	0.01	86 5 20	1.07	26	9 20 36	0.01	7 26 42	1.17
27	9 20 37	0.01	86 4 30	1.07	27	9 20 37	0.01	7 27 12	1.17
28	9 20 38	0.01	86 3 40	1.08	28	9 20 38	0.01	7 27 42	1.17
29	9 20 39	0.01	86 2 50	1.08	29	9 20 39	0.01	7 28 12	1.18
30	9 20 40	0.01	86 2 00	1.08	30	9 20 40	0.01	7 28 42	1.18
31	9 20 41	0.01	10 86 2 18	1.08	31	9 20 41	0.01	10 7 2 18	1.18
32	9 20 42	0.01	86 2 31	1.08	32	9 20 42	0.01	7 29 12	1.18
33	9 20 43	0.01	86 2 40	1.08	33	9 20 43	0.01	7 29 42	1.18
34	9 20 44	0.01	86 2 49	1.08	34	9 20 44	0.01	7 30 12	1.18
35	9 20 45	0.01	86 2 58	1.08	35	9 20 45	0.01	7 30 42	1.19
36	9 20 46	0.01	86 3 07	1.09	36	9 20 46	0.01	7 31 12	1.19
37	9 20 47	0.01	86 3 16	1.09	37	9 20 47	0.01	7 31 42	1.19
38	9 20 48	0.01	86 3 25	1.09	38	9 20 48	0.01	7 32 12	1.19
39	9 20 49	0.01	86 3 34	1.09	39	9 20 49	0.01	7 32 42	1.19
40	9 20 50	0.01	86 3 43	1.09	40	9 20 50	0.01	7 33 12	1.19
41	9 20 51	0.01	10 86 3 0	1.10	41	9 20 51	0.01	10 7 3 0	1.19
42	9 20 52	0.01	86 3 09	1.10	42	9 20 52	0.01	7 33 42	1.20
43	9 20 53	0.01	86 3 18	1.10	43	9 20 53	0.01	7 34 12	1.20
44	9 20 54	0.01	86 3 27	1.10	44	9 20 54	0.01	7 34 42	1.20
45	9 20 55	0.01	86 3 36	1.10	45	9 20 55	0.01	7 35 12	1.20
46	9 20 56	0.01	86 3 45	1.10	46	9 20 56	0.01	7 35 42	1.21
47	9 20 57	0.01	86 3 54	1.10	47	9 20 57	0.01	7 36 12	1.21
48	9 20 58	0.01	86 4 03	1.10	48	9 20 58	0.01	7 36 42	1.21
49	9 20 59	0.01	86 4 12	1.11	49	9 20 59	0.01	7 37 12	1.21
50	9 21 00	0.01	86 4 21	1.11	50	9 21 00	0.01	7 37 42	1.21
51	9 21 01	0.01	86 4 30	1.11	51	9 21 01	0.01	7 38 12	1.22
52	9 21 02	0.01	86 4 39	1.11	52	9 21 02	0.01	7 38 42	1.22
53	9 21 03	0.01	86 4 48	1.11	53	9 21 03	0.01	7 39 12	1.22
54	9 21 04	0.01	86 4 57	1.11	54	9 21 04	0.01	7 39 42	1.22
55	9 21 05	0.01	86 5 06	1.12	55	9 21 05	0.01	7 40 12	1.22
56	9 21 06	0.01	86 5 15	1.12	56	9 21 06	0.01	7 40 42	1.22
57	9 21 07	0.01	86 5 24	1.12	57	9 21 07	0.01	7 41 12	1.22
58	9 21 08	0.01	86 5 33	1.12	58	9 21 08	0.01	7 41 42	1.22
59	9 21 09	0.01	86 5 42	1.12	59	9 21 09	0.01	7 42 12	1.22
60	9 21 10	0.01	86 5 51	1.12	60	9 21 10	0.01	7 42 42	1.22
M	Sec	Lat	Long	Alt	M	Sec	Lat	Long	Alt

M	Case	Dr	Collar	P	M	Case	Dr	Collar	P	M
0					0					0
1					1					1
2					2					2
3					3					3
4					4					4
5					5					5
6					6					6
7					7					7
8					8					8
9					9					9
10					10					10
11					11					11
12					12					12
13					13					13
14					14					14
15					15					15
16					16					16
17					17					17
18					18					18
19					19					19
20					20					20
21					21					21
22					22					22
23					23					23
24					24					24
25					25					25
26					26					26
27					27					27
28					28					28
29					29					29
30					30					30
31					31					31
32					32					32
33					33					33
34					34					34
35					35					35
36					36					36
37					37					37
38					38					38
39					39					39
40					40					40
41					41					41
42					42					42
43					43					43
44					44					44
45					45					45
46					46					46
47					47					47
48					48					48
49					49					49
50					50					50
51					51					51
52					52					52
53					53					53
54					54					54
55					55					55
56					56					56
57					57					57
58					58					58
59					59					59
60					60					60

M.	Surc	D ^r	Targ	D ^r	M	Surc	D ^r	Targ	D ^r	M
0	9 99 75		10.8 220		0	9 99 75		10.8 220		0
1	99577	0.03	85112	1.53	1	99577	0.03	85112	1.53	1
2	99579	.03	85454	1.54	2	99579	.03	85454	1.54	2
3	99581	.03	85456	1.54	3	99581	.03	85456	1.54	3
4	99582	.03	85588	1.54	4	99582	.03	85588	1.54	4
5	99584	.03	85680	1.55	5	99584	.03	85680	1.55	5
6	99586	.03	85773	1.55	6	99586	.03	85773	1.55	6
7	99588	.03	85866	1.55	7	99588	.03	85866	1.55	7
8	99589	.03	85959	1.55	8	99589	.03	85959	1.55	8
9	99591	.03	86052	1.56	9	99591	.03	86052	1.56	9
10	99593	.03	86146	1.56	10	99593	.03	86146	1.56	10
11	99595	.03	10.86239	1.56	11	99595	.03	10.86239	1.56	11
12	99597	.03	86333	1.57	12	99597	.03	86333	1.57	12
13	99599	.03	86427	1.57	13	99599	.03	86427	1.57	13
14	99601	.03	86522	1.57	14	99601	.03	86522	1.57	14
15	99603	.03	86616	1.57	15	99603	.03	86616	1.57	15
16	99605	.03	86711	1.58	16	99605	.03	86711	1.58	16
17	99607	.03	86806	1.58	17	99607	.03	86806	1.58	17
18	99609	.03	86901	1.59	18	99609	.03	86901	1.59	18
19	99611	.03	86996	1.59	19	99611	.03	86996	1.59	19
20	99613	.03	87091	1.59	20	99613	.03	87091	1.59	20
21	99615	.03	87187	1.60	21	99615	.03	87187	1.60	21
22	99617	.03	87283	1.60	22	99617	.03	87283	1.60	22
23	99619	.03	87379	1.60	23	99619	.03	87379	1.60	23
24	99621	.03	87475	1.61	24	99621	.03	87475	1.61	24
25	99623	.03	87572	1.61	25	99623	.03	87572	1.61	25
26	99625	.03	87668	1.61	26	99625	.03	87668	1.61	26
27	99627	.03	87765	1.62	27	99627	.03	87765	1.62	27
28	99629	.03	87862	1.62	28	99629	.03	87862	1.62	28
29	99631	.03	87960	1.61	29	99631	.03	87960	1.61	29
30	99633	.03	88057	1.61	30	99633	.03	88057	1.61	30
31	99635	.03	10.88155	1.61	31	99635	.03	10.88155	1.61	31
32	99637	.03	88253	1.61	32	99637	.03	88253	1.61	32
33	99639	.03	88351	1.61	33	99639	.03	88351	1.61	33
34	99641	.03	88449	1.61	34	99641	.03	88449	1.61	34
35	99643	.03	88548	1.61	35	99643	.03	88548	1.61	35
36	99645	.03	88647	1.61	36	99645	.03	88647	1.61	36
37	99647	.03	88746	1.61	37	99647	.03	88746	1.61	37
38	99649	.03	88845	1.61	38	99649	.03	88845	1.61	38
39	99651	.03	88944	1.61	39	99651	.03	88944	1.61	39
40	99653	.03	89043	1.61	40	99653	.03	89043	1.61	40</

M	Sec	Diff	Tang	Diff	M
0	9.99991	0.01	11.15	6	60
1	9.99992	0.01	15.18	3.03	59
2	9.99993	0.01	19.20	3.04	58
3	9.99994	0.01	23.24	3.06	57
4	9.99995	0.01	27.28	3.07	56
5	9.99996	0.01	31.33	3.08	55
6	9.99997	0.01	35.38	3.11	54
7	9.99998	0.01	39.43	3.11	53
8	9.99999	0.01	43.48	3.12	52
9	10.00000	0.01	47.53	3.14	51
10	10.00001	0.01	51.58	3.15	50
11	10.00002	0.01	55.63	3.16	49
12	10.00003	0.01	59.68	3.18	48
13	10.00004	0.01	63.73	3.19	47
14	10.00005	0.01	67.78	3.21	46
15	10.00006	0.01	71.83	3.22	45
16	10.00007	0.01	75.88	3.23	44
17	10.00008	0.01	79.93	3.24	43
18	10.00009	0.01	83.98	3.26	42
19	10.00010	0.01	88.03	3.28	41
20	10.00011	0.01	92.08	3.29	40
21	10.00012	0.01	96.13	3.31	39
22	10.00013	0.01	100.18	3.32	38
23	10.00014	0.01	104.23	3.34	37
24	10.00015	0.01	108.28	3.35	36
25	10.00016	0.01	112.33	3.37	35
26	10.00017	0.01	116.38	3.38	34
27	10.00018	0.01	120.43	3.39	33
28	10.00019	0.01	124.48	3.41	32
29	10.00020	0.01	128.53	3.41	31
30	10.00021	0.01	132.58	3.43	30
31	10.00022	0.01	136.63	3.45	29
32	10.00023	0.01	140.68	3.48	28
33	10.00024	0.01	144.73	3.50	27
34	10.00025	0.01	148.78	3.51	26
35	10.00026	0.01	152.83	3.53	25
36	10.00027	0.01	156.88	3.55	24
37	10.00028	0.01	160.93	3.57	23
38	10.00029	0.01	164.98	3.58	22
39	10.00030	0.01	169.03	3.60	21
40	10.00031	0.01	173.08	3.62	20
41	10.00032	0.01	177.13	3.64	19
42	10.00033	0.01	181.18	3.65	18
43	10.00034	0.01	185.23	3.68	17
44	10.00035	0.01	189.28	3.69	16
45	10.00036	0.01	193.33	3.71	15
46	10.00037	0.01	197.38	3.73	14
47	10.00038	0.01	201.43	3.75	13
48	10.00039	0.01	205.48	3.77	12
49	10.00040	0.01	209.53	3.79	11
50	10.00041	0.01	213.58	3.81	10
51	10.00042	0.01	217.63	3.83	9
52	10.00043	0.01	221.68	3.85	8
53	10.00044	0.01	225.73	3.87	7
54	10.00045	0.01	229.78	3.89	6
55	10.00046	0.01	233.83	3.91	5
56	10.00047	0.01	237.88	3.93	4
57	10.00048	0.01	241.93	3.95	3
58	10.00049	0.01	245.98	3.97	2
59	10.00050	0.01	250.03	3.99	1
60	10.00051	0.01	254.08	4.02	0

M	Sec	Diff	Tang	Diff	M
0	9.99991	0.01	11.15	6	60
1	9.99992	0.01	15.18	3.03	59
2	9.99993	0.01	19.20	3.04	58
3	9.99994	0.01	23.24	3.06	57
4	9.99995	0.01	27.28	3.07	56
5	9.99996	0.01	31.33	3.08	55
6	9.99997	0.01	35.38	3.11	54
7	9.99998	0.01	39.43	3.11	53
8	9.99999	0.01	43.48	3.12	52
9	10.00000	0.01	47.53	3.14	51
10	10.00001	0.01	51.58	3.15	50
11	10.00002	0.01	55.63	3.16	49
12	10.00003	0.01	59.68	3.18	48
13	10.00004	0.01	63.73	3.19	47
14	10.00005	0.01	67.78	3.21	46
15	10.00006	0.01	71.83	3.22	45
16	10.00007	0.01	75.88	3.23	44
17	10.00008	0.01	79.93	3.24	43
18	10.00009	0.01	83.98	3.26	42
19	10.00010	0.01	88.03	3.28	41
20	10.00011	0.01	92.08	3.29	40
21	10.00012	0.01	96.13	3.31	39
22	10.00013	0.01	100.18	3.32	38
23	10.00014	0.01	104.23	3.34	37
24	10.00015	0.01	108.28	3.35	36
25	10.00016	0.01	112.33	3.37	35
26	10.00017	0.01	116.38	3.38	34
27	10.00018	0.01	120.43	3.39	33
28	10.00019	0.01	124.48	3.41	32
29	10.00020	0.01	128.53	3.41	31
30	10.00021	0.01	132.58	3.43	30
31	10.00022	0.01	136.63	3.45	29
32	10.00023	0.01	140.68	3.48	28
33	10.00024	0.01	144.73	3.50	27
34	10.00025	0.01	148.78	3.51	26
35	10.00026	0.01	152.83	3.53	25
36	10.00027	0.01	156.88	3.55	24
37	10.00028	0.01	160.93	3.57	23
38	10.00029	0.01	164.98	3.58	22
39	10.00030	0.01	169.03	3.60	21
40	10.00031	0.01	173.08	3.62	20
41	10.00032	0.01	177.13	3.64	19
42	10.00033	0.01	181.18	3.65	18
43	10.00034	0.01	185.23	3.68	17
44	10.00035	0.01	189.28	3.69	16
45	10.00036	0.01	193.33	3.71	15
46	10.00037	0.01	197.38	3.73	14
47	10.00038	0.01	201.43	3.75	13
48	10.00039	0.01	205.48	3.77	12
49	10.00040	0.01	209.53	3.79	11
50	10.00041	0.01	213.58	3.81	10
51	10.00042	0.01	217.63	3.83	9
52	10.00043	0.01	221.68	3.85	8
53	10.00044	0.01	225.73	3.87	7
54	10.00045	0.01	229.78	3.89	6
55	10.00046	0.01	233.83	3.91	5
56	10.00047	0.01	237.88	3.93	4
57	10.00048	0.01	241.93	3.95	3
58	10.00049	0.01	245.98	3.97	2
59	10.00050	0.01	250.03	3.99	1
60	10.00051	0.01	254.08	4.02	0

Sin	Tan	Cotang.	Sec	Cosec	Sin	Tan	Cotang.	Sec	Cosec
1	0.017	57.735	1.000	1.000	1	0.017	57.735	1.000	1.000
2	0.034	29.100	1.000	0.999	2	0.034	29.100	1.000	0.999
3	0.051	19.081	1.000	0.998	3	0.051	19.081	1.000	0.998
4	0.069	14.301	1.000	0.997	4	0.069	14.301	1.000	0.997
5	0.087	11.474	1.000	0.996	5	0.087	11.474	1.000	0.996
6	0.104	9.515	1.000	0.995	6	0.104	9.515	1.000	0.995
7	0.122	8.017	1.000	0.994	7	0.122	8.017	1.000	0.994
8	0.139	6.913	1.000	0.993	8	0.139	6.913	1.000	0.993
9	0.156	6.009	1.000	0.992	9	0.156	6.009	1.000	0.992
10	0.174	5.317	1.000	0.991	10	0.174	5.317	1.000	0.991
11	0.191	4.754	1.000	0.990	11	0.191	4.754	1.000	0.990
12	0.208	4.286	1.000	0.989	12	0.208	4.286	1.000	0.989
13	0.225	3.883	1.000	0.988	13	0.225	3.883	1.000	0.988
14	0.242	3.542	1.000	0.987	14	0.242	3.542	1.000	0.987
15	0.259	3.258	1.000	0.986	15	0.259	3.258	1.000	0.986
16	0.276	3.027	1.000	0.985	16	0.276	3.027	1.000	0.985
17	0.293	2.842	1.000	0.984	17	0.293	2.842	1.000	0.984
18	0.310	2.698	1.000	0.983	18	0.310	2.698	1.000	0.983
19	0.327	2.589	1.000	0.982	19	0.327	2.589	1.000	0.982
20	0.344	2.509	1.000	0.981	20	0.344	2.509	1.000	0.981
21	0.361	2.453	1.000	0.980	21	0.361	2.453	1.000	0.980
22	0.378	2.416	1.000	0.979	22	0.378	2.416	1.000	0.979
23	0.395	2.394	1.000	0.978	23	0.395	2.394	1.000	0.978
24	0.412	2.384	1.000	0.977	24	0.412	2.384	1.000	0.977
25	0.429	2.384	1.000	0.976	25	0.429	2.384	1.000	0.976
26	0.446	2.394	1.000	0.975	26	0.446	2.394	1.000	0.975
27	0.463	2.416	1.000	0.974	27	0.463	2.416	1.000	0.974
28	0.480	2.453	1.000	0.973	28	0.480	2.453	1.000	0.973
29	0.497	2.509	1.000	0.972	29	0.497	2.509	1.000	0.972
30	0.514	2.589	1.000	0.971	30	0.514	2.589	1.000	0.971
31	0.531	2.698	1.000	0.970	31	0.531	2.698	1.000	0.970
32	0.548	2.842	1.000	0.969	32	0.548	2.842	1.000	0.969
33	0.565	3.027	1.000	0.968	33	0.565	3.027	1.000	0.968
34	0.582	3.258	1.000	0.967	34	0.582	3.258	1.000	0.967
35	0.599	3.542	1.000	0.966	35	0.599	3.542	1.000	0.966
36	0.616	3.883	1.000	0.965	36	0.616	3.883	1.000	0.965
37	0.633	4.286	1.000	0.964	37	0.633	4.286	1.000	0.964
38	0.650	4.754	1.000	0.963	38	0.650	4.754	1.000	0.963
39	0.667	5.317	1.000	0.962	39	0.667	5.317	1.000	0.962
40	0.684	5.988	1.000	0.961	40	0.684	5.988	1.000	0.961
41	0.701	6.781	1.000	0.960	41	0.701	6.781	1.000	0.960
42	0.718	7.718	1.000	0.959	42	0.718	7.718	1.000	0.959
43	0.735	8.834	1.000	0.958	43	0.735	8.834	1.000	0.958
44	0.752	10.167	1.000	0.957	44	0.752	10.167	1.000	0.957
45	0.769	11.770	1.000	0.956	45	0.769	11.770	1.000	0.956
46	0.786	13.707	1.000	0.955	46	0.786	13.707	1.000	0.955
47	0.803	16.047	1.000	0.954	47	0.803	16.047	1.000	0.954
48	0.820	18.959	1.000	0.953	48	0.820	18.959	1.000	0.953
49	0.837	22.629	1.000	0.952	49	0.837	22.629	1.000	0.952
50	0.854	27.475	1.000	0.951	50	0.854	27.475	1.000	0.951
51	0.871	34.076	1.000	0.950	51	0.871	34.076	1.000	0.950
52	0.888	43.281	1.000	0.949	52	0.888	43.281	1.000	0.949
53	0.905	56.713	1.000	0.948	53	0.905	56.713	1.000	0.948
54	0.922	76.604	1.000	0.947	54	0.922	76.604	1.000	0.947
55	0.939	106.580	1.000	0.946	55	0.939	106.580	1.000	0.946
56	0.956	149.542	1.000	0.945	56	0.956	149.542	1.000	0.945
57	0.973	209.585	1.000	0.944	57	0.973	209.585	1.000	0.944
58	0.990	300.000	1.000	0.943	58	0.990	300.000	1.000	0.943
59	1.007	433.284	1.000	0.942	59	1.007	433.284	1.000	0.942
60	1.024	636.396	1.000	0.941	60	1.024	636.396	1.000	0.941
61	1.041	933.267	1.000	0.940	61	1.041	933.267	1.000	0.940
62	1.058	1360.000	1.000	0.939	62	1.058	1360.000	1.000	0.939
63	1.075	1960.000	1.000	0.938	63	1.075	1960.000	1.000	0.938
64	1.092	2812.000	1.000	0.937	64	1.092	2812.000	1.000	0.937
65	1.109	3996.000	1.000	0.936	65	1.109	3996.000	1.000	0.936
66	1.126	5600.000	1.000	0.935	66	1.126	5600.000	1.000	0.935
67	1.143	7752.000	1.000	0.934	67	1.143	7752.000	1.000	0.934
68	1.160	10700.000	1.000	0.933	68	1.160	10700.000	1.000	0.933
69	1.177	14700.000	1.000	0.932	69	1.177	14700.000	1.000	0.932
70	1.194	20000.000	1.000	0.931	70	1.194	20000.000	1.000	0.931
71	1.211	27000.000	1.000	0.930	71	1.211	27000.000	1.000	0.930
72	1.228	36300.000	1.000	0.929	72	1.228	36300.000	1.000	0.929
73	1.245	48500.000	1.000	0.928	73	1.245	48500.000	1.000	0.928
74	1.262	64300.000	1.000	0.927	74	1.262	64300.000	1.000	0.927
75	1.279	84500.000	1.000	0.926	75	1.279	84500.000	1.000	0.926
76	1.296	110000.000	1.000	0.925	76	1.296	110000.000	1.000	0.925
77	1.313	142000.000	1.000	0.924	77	1.313	142000.000	1.000	0.924
78	1.330	182000.000	1.000	0.923	78	1.330	182000.000	1.000	0.923
79	1.347	232000.000	1.000	0.922	79	1.347	232000.000	1.000	0.922
80	1.364	296000.000	1.000	0.921	80	1.364	296000.000	1.000	0.921
81	1.381	380000.000	1.000	0.920	81	1.381	380000.000	1.000	0.920
82	1.398	492000.000	1.000	0.919	82	1.398	492000.000	1.000	0.919
83	1.415	640000.000	1.000	0.918	83	1.415	640000.000	1.000	0.918
84	1.432	836000.000	1.000	0.917	84	1.432	836000.000	1.000	0.917
85	1.449	1084000.000	1.000	0.916	85	1.449	1084000.000	1.000	0.916
86	1.466	1399000.000	1.000	0.915	86	1.466	1399000.000	1.000	0.915
87	1.483	1796000.000	1.000	0.914	87	1.483	1796000.000	1.000	0.914
88	1.500	2300000.000	1.000	0.913	88	1.500	2300000.000	1.000	0.913
89	1.517	2940000.000	1.000	0.912	89	1.517	2940000.000	1.000	0.912
90	1.534	3760000.000	1.000	0.911	90	1.534	3760000.000	1.000	0.911
91	1.551	4810000.000	1.000	0.910	91	1.551	4810000.000	1.000	0.910
92	1.568	6150000.000	1.000	0.909	92	1.568	6150000.000	1.000	0.909
93	1.585	7840000.000	1.000	0.908	93	1.585	7840000.000	1.000	0.908
94	1.602	9950000.000	1.000	0.907	94	1.602	9950000.000	1.000	0.907
95	1.619	12660000.000	1.000	0.906	95	1.619	12660000.000	1.000	0.906
96	1.636	16160000.000	1.000	0.905	96	1.636	16160000.000	1.000	0.905
97	1.653	20660000.000	1.000	0.904	97	1.653	20660000.000	1.000	0.904
98	1.670	26460000.000	1.000	0.903	98	1.670	26460000.000	1.000	0.903
99	1.687	33960000.000	1.000	0.902	99	1.687	33960000.000	1.000	0.902
100	1.704	43760000.000	1.000	0.901	100	1.704	43760000.000	1.000	0.901
101	1.721	56560000.000	1.000	0.900	101	1.721	56560000.000	1.000	0.900
102	1.738	73060000.000	1.000	0.899	102	1.738	73060000.000	1.000	0.899
103	1.755	94060000.000	1.000	0.898	103	1.755	94060000.000	1.000	0.898
104	1.772	120460000.000	1.000	0.897	104	1.772	120460000.000	1.000	0.897
105	1.789	153260000.000	1.000	0.896	105	1.789	153260000.000	1.000	0.896
106	1.806	194460000.000	1.000	0.895	106	1.806	194460000.000	1.000	0.895
107	1.823	245060000.000	1.000	0.894	107	1.823	245060000.000	1.000	0.894
108	1.840	307060000.000	1.000	0.893	108	1.840	307060000.000	1.000	0.893
109	1.857	382460000.000	1.000	0.892	109	1.857	382460000.000	1.000	0.892
110	1.874	473460000.000	1.000	0.891	110	1.874	473460000.000	1.000	0.891
111	1.891	582460000.000	1.000	0.890	111	1.891	582460000.000	1.000	0.890
112	1.908	712460000.000	1.000	0.889	112	1.908	712460000.000	1.000	0.889
113	1.925	867460000.000	1.000	0.888	113	1.925	867460000.000	1.000	0.888
114	1.942	1052460000.000	1.000	0.887	114	1.942	1052460000.000	1.000	0.887
115	1.959	1272460000.000	1.000	0.886	115	1.959	1272460000.000	1	

D	Lat	Dep	Lat	Dep	Lat	Dep	Lat	Dep	D
4 0			4 15		4 30		4 45		
1	1000	100	1000	100	1000	100	1000	100	1
2	1001	101	1001	101	1001	101	1001	101	2
3	1002	102	1002	102	1002	102	1002	102	3
4	1003	103	1003	103	1003	103	1003	103	4
5	1004	104	1004	104	1004	104	1004	104	5
6	1005	105	1005	105	1005	105	1005	105	6
7	1006	106	1006	106	1006	106	1006	106	7
8	1007	107	1007	107	1007	107	1007	107	8
9	1008	108	1008	108	1008	108	1008	108	9
10	1009	109	1009	109	1009	109	1009	109	10
5 0			5 15		5 30		5 45		
1	1010	110	1010	110	1010	110	1010	110	1
2	1011	111	1011	111	1011	111	1011	111	2
3	1012	112	1012	112	1012	112	1012	112	3
4	1013	113	1013	113	1013	113	1013	113	4
5	1014	114	1014	114	1014	114	1014	114	5
6	1015	115	1015	115	1015	115	1015	115	6
7	1016	116	1016	116	1016	116	1016	116	7
8	1017	117	1017	117	1017	117	1017	117	8
9	1018	118	1018	118	1018	118	1018	118	9
10	1019	119	1019	119	1019	119	1019	119	10
6 0			6 15		6 30		6 45		
1	1020	120	1020	120	1020	120	1020	120	1
2	1021	121	1021	121	1021	121	1021	121	2
3	1022	122	1022	122	1022	122	1022	122	3
4	1023	123	1023	123	1023	123	1023	123	4
5	1024	124	1024	124	1024	124	1024	124	5
6	1025	125	1025	125	1025	125	1025	125	6
7	1026	126	1026	126	1026	126	1026	126	7
8	1027	127	1027	127	1027	127	1027	127	8
9	1028	128	1028	128	1028	128	1028	128	9
10	1029	129	1029	129	1029	129	1029	129	10
7 0			7 15		7 30		7 45		
1	1030	130	1030	130	1030	130	1030	130	1
2	1031	131	1031	131	1031	131	1031	131	2
3	1032	132	1032	132	1032	132	1032	132	3
4	1033	133	1033	133	1033	133	1033	133	4
5	1034	134	1034	134	1034	134	1034	134	5
6	1035	135	1035	135	1035	135	1035	135	6
7	1036	136	1036	136	1036	136	1036	136	7
8	1037	137	1037	137	1037	137	1037	137	8
9	1038	138	1038	138	1038	138	1038	138	9
10	1039	139	1039	139	1039	139	1039	139	10
8 0			8 15		8 30		8 45		
1	1040	140	1040	140	1040	140	1040	140	1
2	1041	141	1041	141	1041	141	1041	141	2
3	1042	142	1042	142	1042	142	1042	142	3
4	1043	143	1043	143	1043	143	1043	143	4
5	1044	144	1044	144	1044	144	1044	144	5
6	1045	145	1045	145	1045	145	1045	145	6
7	1046	146	1046	146	1046	146	1046	146	7
8	1047	147	1047	147	1047	147	1047	147	8
9	1048	148	1048	148	1048	148	1048	148	9
10	1049	149	1049	149	1049	149	1049	149	10
9 0			9 15		9 30		9 45		
1	1050	150	1050	150	1050	150	1050	150	1
2	1051	151	1051	151	1051	151	1051	151	2
3	1052	152	1052	152	1052	152	1052	152	3
4	1053	153	1053	153	1053	153	1053	153	4
5	1054	154	1054	154	1054	154	1054	154	5
6	1055	155	1055	155	1055	155	1055	155	6
7	1056	156	1056	156	1056	156	1056	156	7
8	1057	157	1057	157	1057	157	1057	157	8
9	1058	158	1058	158	1058	158	1058	158	9
10	1059	159	1059	159	1059	159	1059	159	10
10 0			10 15		10 30		10 45		
1	1100	160	1100	160	1100	160	1100	160	1
2	1101	161	1101	161	1101	161	1101	161	2
3	1102	162	1102	162	1102	162	1102	162	3
4	1103	163	1103	163	1103	163	1103	163	4
5	1104	164	1104	164	1104	164	1104	164	5
6	1105	165	1105	165	1105	165	1105	165	6
7	1106	166	1106	166	1106	166	1106	166	7
8	1107	167	1107	167	1107	167	1107	167	8
9	1108	168	1108	168	1108	168	1108	168	9
10	1109	169	1109	169	1109	169	1109	169	10
11 0			11 15		11 30		11 45		
1	1110	170	1110	170	1110	170	1110	170	1
2	1111	171	1111	171	1111	171	1111	171	2
3	1112	172	1112	172	1112	172	1112	172	3
4	1113	173	1113	173	1113	173	1113	173	4
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6	1115	175	1115	175	1115	175	1115	175	6
7	1116	176	1116	176	1116	176	1116	176	7
8	1117	177	1117	177	1117	177	1117	177	8
9	1118	178	1118	178	1118	178	1118	178	9
10	1119	179	1119	179	1119	179	1119	179	10
12 0			12 15		12 30		12 45		
1	1120	180	1120	180	1120	180	1120	180	1
2	1121	181	1121	181	1121	181	1121	181	2
3	1122	182	1122	182	1122	182	1122	182	3
4	1123	183	1123	183	1123	183	1123	183	4
5	1124	184	1124	184	1124	184	1124	184	5
6	1125	185	1125	185	1125	185	1125	185	6
7	1126	186	1126	186	1126	186	1126	186	7
8	1127	187	1127	187	1127	187	1127	187	8
9	1128	188	1128	188	1128	188	1128	188	9
10	1129	189	1129	189	1129	189	1129	189	10
1 0			1 15		1 30		1 45		
1	1130	190	1130	190	1130	190	1130	190	1
2	1131	191	1131	191	1131	191	1131	191	2
3	1132	192	1132	192	1132	192	1132	192	3
4	1133	193	1133	193	1133	193	1133	193	4
5	1134	194	1134	194	1134	194	1134	194	5
6	1135	195	1135	195	1135	195	1135	195	6
7	1136	196	1136	196	1136	196	1136	196	7
8	1137	197	1137	197	1137	197	1137	197	8
9	1138	198	1138	198	1138	198	1138	198	9
10	1139	199	1139	199	1139	199	1139	199	10
2 0			2 15		2 30		2 45		
1	1140	200	1140	200	1140	200	1140	200	1
2	1141	201	1141	201	1141	201	1141	201	2
3	1142	202	1142	202	1142	202	1142	202	3
4	1143	203	1143	203	1143	203	1143	203	4
5	1144	204	1144	204	1144	204	1144	204	5
6	1145	205	1145	205	1145	205	1145	205	6
7	1146	206	1146	206	1146	206	1146	206	7
8	1147	207	1147	207	1147	207	1147	207	8
9	1148	208	1148	208	1148	208	1148	208	9
10	1149	209	1149	209	1149	209	1149	209	10
3 0			3 15		3 30		3 45		
1	1150	210	1150	210	1150	210	1150	210	1
2	1151	211	1151	211	1151	211	1151	211	2
3	1152	212	1152	212	1152	212	1152	212	3
4	1153	213	1153	213	1153	213	1153	213	4
5	1154	214	1154	214	1154	214	1154	214	5
6	1155	215	1155	215	1155	215	1155	215	6
7	1156	216	1156	216	1156	216	1156	216	7
8	1157	217	1157	217	1157	217	1157	217	8
9	1158	218	1158	218	1158	218	1158	218	9
10	1159	219	1159	219	1159	219	1159	219	10
4 0			4 15		4 30		4 45		
1	1200	220	1200	220	1200	220	1200	220	1
2	1201	221	1201	221	1201	221	1201	221	2
3	1202	222	1202	222	1202	222	1202	222	3
4	1203	223	1203	223	1203	223	1203	223	4
5	1204	224	1204	224	1204	224	1204	224	5
6	1205	225	1205	225	1205	225	1205	225	6
7	1206	226	1206	226	1206	226	1206	226	7
8	1207	227	1207	227	1207	227	1207	227	8
9	1208	228	1208	228	1208	228	1208	228	9
10	1209	229	1209	229	1209	229	1209	229	10
5 0			5 15		5 30		5 45		
1	1210	230	1210	230	1210	230	1210	230	1
2	1211	231	1211	231	1211	231	1211	231	2
3	1212	232	1212	232	1212	232	1212	232	3
4	1213	233	1213	233	1213	233	1213	233	4
5	1214	234	1214	234	1214	234	1214	234	5
6	1215	235	1215	235	1215	235	1215	235	6
7	1216	236	1216	236	1216	236	1216	236	7

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
	N	0'	N	15'	N	30'	N	45'	
1	990	139	990	143	981	148	988	152	1
2	1981	278	1979	287	1978	296	1977	304	2
3	2971	418	2969	431	2967	443	2965	456	3
4	3961	557	3959	574	3956	591	3953	608	4
5	4951	696	4948	717	4945	739	4942	761	5
6	5942	835	5938	861	5934	887	5930	914	6
7	6932	974	6928	1004	6923	1035	6919	1065	7
8	7922	1113	7917	1148	7912	1182	7907	1217	8
9	8912	1251	8907	1291	8901	1330	8895	1369	9
10	9902	1392	9897	1435	9890	1478	9884	1521	10
	82	0	81	45'	81	30'	81	15'	
	9	0	9	15'	9	30'	9	45'	
1	9881	156	987	161	986	165	986	169	1
2	1975	313	1974	321	1973	330	1971	339	2
3	2965	460	2961	482	2959	495	2957	508	3
4	3951	626	3948	647	3945	660	3942	677	4
5	4938	782	4933	804	4931	825	4928	847	5
6	5926	939	5922	964	5918	990	5914	1019	6
7	6914	1095	6909	1125	6904	1155	6899	1185	7
8	7902	1251	7896	1286	7890	1320	7884	1355	8
9	8889	1408	8881	1447	8877	1485	8870	1524	9
10	9877	1564	9871	1607	9865	1650	9860	1694	10
	81	0'	80	45'	80	30'	80	15'	
	10	0'	10	15'	10	30'	10	45'	
1	985	171	984	178	983	182	982	187	1
2	1979	347	1968	356	1967	364	1965	373	2
3	2971	521	2962	534	2959	547	2947	560	3
4	3969	695	3966	712	3963	729	3959	746	4
5	4954	868	4950	891	4946	911	4942	935	5
6	5940	1042	5934	1068	5930	1093	5925	1119	6
7	6924	1216	6918	1246	6913	1276	6907	1306	7
8	7908	1389	7902	1424	7896	1458	7890	1492	8
9	8892	1561	8886	1601	8879	1640	8872	1679	9
10	9878	1736	9870	1779	9863	1822	9855	1865	10
	80	0	79	45'	79	30'	79	15'	
	11	0'	11	15'	11	30'	11	45'	
1	982	191	981	195	980	199	979	204	1
2	1975	382	1962	390	1960	399	1958	407	2
3	2945	572	2942	585	2940	598	2937	611	3
4	3925	763	3923	780	3920	797	3916	815	4
5	4908	954	4904	976	4901	997	4895	1018	5
6	5890	1145	5885	1171	5880	1196	5874	1222	6
7	6871	1336	6866	1366	6860	1396	6853	1426	7
8	7853	1526	7846	1561	7839	1591	7832	1629	8
9	8835	1717	8827	1756	8820	1794	8811	1833	9
10	9816	1908	9808	1951	9799	1994	9790	2036	10
	79	0'	78	45'	78	30'	78	15'	
D.	Dep.	Lat.	D.	Dep.	Lat.	D.	Dep.	Lat.	D.

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
12 0	12 15	12 30	12 45	12 0	12 15	12 30	12 45	12 0	12 15
1	12 0	2 12	12 15	2 21	12 30	2 30	12 45	2 39	1
2	12 15	4 24	12 30	4 41	12 45	4 51	1 00	4 59	2
3	12 30	6 36	12 45	6 57	1 00	7 00	1 15	7 09	3
4	12 45	8 48	1 00	8 57	1 15	9 06	1 30	9 15	4
5	1 00	1 06	1 30	1 10	1 45	1 18	1 55	1 27	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
78 0	77 45	77 30	77 15	78 0	77 45	77 30	77 15	78 0	77 45
13 0	13 15	13 30	13 45	13 0	13 15	13 30	13 45	13 0	13 15
1	13 0	2 21	13 15	2 30	13 30	2 39	13 45	2 48	1
2	13 15	4 42	13 30	4 51	13 45	5 00	1 00	5 09	2
3	13 30	6 54	13 45	7 03	1 00	7 12	1 15	7 21	3
4	13 45	9 06	1 00	9 15	1 15	9 24	1 30	9 33	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
77 0	76 45	76 30	76 15	77 0	76 45	76 30	76 15	77 0	76 45
14 0	14 15	14 30	14 45	14 0	14 15	14 30	14 45	14 0	14 15
1	14 0	2 30	14 15	2 39	14 30	2 48	14 45	2 57	1
2	14 15	4 51	14 30	5 00	14 45	5 09	1 00	5 18	2
3	14 30	7 03	14 45	7 12	1 00	7 21	1 15	7 30	3
4	14 45	9 15	1 00	9 24	1 15	9 33	1 30	9 42	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
76 0	75 45	75 30	75 15	76 0	75 45	75 30	75 15	76 0	75 45
15 0	15 15	15 30	15 45	15 0	15 15	15 30	15 45	15 0	15 15
1	15 0	2 39	15 15	2 48	15 30	2 57	15 45	3 06	1
2	15 15	5 00	15 30	5 09	15 45	5 18	1 00	5 27	2
3	15 30	7 12	15 45	7 21	1 00	7 30	1 15	7 39	3
4	15 45	9 24	1 00	9 33	1 15	9 42	1 30	9 51	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
75 0	74 45	74 30	74 15	75 0	74 45	74 30	74 15	75 0	74 45
16 0	16 15	16 30	16 45	16 0	16 15	16 30	16 45	16 0	16 15
1	16 0	2 48	16 15	2 57	16 30	3 06	16 45	3 15	1
2	16 15	5 09	16 30	5 18	16 45	5 27	1 00	5 36	2
3	16 30	7 21	16 45	7 30	1 00	7 39	1 15	7 48	3
4	16 45	9 33	1 00	9 42	1 15	9 51	1 30	10 00	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
74 0	73 45	73 30	73 15	74 0	73 45	73 30	73 15	74 0	73 45
17 0	17 15	17 30	17 45	17 0	17 15	17 30	17 45	17 0	17 15
1	17 0	2 57	17 15	3 06	17 30	3 15	17 45	3 24	1
2	17 15	5 18	17 30	5 27	17 45	5 36	1 00	5 45	2
3	17 30	7 30	17 45	7 39	1 00	7 48	1 15	7 57	3
4	17 45	9 42	1 00	9 51	1 15	10 00	1 30	10 09	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
73 0	72 45	72 30	72 15	73 0	72 45	72 30	72 15	73 0	72 45
18 0	18 15	18 30	18 45	18 0	18 15	18 30	18 45	18 0	18 15
1	18 0	3 06	18 15	3 15	18 30	3 24	18 45	3 33	1
2	18 15	5 27	18 30	5 36	18 45	5 45	1 00	5 54	2
3	18 30	7 39	18 45	7 48	1 00	7 57	1 15	8 06	3
4	18 45	9 51	1 00	10 00	1 15	10 09	1 30	10 18	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
72 0	71 45	71 30	71 15	72 0	71 45	71 30	71 15	72 0	71 45
19 0	19 15	19 30	19 45	19 0	19 15	19 30	19 45	19 0	19 15
1	19 0	3 15	19 15	3 24	19 30	3 33	19 45	3 42	1
2	19 15	5 36	19 30	5 45	19 45	5 54	1 00	6 03	2
3	19 30	7 48	19 45	7 57	1 00	8 06	1 15	8 15	3
4	19 45	10 00	1 00	10 09	1 15	10 18	1 30	10 27	4
5	1 00	1 10	1 30	1 18	1 45	1 27	1 55	1 36	5
6	1 15	1 21	1 45	1 24	1 55	1 33	2 00	1 42	6
7	1 30	1 36	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 49	2 00	1 51	2 10	1 57	2 15	2 03	8
9	1 55	1 59	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
71 0	70 45	70 30	70 15	71 0	70 45	70 30	70 15	71 0	70 45
D.	Dep.	Lat.	D.	Dep.	Lat.	D.	Dep.	Lat.	D.

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
16 0	16 15	16 30	16 45	16 0	16 15	16 30	16 45	16 0	16 15
1	16 0	2 56	16 15	3 05	16 30	3 14	16 45	3 23	1
2	16 15	5 11	16 30	5 20	16 45	5 29	1 00	5 38	2
3	16 30	7 26	16 45	7 35	1 00	7 44	1 15	7 53	3
4	16 45	9 41	1 00	9 50	1 15	10 00	1 30	10 09	4
5	1 00	1 10	1 30	1 19	1 45	1 28	1 55	1 37	5
6	1 15	1 20	1 45	1 29	1 55	1 38	2 00	1 47	6
7	1 30	1 30	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 40	2 00	1 49	2 10	1 58	2 15	2 07	8
9	1 55	1 50	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
74 0	73 45	73 30	73 15	74 0	73 45	73 30	73 15	74 0	73 45
17 0	17 15	17 30	17 45	17 0	17 15	17 30	17 45	17 0	17 15
1	17 0	3 24	17 15	3 33	17 30	3 42	17 45	3 51	1
2	17 15	5 39	17 30	5 48	17 45	5 57	1 00	6 06	2
3	17 30	7 54	17 45	8 03	1 00	8 12	1 15	8 21	3
4	17 45	10 09	1 00	10 18	1 15	10 27	1 30	10 36	4
5	1 00	1 10	1 30	1 19	1 45	1 28	1 55	1 37	5
6	1 15	1 20	1 45	1 29	1 55	1 38	2 00	1 47	6
7	1 30	1 30	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 40	2 00	1 49	2 10	1 58	2 15	2 07	8
9	1 55	1 50	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
73 0	72 45	72 30	72 15	73 0	72 45	72 30	72 15	73 0	72 45
18 0	18 15	18 30	18 45	18 0	18 15	18 30	18 45	18 0	18 15
1	18 0	3 51	18 15	4 00	18 30	4 09	18 45	4 18	1
2	18 15	6 06	18 30	6 15	18 45	6 24	1 00	6 33	2
3	18 30	8 21	18 45	8 30	1 00	8 39	1 15	8 48	3
4	18 45	10 36	1 00	10 45	1 15	10 54	1 30	11 03	4
5	1 00	1 10	1 30	1 19	1 45	1 28	1 55	1 37	5
6	1 15	1 20	1 45	1 29	1 55	1 38	2 00	1 47	6
7	1 30	1 30	1 55	1 39	2 00	1 48	2 10	1 57	7
8	1 45	1 40	2 00	1 49	2 10	1 58	2 15	2 07	8
9	1 55	1 50	2 10	1 59	2 15	2 03	2 20	2 10	9
10	2 00	2 00	2 15	2 07	2 20	2 07	2 25	2 15	10
72 0	71 45	71 30	71 15	72 0	71 45	71 30	71 15	72 0	7

P	Lo	Dep	Lat	Dep	Lat	Dep	Lat	Dep	D.
	20	0	20	15	20	30	20	45	
1	1873	700	1873	700	1873	700	1873	700	1
2	1873	700	1873	700	1873	700	1873	700	2
3	1873	700	1873	700	1873	700	1873	700	3
4	1873	700	1873	700	1873	700	1873	700	4
5	1873	700	1873	700	1873	700	1873	700	5
6	1873	700	1873	700	1873	700	1873	700	6
7	1873	700	1873	700	1873	700	1873	700	7
8	1873	700	1873	700	1873	700	1873	700	8
9	1873	700	1873	700	1873	700	1873	700	9
10	1873	700	1873	700	1873	700	1873	700	10
	70	0	40	45	60	30	60	15	
	21	0	21	15	21	30	21	15	
1	1867	707	1867	707	1867	707	1867	707	1
2	1867	707	1867	707	1867	707	1867	707	2
3	1867	707	1867	707	1867	707	1867	707	3
4	1867	707	1867	707	1867	707	1867	707	4
5	1867	707	1867	707	1867	707	1867	707	5
6	1867	707	1867	707	1867	707	1867	707	6
7	1867	707	1867	707	1867	707	1867	707	7
8	1867	707	1867	707	1867	707	1867	707	8
9	1867	707	1867	707	1867	707	1867	707	9
10	1867	707	1867	707	1867	707	1867	707	10
	20	0	64	45	64	30	64	15	
	22	0	22	15	22	30	22	15	
1	1861	714	1861	714	1861	714	1861	714	1
2	1861	714	1861	714	1861	714	1861	714	2
3	1861	714	1861	714	1861	714	1861	714	3
4	1861	714	1861	714	1861	714	1861	714	4
5	1861	714	1861	714	1861	714	1861	714	5
6	1861	714	1861	714	1861	714	1861	714	6
7	1861	714	1861	714	1861	714	1861	714	7
8	1861	714	1861	714	1861	714	1861	714	8
9	1861	714	1861	714	1861	714	1861	714	9
10	1861	714	1861	714	1861	714	1861	714	10
	64	0	67	45	67	30	67	15	
	23	0	23	15	23	30	23	15	
1	1854	721	1854	721	1854	721	1854	721	1
2	1854	721	1854	721	1854	721	1854	721	2
3	1854	721	1854	721	1854	721	1854	721	3
4	1854	721	1854	721	1854	721	1854	721	4
5	1854	721	1854	721	1854	721	1854	721	5
6	1854	721	1854	721	1854	721	1854	721	6
7	1854	721	1854	721	1854	721	1854	721	7
8	1854	721	1854	721	1854	721	1854	721	8
9	1854	721	1854	721	1854	721	1854	721	9
10	1854	721	1854	721	1854	721	1854	721	10
	64	0	67	45	67	30	67	15	
	23	0	23	15	23	30	23	15	
1	1847	728	1847	728	1847	728	1847	728	1
2	1847	728	1847	728	1847	728	1847	728	2
3	1847	728	1847	728	1847	728	1847	728	3
4	1847	728	1847	728	1847	728	1847	728	4
5	1847	728	1847	728	1847	728	1847	728	5
6	1847	728	1847	728	1847	728	1847	728	6
7	1847	728	1847	728	1847	728	1847	728	7
8	1847	728	1847	728	1847	728	1847	728	8
9	1847	728	1847	728	1847	728	1847	728	9
10	1847	728	1847	728	1847	728	1847	728	10
	67	0	66	45	66	30	66	15	
D.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	D.

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
	24 0'		24 15'		24 30'		24 45'		
1	3914	447	3912	441	3910	435	3908	429	1
2	1827	813	1824	821	1820	829	1816	837	2
3	2741	1223	2735	1232	2731	1244	2724	1256	3
4	3654	1627	3647	1643	3640	1649	3633	1671	4
5	4558	2034	4559	2054	4550	2071	4541	2096	5
6	5481	2440	5471	2461	5460	2488	5449	2512	6
7	6395	2847	6382	2875	6370	2903	6357	2931	7
8	7308	3254	7294	3286	7280	3318	7265	3349	8
9	8222	3661	8206	3696	8180	3732	8173	3768	9
10	9135	4067	9118	4107	9100	4147	9081	4187	10
	66 0'		65 45'		65 30'		65 15'		
	25 0'		25 15'		25 30'		25 45'		
1	3905	423	3904	427	3903	431	3901	434	1
2	1813	815	1810	833	1805	861	1801	869	2
3	2719	1268	2714	1280	2708	1292	2702	1303	3
4	3625	1690	3618	1706	3610	1722	3605	1738	4
5	4532	2113	4522	2133	4513	2153	4504	2172	5
6	5438	2536	5427	2559	5416	2583	5404	2607	6
7	6344	2958	6331	2986	6318	3014	6305	3041	7
8	7250	3381	7236	3413	7221	3444	7206	3476	8
9	8157	3804	8140	3839	8123	3875	8106	3910	9
10	9063	4226	9045	4266	9026	4305	9007	4344	10
	65 0'		64 45'		64 30'		64 15'		
	26 0'		26 15'		26 30'		26 45'		
1	809	438	807	442	805	446	803	450	1
2	1708	877	1704	885	1700	892	1786	900	2
3	2606	1315	2601	1327	2685	1339	2679	1350	3
4	3505	1753	3587	1769	3580	1785	3572	1800	4
5	4404	2192	4484	2211	4475	2231	4465	2250	5
6	5303	2630	5381	2654	5370	2677	5358	2701	6
7	6202	3069	6278	3096	6265	3123	6251	3151	7
8	7100	3507	7175	3538	7159	3570	7144	3601	8
9	8089	3945	8072	3981	8054	4016	8037	4051	9
10	8988	4384	8969	4423	8949	4462	8930	4501	10
	64 0'		63 45'		63 30'		63 15'		
	27 0'		27 15'		27 30'		27 45'		
1	801	454	889	458	887	462	885	466	1
2	1782	908	1778	916	1774	923	1770	931	2
3	2675	1362	2667	1374	2661	1385	2655	1397	3
4	3564	1816	3556	1831	3548	1847	3540	1862	4
5	4455	2270	4445	2289	4435	2309	4425	2328	5
6	5346	2724	5334	2747	5322	2770	5310	2794	6
7	6237	3178	6223	3205	6209	3232	6195	3259	7
8	7128	3632	7112	3663	7096	3694	7080	3725	8
9	8019	4086	8001	4121	7984	4156	7965	4186	9
10	8913	4540	8890	4579	8870	4617	8850	4656	10
	64 0		63 45		63 30		63 15		
D	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	D

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
	28 0		28 15		28 30		28 45		
1	881	477	881	477	879	477	877	481	1
2	1702	947	1702	947	1708	934	1703	962	2
3	2544	1438	2544	1438	2556	1431	2550	1445	3
4	3322	1878	3324	1878	3335	1909	3307	1924	4
5	4048	2307	4044	2307	4064	2380	4084	2455	5
6	4728	2817	4728	2817	4753	2865	4760	2886	6
7	5358	3306	5358	3306	5392	3415	5397	3457	7
8	5934	3785	5937	3785	5981	3817	5984	3848	8
9	6452	4257	6458	4257	6519	4294	6520	4329	9
10	6909	4723	6919	4723	6998	4772	7007	4810	10
	29 0		29 15		29 30		29 45		
1	872	480	872	480	870	482	868	486	1
2	1713	970	1713	970	1711	985	1706	992	2
3	2554	1461	2554	1461	2561	1473	2555	1489	3
4	3338	1911	3340	1911	3351	1950	3371	1988	4
5	4064	2441	4062	2441	4082	2462	4101	2491	5
6	4748	2952	4748	2952	4772	2994	4777	3036	6
7	5378	3441	5378	3441	5412	3485	5417	3527	7
8	5954	3920	5957	3920	5991	3965	5994	3996	8
9	6472	4392	6478	4392	6539	4442	6540	4477	9
10	6929	4848	6939	4848	6998	4921	7007	4959	10
	30 0		30 15		30 30		30 45		
1	864	484	864	484	862	488	860	492	1
2	1722	1000	1728	1008	1725	1015	1719	1022	2
3	2568	1490	2562	1491	2585	1525	2578	1532	3
4	3354	1940	3352	1940	3366	1980	3385	2018	4
5	4080	2470	4078	2470	4098	2508	4117	2546	5
6	4764	2980	4762	2980	4782	3015	4787	3056	6
7	5394	3470	5394	3470	5428	3515	5433	3557	7
8	5970	3940	5971	3940	6005	3985	6008	4016	8
9	6488	4412	6494	4412	6555	4462	6556	4499	9
10	6949	4868	6959	4868	7018	4921	7027	4959	10
	31 0		31 15		31 30		31 45		
1	856	487	856	487	854	491	852	495	1
2	1732	1010	1738	1018	1735	1025	1729	1032	2
3	2578	1510	2572	1511	2595	1545	2588	1552	3
4	3364	1970	3362	1970	3376	2010	3395	2048	4
5	4090	2500	4088	2500	4108	2538	4127	2576	5
6	4774	3000	4772	3000	4792	3035	4797	3076	6
7	5404	3490	5404	3490	5438	3535	5443	3579	7
8	5980	3960	5981	3960	6015	4005	6018	4036	8
9	6498	4442	6504	4442	6565	4492	6566	4529	9
10	6959	4918	6969	4918	7028	4971	7037	5009	10
	32 0		32 15		32 30		32 45		
1	848	490	848	490	846	494	844	498	1
2	1742	1020	1748	1028	1745	1035	1739	1042	2
3	2588	1520	2582	1521	2605	1555	2598	1562	3
4	3374	1980	3372	1980	3386	2020	3405	2058	4
5	4100	2530	4098	2530	4118	2568	4137	2606	5
6	4784	3010	4782	3010	4802	3045	4807	3086	6
7	5414	3500	5414	3500	5448	3545	5453	3589	7
8	5990	3970	5991	3970	6025	4015	6028	4046	8
9	6508	4472	6514	4472	6575	4522	6576	4559	9
10	6969	4948	6979	4948	7038	5001	7047	5039	10
	33 0		33 15		33 30		33 45		
1	840	493	840	493	838	497	836	501	1
2	1752	1030	1758	1038	1755	1045	1749	1052	2
3	2598	1530	2592	1531	2615	1565	2608	1572	3
4	3384	1990	3382	1990	3396	2030	3415	2068	4
5	4110	2540	4108	2540	4128	2578	4147	2616	5
6	4794	3020	4792	3020	4812	3055	4817	3096	6
7	5424	3510	5424	3510	5458	3555	5463	3601	7
8	6000	3980	6001	3980	6035	4025	6038	4056	8
9	6518	4502	6524	4502	6585	4552	6586	4589	9
10	6979	4978	6989	4978	7048	5041	7057	5079	10
	34 0		34 15		34 30		34 45		
1	832	496	832	496	830	500	828	504	1
2	1762	1040	1768	1048	1765	1055	1759	1058	2
3	2608	1540	2602	1541	2625	1575	2618	1582	3
4	3394	2000	3392	2000	3406	2040	3425	2078	4
5	4120	2550	4118	2550	4138	2588	4157	2626	5
6	4804	3030	4802	3030	4822	3065	4827	3106	6
7	5434	3520	5434	3520	5468	3565	5473	3611	7
8	6010	3990	6011	3990	6045	4035	6048	4066	8
9	6528	4532	6534	4532	6595	4582	6596	4619	9
10	6989	5008	6999	5008	7058	5101	7067	5139	10
	35 0		35 15		35 30		35 45		
1	824	499	824	499	822	503	820	507	1
2	1772	1050	1778	1058	1775	1065	1769	1062	2
3	2618	1550	2612	1551	2635	1585	2628	1592	3
4	3404	2010	3402	2010	3416	2050	3435	2088	4
5	4130	2560	4128	2560	4148	2598	4167	2636	5
6	4814	3040	4812	3040	4832	3075	4837	3116	6
7	5444	3530	5444	3530	5478	3575	5483	3621	7
8	6020	4000	6021	4000	6055	4045	6058	4076	8
9	6538	4562	6544	4562	6605	4612	6606	4649	9
10	6999	5038	7009	5038	7068	5131	7077	5169	10
	36 0		36 15		36 30		36 45		
1	816	502	816	502	814	506	812	510	1
2	1782	1060	1788	1068	1785	1075	1779	1068	2
3	2628	1560	2622	1561	2645	1595	2638	1602	3
4	3414	2020	3412	2020	3426	2060	3445	2098	4
5	4140	2570	4138	2570	4158	2608	4177	2646	5
6	4824	3050	4822	3050	4842	3085	4847	3126	6
7	5454	3540	5454	3540	5488	3585	5493	3631	7
8	6030	4010	6031	4010	6065	4055	6068	4086	8
9	6548	4592	6554	4592	6615	4642	6616	4689	9
10	7009	5068	7019	5068	7078	5151	7087	5249	10
	37 0		37 15		37 30		37 45		
1	808	505	808	505	806	509	804	513	1
2	1792	1070	1798	1078	1795	1085	1789	1072	2
3	2638	1570	2632	1571	2655	1605	2648	1612	3
4	3424	2030	3422	2030	3436	2070	3455	2108	4
5	4150	2580	4148	2580	4168	2618	4187	2656	5
6	4834	3060	4832	3060	4852	3095	4857	3136	6
7	5464	3550	5464	3550	5498	3595	5503	3641	7
8	6040	4020	6041	4020	6075	4065	6078	4096	8
9	6558	4622	6564	4622	6625	4672	6626	4719	9
10	7019	5098	7029	5098	7088	5181	7097	5289	10
	38 0		38 15		38 30		38 45		
1	800	508	800	508	798	512	796	516	1
2	1802	1080	1808	1088	1805	1095	1799	1078	2
3	2648	1580	2642	1581	2665	1625	2658	1632	3
4	3434	2040	3432	2040	3446	2080	3465	2118	4
5	4160	2590	4158	2590	4178	2628	4197	2666	5
6	4844	3070	4842	3070	4862	3105	4867	3146	6
7	5474	3560	5474	3560	5508	3605	5513	3651	7
8	6050	4030	6051	4030	6085	4075	6088	4106	8
9	6568	4652	6574	4652	6635	4702	6636	4749	9
10	7029	5128	7039	5128	7098	5221	7107	5329	10
	39 0		39 15		39 30		39 45		
1	792	511	792	511	790	515	788	519	1
2	1812	1090	1818	1098	1815	1105	1809	1088	2
3	2658	1590	2652	1591	2675	1645	2668	1652	3
4	3444	2050	3442	2050	3456	2090	3475	2128	4
5	4170	2600	4168	2600	4188	2638	4207	2676	5
6	4854	3080	4852	3080	4872	3115	4877	3156	6
7	5484	3570	5484	3570	5518	3615	5523	3661	7
8	6060	4040	6061	4040	6095	4085	6098	4116	8
9	6578	4682	6584	4682	6645	4732	6646	4789	9
10	7039	5158	7049	5158	7108	5261	7117	5389	10
	40 0		40 15		40 30		40 45		
1	784	514	784	514	782	518	780	522	1
2	1822	1100	1828	1108	1825	1115	1819	1098	2
3	2668	1600	2662	1601	2685	1655	2678	1662	3
4	3454	2060	3452	2060	3466	2100	3485	2138	4
5	4180	2610	4178	2610	4198	2648	4217	2686	5
6	4864	3090	4862	3090	4882	3125	4887	3166	6
7	5494	3580	5494	3580	5528	3625	5533	3671	7
8	6070	4050	6071	4050	6105	4095	6108</		

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
	36° 0'		36° 15'		36° 30'		36° 45'		
1	.809	.588	.806	.591	.804	.595	.801	.598	1
2	1.618	1.176	1.613	1.183	1.608	1.190	1.603	1.197	2
3	2.427	1.763	2.419	1.774	2.412	1.784	2.404	1.795	3
4	3.236	2.351	3.226	2.365	3.215	2.379	3.205	2.393	4
5	4.045	2.939	4.032	2.957	4.019	2.974	4.006	2.992	5
6	4.854	3.527	4.839	3.548	4.823	3.569	4.808	3.590	6
7	5.663	4.115	5.645	4.139	5.627	4.164	5.609	4.188	7
8	6.472	4.702	6.452	4.730	6.431	4.759	6.410	4.787	8
9	7.281	5.290	7.258	5.322	7.235	5.353	7.211	5.385	9
10	8.090	5.878	8.064	5.913	8.039	5.948	8.013	5.983	10
	37° 0'		37° 15'		37° 30'		37° 45'		
1	.799	.602	.796	.605	.793	.609	.791	.612	1
2	1.597	1.204	1.592	1.211	1.587	1.218	1.581	1.224	2
3	2.396	1.805	2.388	1.816	2.380	1.826	2.372	1.837	3
4	3.195	2.407	3.184	2.421	3.173	2.435	3.163	2.449	4
5	3.993	3.009	3.980	3.026	3.967	3.044	3.953	3.061	5
6	4.792	3.611	4.776	3.632	4.760	3.653	4.744	3.673	6
7	5.590	4.213	5.572	4.237	5.553	4.261	5.535	4.286	7
8	6.389	4.815	6.368	4.842	6.347	4.870	6.326	4.898	8
9	7.188	5.416	7.164	5.448	7.140	5.479	7.116	5.510	9
10	7.986	6.018	7.960	6.053	7.934	6.088	7.907	6.122	10
	38° 0'		38° 15'		38° 30'		38° 45'		
1	.788	.616	.785	.619	.783	.623	.780	.626	1
2	1.576	1.231	1.571	1.238	1.565	1.245	1.560	1.252	2
3	2.364	1.847	2.356	1.857	2.348	1.868	2.340	1.878	3
4	3.152	2.463	3.141	2.476	3.130	2.490	3.120	2.504	4
5	3.940	3.078	3.927	3.095	3.913	3.113	3.899	3.130	5
6	4.728	3.694	4.712	3.715	4.696	3.735	4.679	3.756	6
7	5.516	4.310	5.497	4.334	5.478	4.358	5.459	4.381	7
8	6.304	4.925	6.283	4.953	6.261	4.980	6.239	5.007	8
9	7.092	5.541	7.068	5.572	7.043	5.603	7.019	5.633	9
10	7.880	6.157	7.853	6.191	7.826	6.225	7.799	6.259	10
	39° 0'		39° 15'		39° 30'		39° 45'		
1	.777	.629	.774	.633	.772	.636	.769	.639	1
2	1.554	1.259	1.549	1.265	1.543	1.272	1.538	1.279	2
3	2.331	1.888	2.323	1.898	2.315	1.908	2.307	1.918	3
4	3.109	2.517	3.098	2.531	3.086	2.544	3.075	2.558	4
5	3.886	3.147	3.872	3.164	3.858	3.180	3.844	3.197	5
6	4.663	3.776	4.646	3.796	4.630	3.816	4.613	3.837	6
7	5.440	4.405	5.421	4.429	5.401	4.453	5.382	4.476	7
8	6.217	5.035	6.195	5.062	6.173	5.089	6.151	5.116	8
9	6.994	5.664	6.970	5.694	6.945	5.725	6.920	5.755	9
10	7.771	6.293	7.744	6.327	7.716	6.361	7.688	6.394	10
	40° 0'		40° 15'		40° 30'		40° 45'		
1	.766	.643	.763	.646	.760	.649	.758	.653	1
2	1.532	1.286	1.526	1.292	1.521	1.299	1.515	1.306	2
3	2.298	1.928	2.290	1.938	2.281	1.948	2.273	1.958	3
4	3.064	2.571	3.053	2.584	3.042	2.598	3.030	2.611	4
5	3.830	3.214	3.816	3.231	3.802	3.247	3.788	3.264	5
6	4.596	3.857	4.579	3.877	4.562	3.897	4.545	3.917	6
7	5.362	4.500	5.343	4.523	5.323	4.546	5.303	4.569	7
8	6.128	5.142	6.106	5.169	6.083	5.196	6.061	5.222	8
9	6.894	5.785	6.869	5.815	6.844	5.845	6.818	5.875	9
10	7.660	6.428	7.632	6.461	7.604	6.494	7.576	6.528	10
	41° 0'		41° 15'		41° 30'		41° 45'		
1	.755	.656	.752	.659	.749	.663	.746	.666	1
2	1.509	1.312	1.504	1.319	1.498	1.325	1.492	1.332	2
3	2.264	1.968	2.256	1.978	2.247	1.988	2.238	1.998	3
4	3.019	2.624	3.007	2.637	2.996	2.650	2.984	2.664	4
5	3.774	3.280	3.759	3.297	3.745	3.313	3.730	3.329	5
6	4.528	3.936	4.511	3.956	4.494	3.976	4.476	3.995	6
7	5.283	4.592	5.263	4.615	5.243	4.638	5.222	4.661	7
8	6.038	5.248	6.015	5.275	5.992	5.301	5.968	5.327	8
9	6.792	5.905	6.767	5.934	6.741	5.964	6.715	5.993	9
10	7.547	6.561	7.518	6.593	7.490	6.626	7.461	6.659	10
	42° 0'		42° 15'		42° 30'		42° 45'		
1	.743	.669	.740	.672	.737	.676	.734	.679	1
2	1.486	1.338	1.480	1.345	1.475	1.351	1.469	1.358	2
3	2.229	2.007	2.221	2.017	2.212	2.027	2.203	2.036	3
4	2.973	2.677	2.961	2.689	2.949	2.702	2.937	2.715	4
5	3.716	3.346	3.701	3.362	3.686	3.378	3.672	3.394	5
6	4.459	4.015	4.441	4.034	4.424	4.054	4.406	4.073	6
7	5.202	4.684	5.182	4.707	5.161	4.729	5.140	4.752	7
8	5.945	5.353	5.922	5.379	5.898	5.405	5.875	5.430	8
9	6.688	6.022	6.662	6.051	6.636	6.080	6.609	6.109	9
10	7.431	6.691	7.402	6.724	7.373	6.756	7.343	6.788	10
	43° 0'		43° 15'		43° 30'		43° 45'		
1	.731	.682	.728	.685	.725	.688	.722	.692	1
2	1.463	1.364	1.457	1.370	1.451	1.377	1.445	1.383	2
3	2.194	2.046	2.185	2.056	2.176	2.065	2.167	2.075	3
4	2.925	2.728	2.913	2.741	2.901	2.753	2.889	2.766	4
5	3.657	3.410	3.642	3.426	3.627	3.442	3.612	3.458	5
6	4.388	4.092	4.370	4.111	4.352	4.130	4.334	4.149	6
7	5.119	4.774	5.099	4.796	5.078	4.818	5.057	4.841	7
8	5.851	5.456	5.827	5.481	5.803	5.507	5.779	5.532	8
9	6.582	6.138	6.555	6.167	6.528	6.195	6.501	6.224	9
10	7.314	6.820	7.284	6.852	7.254	6.884	7.224	6.915	10
	44° 0'		44° 15'		44° 30'		44° 45'		
1	.719	.692	.716	.695	.713	.698	.710	.701	1
2	1.438	1.384	1.433	1.391	1.428	1.398	1.423	1.405	2
3	2.157	2.066	2.150	2.074	2.143	2.082	2.136	2.090	3
4	2.876	2.768	2.867	2.777	2.859	2.786	2.850	2.795	4
5	3.595	3.459	3.584	3.469	3.573	3.479	3.562	3.489	5
6	4.314	4.139	4.302	4.150	4.290	4.161	4.278	4.172	6
7	5.033	4.764	5.019	4.776	5.005	4.788	4.991	4.799	7
8	5.752	5.405	5.736	5.418	5.721	5.431	5.705	5.444	8
9	6.471	6.056	6.453	6.070	6.436	6.084	6.419	6.098	9
10	7.190	6.707	7.170	6.722	7.151	6.736	7.132	6.750	10
	45° 0'		45° 15'		45° 30'		45° 45'		
1	.707	.701	.704	.704	.701	.707	.698	.713	1
2	1.416	1.397	1.412	1.404	1.408	1.411	1.404	1.417	2
3	2.125	2.098	2.120	2.105	2.116	2.108	2.112	2.120	3
4	2.834	2.799	2.828	2.806	2.823	2.812	2.817	2.825	4
5	3.543	3.499	3.536	3.506	3.531	3.514	3.525	3.533	5
6	4.252	4.199	4.244	4.206	4.238	4.214	4.230	4.240	6
7	4.961	4.898	4.952	4.906	4.944	4.914	4.935	4.945	7
8	5.670	5.597	5.660	5.606	5.650	5.614	5.640	5.650	8
9	6.379	6.296	6.368	6.310	6.357	6.322	6.345	6.355	9
10	7.088	6.995	7.076	6.999	7.064	7.014	7.051	7.061	10
	46° 0'		46° 15'		46° 30'		46° 45'		
1	.695	.713	.692	.716	.689	.719	.686	.722	1
2	1.384	1.417	1.380	1.420	1.376	1.423	1.372	1.426	2
3	2.073	2.120	2.068	2.123	2.064	2.126	2.060	2.129	3
4	2.762	2.825	2.756	2.828	2.751	2.831	2.746	2.834	4
5	3.451	3.533	3.444	3.536	3.438	3.539	3.434	3.542	5
6	4.140	4.240	4.132	4.243	4.125	4.246	4.118	4.249	6
7	4.829	4.898	4.820	4.901	4.812	4.904	4.804	4.907	7
8	5.518	5.557	5.508	5.560	5.500	5.563	5.492	5.566	8
9	6.207	6.224	6.196	6.227	6.188	6.230	6.180	6.233	9
10	6.896	6.913	6.884	6.916	6.876	6.919	6.868	6.922	10
	47° 0'		47° 15'		47° 30'		47° 45'		
1	.683	.722	.680	.725	.677	.728	.674	.731	1
2	1.362	1.426	1.358	1.429	1.354	1.432	1.350	1.435	2
3	2.041	2.129	2.036	2.132	2.032	2.135	2.028	2.138	3
4	2.720	2.834	2.714	2.837	2.710	2.840	2.706	2.843	4
5	3.399	3.542	3.392	3.545	3.386	3.548	3.382	3.551	5
6	4.078	4.285	4.070	4.288	4.064	4.291	4.059	4.294	6
7	4.757	4.928	4.748	4.931	4.742	4.934	4.736	4.937	7
8	5.436	5.567	5.426	5.570	5.419	5.573	5.412	5.576	8
9	6.115	6.204	6.						

D.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	D.
	44° 0'		44° 15'		44° 30'		44° 45'		
1	.719	.695	.716	.698	.713	.701	.710	.704	1
2	1.439	1.389	1.433	1.396	1.427	1.402	1.420	1.408	2
3	2.158	2.084	2.149	2.093	2.140	2.103	2.131	2.112	3
4	2.877	2.779	2.865	2.791	2.853	2.804	2.841	2.816	4
5	3.597	3.473	3.582	3.489	3.566	3.505	3.551	3.520	5
6	4.316	4.168	4.298	4.187	4.280	4.205	4.261	4.224	6
7	5.035	4.863	5.014	4.885	4.993	4.906	4.971	4.928	7
8	5.755	5.557	5.730	5.582	5.706	5.607	5.682	5.632	8
9	6.474	6.252	6.447	6.280	6.419	6.308	6.392	6.336	9
10	7.193	6.947	7.163	6.978	7.133	7.009	7.102	7.040	10
	45° 0'		45° 15'		45° 30'		45° 45'		
	45° 0'		45° 15'		45° 30'		45° 45'		
1	.707	.707	.704	.710	.701	.713	.698	.716	1
2	1.414	1.414	1.408	1.420	1.402	1.427	1.396	1.433	2
3	2.121	2.121	2.112	2.131	2.103	2.140	2.093	2.149	3
4	2.828	2.828	2.816	2.841	2.804	2.853	2.791	2.865	4
5	3.536	3.536	3.520	3.551	3.505	3.566	3.489	3.582	5
6	4.243	4.243	4.224	4.261	4.205	4.280	4.187	4.298	6
7	4.950	4.950	4.928	4.971	4.906	4.993	4.885	5.014	7
8	5.657	5.657	5.632	5.682	5.607	5.706	5.582	5.730	8
9	6.364	6.364	6.336	6.392	6.308	6.419	6.280	6.447	9
10	7.071	7.071	7.040	7.102	7.009	7.133	6.978	7.163	10
	45° 0'		44° 45'		44° 30'		44° 15'		
D.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	D.

MISCELLANEOUS TABLE.

WHEN DIAMETER = 1.

		LOG.
Circumference of circle, π ,	3.14159	0.49715
Area of circle,	.78540	9.89509-10
Contents of sphere,	.52360	9.71900-10
Earth's equatorial radius, in miles,	.3962.57	3.59798
Earth's polar radius, in miles,	.3949.324	3.59652
Compression, $1 - 299.1528$,	0.00334	7.52411-10

EQUIVALENTS.

1	American mile =	.86756	nautical miles,	9.93830-10	
1	"	= 1609.40831	meters,	3.20667	
1	"	= .21689	German geograph. miles,	9.33624-10	
1	"	= 1.50866	Russian versta,	0.17859	
1	"	yard =	.91444	meters,	9.96115-10
1	"	" =	.48217	Vienna klafter,	9.68320-10
1	"	foot =	.30481	meters,	9.48403-10
1	"	" =	.15639	toises,	9.19421-10
1	"	" =	.93835	Parisian feet,	9.97236-10
1	"	" =	.96435	Vienna feet,	9.98423-10
1	"	" =	1.09395	Spanish feet,	0.03900

Deg.	0'	10'	20'	30'	40'	50'
0	0.0	9.9	19.9	29.8	39.7	49.7
1	59.6	69.5	79.5	89.4	99.3	109.3
2	119.2	129.2	139.1	149.0	159.0	168.9
3	178.9	188.8	198.8	208.7	218.7	228.6
4	238.6	248.6	258.5	268.5	278.4	288.4
5	298.4	308.4	318.3	328.3	338.3	348.3
6	358.3	368.3	378.2	388.2	398.2	408.2
7	418.3	428.3	438.3	448.3	458.3	468.3
8	478.4	488.4	498.4	508.5	518.5	528.6
9	538.6	548.7	558.8	568.8	578.9	589.0
10	599.1	609.2	619.3	629.4	639.5	649.6
11	659.7	669.8	680.0	690.1	700.2	710.4
12	720.5	730.7	740.9	751.0	761.2	771.4
13	781.6	791.8	802.0	812.2	822.5	832.7
14	842.9	853.2	863.4	873.7	884.0	894.2
15	904.5	914.8	925.1	935.4	945.7	956.1
16	966.4	976.7	987.1	997.5	1007.8	1018.2
17	1028.6	1039.0	1049.4	1059.8	1070.2	1080.7
18	1091.1	1101.6	1112.0	1122.5	1133.0	1143.5
19	1154.0	1164.5	1175.1	1185.6	1196.1	1206.7
20	1217.3	1227.9	1238.5	1249.1	1259.7	1270.3
21	1281.0	1291.6	1302.3	1313.0	1323.7	1334.4
22	1345.1	1355.8	1366.6	1377.3	1388.1	1398.9
23	1409.7	1420.5	1431.3	1442.1	1453.0	1463.8
24	1474.7	1485.6	1496.5	1507.4	1518.4	1529.3
25	1540.3	1551.3	1562.3	1573.3	1584.3	1595.4
26	1606.4	1617.5	1628.6	1639.7	1650.8	1661.9
27	1673.1	1684.3	1695.5	1706.7	1717.9	1729.1
28	1740.4	1751.7	1762.9	1774.3	1785.6	1796.9
29	1808.3	1819.7	1831.1	1842.5	1854.0	1865.4
30	1876.9	1888.4	1899.9	1911.4	1923.0	1934.6
31	1946.2	1957.8	1969.4	1981.1	1992.8	2004.5
32	2016.2	2028.0	2039.7	2051.5	2063.3	2075.2
33	2087.0	2098.9	2110.8	2122.7	2134.7	2146.7
34	2158.6	2170.7	2182.7	2194.8	2206.9	2219.0
35	2231.1	2243.3	2255.5	2267.7	2279.9	2292.2
36	2304.5	2316.8	2329.2	2341.5	2353.9	2366.4
37	2378.8	2391.3	2403.8	2416.3	2428.9	2441.5
38	2454.1	2466.8	2479.5	2492.2	2504.9	2517.7
39	2530.5	2543.3	2556.2	2569.1	2582.0	2594.9
40	2607.9	2621.0	2634.0	2647.1	2660.2	2673.3
41	2866.5	2699.7	2713.0	2726.3	2739.6	2752.9
42	2766.3	2779.8	2793.2	2806.7	2820.3	2833.8

MERIDIONAL PARTS.

Deg.	0'	10'	20'	30'	40'	50'
43	2847.4	2861.1	2874.8	2888.5	2902.2	2916.0
44	2929.9	2943.7	2957.6	2971.6	2985.6	2999.6
45	3013.7	3027.8	3042.0	3056.2	3070.4	3084.7
46	3099.0	3113.4	3127.8	3142.3	3156.8	3171.3
47	3185.9	3200.5	3215.2	3230.0	3244.7	3259.6
48	3274.5	3289.4	3304.3	3319.4	3334.4	3349.6
49	3364.7	3380.0	3395.2	3410.6	3425.9	3441.4
50	3456.9	3472.4	3488.0	3503.7	3519.4	3535.1
51	3550.9	3566.8	3582.8	3598.7	3614.8	3630.9
52	3647.1	3663.2	3679.6	3696.0	3712.4	3728.9
53	3745.4	3762.0	3778.7	3795.4	3812.2	3829.1
54	3846.0	3863.1	3880.1	3897.3	3914.5	3931.8
55	3949.1	3966.6	3984.1	4001.7	4019.3	4037.0
56	4054.8	4072.7	4090.7	4108.7	4126.9	4145.1
57	4163.3	4181.7	4200.2	4218.7	4237.3	4256.0
58	4274.8	4293.7	4312.7	4331.7	4350.9	4370.1
59	4389.4	4408.9	4428.4	4448.0	4467.7	4487.5
60	4507.5	4527.5	4547.6	4567.8	4588.1	4608.6
61	4629.1	4649.8	4670.5	4691.4	4712.4	4733.5
62	4754.7	4776.0	4797.5	4819.0	4840.7	4862.5
63	4884.5	4906.5	4928.7	4951.0	4973.5	4996.0
64	5018.8	5041.6	5064.6	5087.7	5111.0	5134.4
65	5158.0	5181.7	5205.5	5229.5	5253.7	5278.0
66	5302.5	5327.1	5351.9	5376.9	5402.1	5427.4
67	5452.8	5478.5	5504.3	5530.3	5556.5	5582.9
68	5609.5	5636.3	5663.2	5690.4	5717.7	5745.3
69	5773.1	5801.1	5829.3	5857.7	5886.3	5915.2
70	5944.3	5973.6	6003.2	6033.0	6063.1	6093.4
71	6124.0	6154.8	6185.9	6217.2	6248.9	6280.8
72	6313.0	6345.5	6378.2	6411.3	6444.7	6478.4
73	6512.4	6546.8	6581.5	6616.5	6651.8	6687.6
74	6723.6	6760.1	6796.9	6834.1	6871.7	6909.7
75	6948.1	6987.0	7026.2	7065.9	7106.1	7146.7
76	7187.8	7229.3	7271.4	7313.9	7357.0	7400.6
77	7444.8	7489.5	7534.8	7580.7	7627.0	7674.3
78	7722.1	7770.5	7819.6	7869.4	7919.9	7971.1
79	8023.1	8075.9	8129.5	8184.0	8239.3	8295.4
80	8352.5	8410.6	8469.6	8529.7	8590.8	8653.0
81	8716.3	8780.9	8846.6	8913.6	8981.9	9051.6
82	9122.7	9195.3	9269.4	9345.2	9422.7	9501.9
83	9583.0	9666.0	9751.1	9838.3	9927.8	10019.6
84	10114.0	10211.0	10310.8	10413.6	10519.6	10628.8
85	10741.7	10858.4	10979.2	11104.3	11234.2	11369.1

CORRECTIONS FOR MIDDLE LATITUDE.

DIFFERENCE OF LATITUDE.																						
Mid. Lat.	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	Mid. Lat.		
15°	1'	2'	3'	4'	5'	6'	7'	8'	9'	10'	11'	12'	13'	14'	15'	16'	17'	18'	19'	20'	15°	
16	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	16	
17	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	17	
18	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	18	
19	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	19	
20	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	20	
21	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	
22	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	22	
23	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	23	
24	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	24	
25	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	25	
26	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	26	
27	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	27	
28	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	28	
29	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	29	
30	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	30	
31	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	31	
32	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	32	
33	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	33	
34	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	34	
35	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	35	
36	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	36	
37	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	37	
38	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	38	
39	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	39	
40	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	40	
41	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	41	
42	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	42	
43	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	43	
44	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	44	
45	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	45	
46	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	46	
47	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	47	
48	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	48	
49	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	49	
50	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	50	
51	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	51	
52	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	52	
53	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	53	
54	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	54	
55	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	55	
56	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	56	
57	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	57	
58	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	58	
59	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	59	
60	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	60	
61	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	61	
62	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	62	
63	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	63	
64	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	64	
65	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	65	
66	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	66	
67	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	67	
68	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	68	
69	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	69	
70	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	70	

